737 FMC USER'S GUIDE Advanced Guide to the 737 Flight Management Computer

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Let's skip the haughty phrases normally reserved for book introductions and get right to the point. This manual is about improving your piloting skills through the integration of the Flight Management Computer.

The FMC User's Guide is a collection of data from many sources, including the factory and airline manuals, training material, instructors, line pilots like yourself, and others.

This manual is written for the pilot who has already acquired basic skills of FMC operation.

The guide will be updated by the issuance of revisions. Revisions are necessary to keep up with industry procedures, hardware and software development, to add techniques as I learn them, and to correct mistakes. Send in the registration card so you will be placed in my database. You can also check my web site for revision information. Please ensure that I have your current address so that I may send a notice when the next revision is available. A small fee will be required to keep you manual up to date. I encourage the use of e-mail as it will help to keep my long distance phone bill down.

The Smiths FMC, installed in all Boeing 737-300s through 800s, has been used by the author in preparing this manual.

Here is a word of caution to those operating the Honeywell FMC, used in the Airbus, the F-100, MD-11, and all Big Boeings. These Honeywell FMCs come in two base lines, due to different kickoff customers. I call them the Boeing and the European baselines. The Boeing baseline of Honeywell is quite similar to the Boeing baseline of Smiths. Much of the information in this manual does pertain to the B-757/767, the B747-400, and the B777, but many differences do exist. I recommend the BIG BOEING FMC USER'S GUIDE we now produce for users of this equipment. The Honeywell European baseline (found on the MD-11, Fokker, and Airbus) is quite different and no attempt is made at this time to cover these computers.

The 737 FMC USER'S GUIDE is designed to be used as a reference and as a supplement to the operator's publications. If any suggestions herein conflict with approved procedures in your airplane flight manual, our company's procedures, or the manufacturer's pilot guides, these other sources shall take precedence over these contents.

Due to the variable content and ongoing revisions of each operator's customized navigation database, these page displays are only intended to provide a general description of overall systems capability. They do not necessarily reflect customized data of the specific operator, nor are they intended to reflect valid navigation or performance data.

The layout is such that information is presented in a fashion that is readily available. It is organized by Mode Key sequence. This sequence approximates the chronological use of the FMC during a typical flight. For a quick reference, use the index in the back of the book.

Although thoroughly researched, the information in this handbook is subject to change after publication. I welcome your suggestions for improvements and invite you to send me your real time experiences to include herein. This will tap the experience of may pilots and will be passed on to all revision subscribers. This is a very educational experience.

HISTORY OF LEAR SIEGLER

The Flight Management Computer in the Boeing 737 family is manufactured by the Smith Industries, SLI Avionics Systems Corporation in Grand Rapids, Michigan. The company has quite an interesting history. The FMC is probably not the first instrument you've used from this group.

In 1930, William P. Lear formed a company in Chicago he called Lear Wuerful, Inc. Its first industrial contribution was an automobile radio he invented.

The next year the company name was changed to Lear Development, Inc. and introduced a low-cost light weight aircraft radio transceiver called the Magic Brain. By 1935, the company was almost entirely engaged in design, development, and manufacture of airborne radio transceivers and direction finding equipment, including the Lear-O-Scope radio direction finder.

During WW II, Lear engineers developed the Fastop electromagnetic clutch for accurately stopping devices operated by high speed electric motors. These mechanisms were used in landing gear assemblies on every B-24 and B-29 built.

The Learmatic Navigator, an instrument providing a pilot with straight-track navigation using any radio station available was introduced in 1940 and won Bill Lear the Frank M. Hawks Memorial Award.

During the war, the company was building linear and rotary actuators, power units, and automatic and remote electrical controls.

The headquarters were moved to Grand Rapids in 1945.

In 1950, Bill Lear was awarded the Collier Trophy for the development of the Auto Flight Control System for the F-5. (The Collier Trophy is an annual award for the greatest achievement in aviation in America. Glen Curtis was awarded the first in 1912 by the Aero Club of America for his flying boat.)

By 1958, production of the Flight Director-Attitude Indicator and All-Attitude Two-Gyro Master Reference System for the USAF's Integrated Panel cockpit display established Lear as the USA's first production supplier of this type of equipment for the military.

In 1962, Lear and Siegler Corp of Illinois announced a merger - Lear Siegler. From 1969 through the seventies, the Instrument Division placed a lot of equipment into space: a camera on Gordon Cooper's spacecraft, the pilot's ADI and other instruments on the Gemini program, instruments on the Apollo spacecraft (lunar and command module). LSI had produced the DG for the lunar rover that operated on the moon in 1970. The computer systems moved from the space program to the B 747 in 1970, followed by the Performance Data Computer System (1982), the digital flight control system for the F-15E (1985), weapons management system for the F-14D Tomcat (1985) and the Self-contained Navigation System for the Air Force's C-130 (1985).

Smiths was founded in 1851 by Samuel Smith (1827-1875). The son of a potato merchant, he was a watch and clockmaker, and started his first shop in Newington Causeway, South London, near the El-ephant & Castle, "an area crowded with shops interspersed with several splendid gin palaces". The business prospered and expanded under the founder's son, Samuel, Jr (eldest of twelve). In 1871 the business was moved to The Strand. In 1882 additional branches were opened in Piccadilly and Trafalgar Square.

It is not surprising that the skills of watch makers were considered appropriate to the requirements of the emerging motor industry, even though speed limits were as low as 12 mph. Allen Gordon-Smith, Sam Jr.'s fifth child and manager of the Piccadilly shop, joined the pioneers as one of the people credited with the invention of the mileometer. King Edward VII asked, "Why can't you make an instrument to show the speed I am traveling, as well as the distance?" The outcome was the first British speedometer, installed in King Edward's 18/28 hp Mercedes. Three years and several speedometers later, the company was granted a Royal Warrant. By 1908, sales of Smiths Perfect Speedometers exceeded 100 per week. The Goldenlyte headlamp business was acquired and also the car lighting and starting business of Trier and Martin in 1913.

In 1911, a Blackburn B1, equipped with a Smiths tachometer, was the first aircraft to fly with a Smiths instrument.

S. Smith & Sons (Motor Accessories) Ltd., became a public company in 1914. The use of wristwatches grew during W.W.I; the company also made 'tankometers', kite balloon wind indicators, shell fuses, wire rope, lighting sets, signalling lamps, and KLG spark plugs. In 1917, they acquired an airspeed indicator invented by Holcomb Clift, using an oilskin diaphragm. This product became the recognized standard indicator of its day. Such an instrument was fitted to the record-breaking Vickers Vimy bomber in which Alcock and Brown made their historic crossing of the Atlantic in 1919.

The company successfully weathered the depression years of the early twenties.

In 1927, Smiths gained controlling interest in Jaeger Ltd., a speedometer maker, plus Robinhood Engineering Works Ltd. Apparently though, Sir Allen's first love was clock making, to which he devoted himself. In 1928 he formed the All British Escapement Co., Ltd. Previously, all these items had been imported from Switzerland. This proved useful during W.W. II. The clock side of the business was further boosted in 1931 with the introduction of the first synchronous electric clock.

In 1929, Smiths Aircraft Instruments was formed, though Smiths was already supplying instruments and accessories to many manufacturers including the victorious Schneider Trophy airplanes.

Product expansion included the first electrical fuel gauge in 1932, followed by electrical thermometers and oil pressure gauges.

In 1931, Smiths acquired a pneumatic autopilo from Henry Hughes & Son Ltd., marine engineers. The first Smiths autopilot was produced in 1933.

By 1936 the Smiths Desynn System of remote indication became standard equipment on practically every British-built aircraft. Sir Allen headed a team of eight executives who visited the U.S. to conduct a comprehensive survey of American techniques in aviation instrumentation. It is possible that he met Bill Lear. As a result, Smiths acquired a license from Bendix for the production in Britain of aviation instruments, including the altimeter.

With W.W.II imminent, the company moved out of the London area to Bishops Cleeve, Cheltenham. Sir Allen left the company to work in the government's Ministry of Aircraft Production. He returned in 1945 and began to expand, forming Radiomobile Ltd to manufacture car radios. An electric auto-pilot was introduced in 1947. Sir Allen died in 1951.

By 1961 motor accessories still dominated; every one of the one million Morris Minors produced up to that time had Smiths instrumentation.

Smiths' first Boeing contract was for 160 machmeters for the 727. In 1964, the Trident became the first civil airliner to land in fog under fully automatic control with visibility no more that 50 meters - equipped with an autopilot from Smiths.

The last fifteen years has seen the gradual decline and disappearance of the once great automotive and time keeping businesses and the emergence of new electronically based high-technology businesses. The most dramatic has been the appearance of concepts such as the all glass flight deck and other computeraided systems.

The clock factory was closed in 1979 and the distribution business closed in 1983, severing its link with the company's origins.

In 1983, the automotive group was sold to Lucas Industries, a long time competitor.

Smiths established a U.S. operation in 1958, but it was not until the acquisition of the Instrument and Avionics Systems Division of Lear Siegler, Inc. i 1987 that the U.S. operations took on the importance that they have today.

As B737 pilots, we're linked to destiny through Smiths indicators such as the airspeed, altimeter, fuel, flap, and engine instruments, the clock, and the A/T system. 7.

Principles of FMC (and Autoflight) operation, as viewed by your authors. If the following concepts conflict with your company SOP, then your company SOP must prevail.

- 1. One pilot always flies the airplane. Sounds obvious, but it is surprising how often both 8. pilots will have their heads down during an FMC modification.
- Think of the FMC as your "electronic flight 2. bag". Most (but not all) of the information you need in flight can be retrieved from the FMC.
- Understand the advantages of glass. Perfor-3. mance and navigation are more accurate. Although it takes a few minutes more to preflight the automation and enter the flight plan, many routine operations in flight are easier, quicker and more accurate. Analog flight instruments are expensive to repair. It's cheaper to replace a 9. CRT or LCD.
- Independent verification is required if initial 4. position is entered by latitude and longitude. 10. This means that the other pilot (either pilot can make the initial entry) independently verifies 11. If you'reoperating non-GPS equipment, recogthe initial position using a separate source document. In international operations crossing into East longitudes or the Equator, use caution and avoid transposing E for W or N for S. One pilot does not read the latitude and longitude to the other pilot! It is the authors' opinion that a database entry of the Airport Reference Point is safer to use than a manually entered gate position.
- If departure time is sneaking up on you, and you 5. don't have time to key the entire route, then don't. Load enough waypoints to get your airplane to TOC and to a point where you will have enough time to load the remainder of the route. After all, rope-start airplanes with INS could 13. Think of Vertical Speed as "Very Special". only load 9 waypoints at a time. Oh, yes. We like to anchor the end of a partial route with the ICAO four letter identifier of the destination airport. That lets the FMC take a wag at the fuel 14. This is a book about the Flight Management score until you have time to feed it better information. The ICAO airport will be automatically replaced with the appropriate arrival and runway when you enter it.
- Use extra time to enter the most complete infor-6. mation into the FMC. On very short flights, there is little practical reason to enter several enroute winds. On long range flights, forecast winds play an important role in fuel predictions. Entering the most likely arrival path, runway and speeds will enable the FMC to most accurately predict time and fuel at destination. Also,

entry of the destination runway will permit modifications to be made at the end of the flight plan that do not affect the fuel score.

- Appreciate the speed and accuracy of the FMC, but be prepared for glitches.
- At some point during the descent, only the most necessary FMC entries are made. This point may vary, and is the subject of lively debate among standardization weenies. They will advocate points anywhere from TOD to the traffic pattern. Our view is that when you get busy, that's the time to spend less time with the FMC. That point might be TOD at ORD, but 5,000 feet at DSM. At that point, airplane control is changed to LVL CH and HDG SEL when the path and track deviate from that which is programmed in the FMC.
- Know your airplane and verify FMC calculations. Every number displayed by the FMC should pass your test of reasonableness.
- The airplane can be operated safely on raw data, just like a 727.
- nize situations where the possibility of map shift exists. Remote areas served by a single VOR, or multiple VORs located close together qualify. Operations over or in the vicinity of the former USSR, North Korea or China are candidates for extra caution, also.
- 12. If time is critical in flight and one of the pilots is new to glass, it is prudent that the best qualified pilot make the FMC modification. It is important that new captains recognize this and manage their cockpits accordingly. When the urgency has passed, the pilot who made the modification should thoroughly explain the keystrokes used to make the change.
- With the exception of three specific situations, some mode of autoflight other than V/S is probably more appropriate.
- System, but because it is inexorably linked to Autoflight, we would be remiss in not mentioning one more thing. There will be times that the FMC and Autoflight are not appropriate to the situation, and the safest way to operate the airplane is to disconnect the magic and handfly it. Examples of this might be in reacting to a TCAS warning to avoid a potential collision, to side-step to an adjacent runway or to stop your climb in response to an urgent request on the part of ATC.

- 15. Anytime a crew makes an entry into the FMC that has the potential of changing the flight path, the other crew should be invited to confirm prior to execution. If only one pilot receives a clearance or makes a CDU entry and executes it, the other pilot may be unaware of why the airplane starts a maneuver or the FMS changes modes.
- 16. Even though the HSI Map is no more accurate than the updated FMC position, we recommend both pilots fly in Map. If in an area that is suspect of inaccurate navaids, occasionally check your FMC position against raw data, but return to the Map mode. This is easily done if flying on an airway. GPS input will solve this problem.
 - 1) The pilot must understand completely the concept of "Real vs. FMC" position.
 - 2) The pilot must be proficient in verifying FMC position. Page 4.10 describes one technique. Even on domestic flights, every time you got an IRS NAV ONLY or VERIFY POSITION message, do a quick position check.
 - 3) This should be a simulator training item onstration during IOE.

5) During terrain-critical approaches, one pilot must monitor raw data not later than the Initial Approach Fix (IAF) or the equivalent point. In all cases, one pilot must monitor raw data inside the Final Approach Fix (FAF).

The author recognizes that the SOP of some airlines require that one pilot monitor raw data under certain circumstances. These typically include high terrain and areas of suspected inaccurate updating.

The disadvantages to this procedure include:

- 1) The possibility of diminished situational awareness on the part of the pilot monitoring raw data.
- 2) Difficulty on the part of the pilot monitoring raw data to assess and verify modifications to the route.
- 3) Reduced ability to recognize an along-track map shift in a timely manner.
- 4) Potential for less-than-optimum FMC updating on some airplanes.
- during transition; or at least a specific dem- 17. Automation should only be a supplement to a pilot's airmanship and not a substitute; automation is only the means to an end. Unfortunately, this philosophy is not always taught and the excessive emphasis on automation can result in the loss of basic flying skills. Norm Komich

May 98

The *FMC USER'S GUIDE* employs the following conventions to make it easier for you to learn useful information without slogging through a lot of words.

CAUTION Action that may damage equipment, delay a flight, or cause some other undesireable outcome.

U3.0 & up Specific software will be provided in this special box. The title defines the particular update(U).

Should a procedure possibly

Procedures, this symbol will

present a conflict with a

S carrier's Standard Operating

be displayed.

Information considered "technique" will be in this special box. "Technique" is presented for your consideration only. In some cases it may not be an approved procedure for your operation. It is presented for your education, usually to demonstrate capabilities of the FMCS.

CHECKAIRMEN ONLY Demonstration to be carried out by an instructor pilot or a person familiar and comfortable with the equipment. If the procedure goes against company

precedures, of course company

procedures take precedence.



U10.2 software will support a color Liquid Crystal Display (LCD) CDU. Currently there are 5 colors being implemented:

COLOR CODING OF TEXT

CYAN (C)	Inactive Route page titles.
GREEN (G)	Active toggles and actively tuned navaid data.
MAGENTA (M)	Active go-to waypoint, target speed, and target altitude.
	Active Hold pattern data is also displayed in magenta.
WHITE (W)	ACARS prompts that have been selected, edits to the
	flight plan, cruise altitude, etc.
AMBER (A)	Maintenance pages to indicate that a dual FMC mismatch has occured.

If you have questions or suggestions, please call. E-mail is preferred. Bill Bulfer <bbulfer@firstnethou.com>



CONDENSED PREFLIGHT



Dec 02

The purpose of this page is to give the pilot an overview of the enroute process of the FMC. This page takes the pilot from climb to approach.



B 737 SYSTEM DESCRIPTION

The Flight Management Computer (FMC) in the Boeing 737 has been developed from the Lear Siegler (LS-54) family of processors. There are four basic models; the smaller the number preceding the Modular Concept Unit (MCU), the smaller the box.

2904A series.

U1.x software base. 8 MCU non EFIS. 2904D series.

U3, U4, U5, or U6 software base. 8 MCU. 2904F series.

U4, U5, or U6 software base. 8 MCU. 2907A series.

U7/8/10 software base. Dual/4 MCU.

A byte is the smallest discrete memory unit which a microprocessor can handle. A *word* is generally the largest discrete unit that a microprocessor can handle *efficiently*. The unit of measure for the database is 16-bit words. On the Motorola 68x family of processors, a *word* is two bytes. A *long-word* is four bytes. 1 meg is 1024 words.

The FMC and the CDU make up the 737 Flight Management Computer System (FMCS).

It is convenient to think of the FMC as an electronic Operations Manual. This is a simplification, for the FMC furnishes a great deal more information than can be obtained from the Ops Manual. The cost ptimum speed schedules used in climb, cruise, and escent are an excellent example. This is the essential difference between the FMC and a conventional area nav system.

The Flight Management Computer and Control Display Units (FMC/CDU) provide the pilots with a flight management tool which performs navigational and performance computations. Computations related to lateral navigation include items such as courses to be flown, ETA's, and distances-to-go. Route segments may be flown as Great Circle tracks between flight-planned waypoints, as constant heading legs, or as published airways, depending on flight plan criteria. For vertical navigation, computations include items such as fuel-burn data and optimum speeds and altitudes.

In addition, the FMC also provides control and guidance commands which can be coupled to the Autopilot/Flight Director System (AFDS) and Autothrottle (A/T). This allows integrated FMS operation with automatic lateral and vertical navigation. In this way, the FMC unburdens the crew from many routine system integration tasks and allows them to concentrate upon management of the flight.

The crew may select any degree of automation desired. This can mean simply using the CDU for reference during manual flight, or using conventional autopilot functions, or selecting full FMS operation with automatic flight path guidance and performance control.

The basic system configuration consists of a Flight Management Computer and one Control Display Unit. Some installations of the FMCS may include two CDUs, one for each pilot, and an alternate navigation system, called the Alternate Navigation Control/Display Unit (ANCDU). The ANCDU operates independently of any other CDU. It can be used as a standard CDU in a non-nav mode for crew inputs only, to provide an alternate independent source of navigation for cross-checking other systems, or with the FMC inop, the ANCDU can be used to provide back-up IRS navigation by providing lateral guidance information to the (E)HSIs and autopilot.



The FMC storage is made up of three types of memory: erasable programmable read-only memory (EPROM), nonvolatile random access memory (NV RAM), and high-speed volatile random access memory (HS RAM).

Power for the NV RAM memory is provided by the computer power supply whenever power is applied to the FMC. When power is removed, the memory elements are switched to a low-power standby state specially designed for data retention. Power for the standby mode is provided by an internal solid-state dry lithium battery.

The FMC contains storage space for two data bases; they are the Navigation database, of which the Temporary database is a part, and the Performance database.

The Navigation database is stored in the NV RAM memory and in two parts: a main body of active data that is effective until a specified expiration date, and a set of data revisions for the next period of effectivity.

Nav database suppliers as of June 2001 are Jeppesen Sanderson, Swissair, Thales Avionics (Racal), LIDO GmbH, SAS, and NIMA.

The Performance database has the average model of the aircraft and the engines.

The average aircraft model includes high speed drag polars, a buffet limit envelope, certified operating limits, and speed and altitude capability of engine out.

This model is used during computations of fuel flow, thrust, engine limits and target values, and for corrections for the effects of air-conditioning and anti-icing bleeds. Thrust targets for turbulence penetration are also provided for crew advisory.

The aerodynamic and engine models used as the performance database for the FMCS represent the average, in-service model of the 737. This data is from aircraft design information and flight tests and have been shown through experience to represent the characteristics of the average fleet. However, each aircraft may have its own peculiarities so the FMC contains provisions allowing maintenance personnel to make adjustments to suite each individual aircraft. Factors which adjust the aircraft's drag and fuel flow modeling data over a range of -9.9% to +9.9% from the baseline are enterable from the CDU. They are retained in NV RAM memory for continued use. (Ref: Perf Factors)

The Loadable Defaults function provides a mechanism for the carrier to prepare and load a customized list of default parameters. Typical default examples are:

Transition AltitudeClimb ModeDeparture Airport Spd rest.TO Flap for QRHMax & min spd in clb, crz, desACARS messagesQRH data tablesClimb Mode

There are three independent computing units within the FMC: (1) the Navigation Processor for navigation computations, lateral and vertical steering guidance, and CDU management; (2) the Performance Processor for performance computations, flight envelope protection, and some vertical steering guidance related to target speeds, and (3) the Input/Output Processor, which performs the functions associated with I/O handling and some management of the CDU and management of the Built-In Test (BIT).

The link among the three controlled by the Global RAM, which acts as a common "mailbox" message and data shuttle point. It holds, in a single place, all the information the three processors require.

The FMC is certified to navigate accurately within a VOR/DME and GPS environment.

FMC navigational computations are based upon an FMC System position that is established using radio inputs and/or IRU present position. The FMC position may be based upon IRU data only; however, available GPS, DME or VOR/DME inputs are normally used to refine and update the FMC Posi-



We don't actually navigate off the inertial platforms. All they do is provide independent inputs to the FMC(s) which integrate the sensors into a nav solution which is better than any one of the sensors.

In a dual IRU installation, the FMC uses five positions to arrive at navigation solutions:

It obtains basic position and velocity data from the IRU. The left IRU is used unless invalid or deselected. The IRU position is then checked against the data received from ground and/or space based sensors to determine the IRS drift rates and offset corrections.

Using all this data, the FMC generates the Best position every five seconds.

The Radio position data is obtained using GPS, DME-DME, ILS LOC, or VOR/DME updating when radio aids are available. Since the FMC assumes the Radio position is more accurate than the IRS position in use, the Best position is biased heavily toward the Radio position, and may cause problems if the Radio position is not accurate.

The updated Best position is used to correct the System position, which is the navigation position used for airplane guidance in LNAV.

INERTIAL REFERENCE UNIT

Dec 02

This material is based on a paper writen by Richard Stensland and by correspondence with Stuart Law on the Bluecoat Forum.

STRAPDOWN INERTIAL NAVIGATION

Inertial navigation is the process of determining a vehicle's location using internal inertial sensors rather than external references. Three accelerometers and three gyros are needed because, in a threedimensional world, an aircraft can simultaneously accelerate and rotate in three axes.

The term strapdown indicates that the gyros and accelerometers are mounted solidly to the aircraft. It eliminates the need for gimbals, bearings, and torque motors to keep the sensors level with the surface of the earth. The accelerometers are mounted such that the input axis of one accelerometer is always in the longitudinal axis, one is in the lateral axis, and one is in the vertical axis. Likewise, the gyros are mounted such that one gyro senses roll, one senses pitch, and the other senses yaw.

The laser gyros allow the microprocessors to maintain a stable platform mathematically, rather than mechanically. This results in an increase in system reliability and accuracy.

The primary source of attitude, velocity, and position information is the Inertial Reference System (IRS). The development of the IRS had to await the advent of the laser and advances in such optical technology as fiber-optic cables and highly reflective mirrors. From this technology there have emerged two classes of optical rotation sensors: fiber-optic gyros and ring-laser gyros.

The laser gyro has caused a technological revolution in the design of inertial reference and navigation systems. Laser gyros are not gyros in the traditional sense of the word. Rather, they are angular rate sensors that operate in one particular axis. This solid-state, high-precision, angular rate sensor is ideally suited for strapdown system configurations. This has been made possible through the advent of the laser gyro and high-speed microprocessors. The microprocessor calculates velocity, position, and attitude from the angular rate measurements and inertial sensors' acceleration.

AIR DATA INERTIAL REFERENCE UNIT

The Air Data Inertial Reference Unit (ADIRU) has three parts; power supply, inertial reference (IR), and the air data reference (ADR). On the 300-400-500, the air data reference is separate.

The ADIRU operates with either power source, 115v ac or 28v dc. The power supply feeds the ADR, the IR, the ISDU and to the air data modules (ADMs).

The IRS includes two ADIRUs, one inertial system display unit (ISDU), and one mode select unit. The IR is the heart of the IRS. The main function of each IR is to sense and compute linear accelerations and angular turning rates about each of the airplane's axis. This data is used for pitch and roll displays and navigational computations.

The sensed data is resolved to local vertical coordinates and combined with air data inputs to compute attitude (pitch, roll, and yaw), position (latitude and longitude), true and magnetic heading, inertial velocity vectors, linear accelerations, angular rates, track angle, wind speed and direction, inertial altitude, vertical speed and acceleration, ground speed, drift angle, flight path angle and acceleration.

The only other inputs required are initial position, barometric altitude, and true airspeed. Initial position is required because present position is calculated from the distance and direction traveled from the starting point. Barometric altitude stabilizes the vertical navigation, and thereby stabilizes the vertical velocity and inertial altitude outputs.

The ADR supplies altitude, vertical speed, and true airspeed to the IR processor. The IR uses this ADR data as part of its inertial altitude, vertical speed and wind calculations.

Barometric correction comes from the common display system (CDS).

ACCELEROMETER

The three ring laser gyros can accurately measure rotation in any axis, however they give no measurement of the aircraft's movement through space. This is accomplished by three inertial accelerometers. The accelerometer is a mass centered in an outer case by two springs.

When the airplane accelerates or decelerates, the mass moves from the center. A pick-off device is positioned so that it can measure the size of the swing, and generate an electrical signal proportional to the swing. This signal is amplified proportionately into a current, which is used to torque the mass back to the null position. This recentering operation allows the accelerometer to sense very small changes in acceleration over a wide range. The amount of the signal necessary to keep the mass centered is proportional to airplane acceleration.

The current output of the accelerometer is an analog signal. The current is converted to a digital signal and supplied to the IR processor. The IR processor integrates the feedback signal with time to calculate velocity and then integrates the calculated velocity with time to calculate distance flown.

For example, a vehicle accelerating at three feet per second squared would be traveling at a velocity of 30 feet per second after 10 seconds have passed. Note that acceleration was simply multiplied by time to get velocity. The processor also integrates the calculated velocity to determine position. For example, a vehicle traveling at a velocity of 30 feet per second for 10 seconds will have changed position by 300 feet. Velocity was simply multiplied by time to determine the position.

initial position to calculate present position.

LASER

The laser gyro operates on the Sagnac effect. (Georges Marc Marie Sagnac - 1913).

The first ring-laser gyro was demonstrated by Sperry Gyroscope Co. (now Honeywell) in 1963.

The laser gyro can have three or more sides. The Honeywell gyro is actually triangular-shaped, cut and drilled from a block of temperature-stable glass.

Each side of the 737 and 757 / 767 gyro is 4.2 inches long. The new series 737 has sides reduced to 2 inches in length.

At each corner is a very accurate mirror. One mirror is partially transparant so that some of the light can shine through it.

A small amount of helium-neon gas is sealed into the tunnel. A dc voltage is applied to anodes and a cathode when you turn the MSU switch out of the OFF position. The discharge that develops is similar to that in a neon sign. The discharge excites helium atoms into several energy states. Many of these helium atoms collect in a relatively stable energy state, which is at nearly the same energy level as excited neon atoms. Because these levels are so close to each other, they can easily exchange energy. This happens when an excited helium atom collides with an unexcited neon atom, causing the helium atom to lose its energy while the neon atom becomes excited. This process is known as "pumping", because neon atoms are thereby pumped into a high-energy state.

Light amplification occurs when a photon strikes a neon atom that has been pumped into the excited state, causing the atom to generate an additional photon as it makes a transition into the lower energy state. Pumping is necessary in that it ensures that more neon atoms are at the higher energy level than at the lower level. Lower energy level atoms use up the photons, whereas the higher energy level atoms emit photons. As long as there are more higher level atoms than lower level atoms, there will be more photons emitted than absorbed. This results in a net gain of photons, or an amplification of light also known as "lasing".

In a laser cavity, photons are emitted (or light is radiated) in all directions. However, only the light crease in frequency, that radiates in a straight line between the mirrors is whereas the other beam will reinforced by repeated trips through the gain me- exhibit a frequency dedium. The mirrors are specially coated to act as both crease.

reflectors and optical filters, reflecting the single frequency of light that the system uses and absorbing all others. This repeated amplification of the light reflecting between the mirrors soon reaches saturation, and a steady-state oscillation results. The IR processor then adds distance flown to the This light oscillating between the mirrors is typically called a laser beam. To obtain useful laser light outside the laser cavity, a small percentage of the laser beam is allowed to pass through one of the



block in opposite directions. One beam travels in a clockwise direction and the other travels in a counterclockwise direction.

The laser gyro measures rotation by using the properties of these two laser beams rotating in opposite directions.

Now, imagine one laser beam traveling clockwise - we'll call Beam 1, and one traveling counter clockwise - we'll call Beam 2.

Rotate the graphic a few degrees clockwise. Beam 1, which left point A traveling clockwise around the cavity at the speed of light, reaches its starting point, which, due to the slight clockwise rotation, has moved to another point, we'll think of as Point B. Beam 1's path is now longer than it would have been had the picture not been rotated, so the wavelength must lengthen proportionately.

Meanwhile, Beam 2, traveling counter-clockwise, has a shorter path than Beam 1's because its starting point has also moved to point B. Beam 2's shortened path results in shortened wavelengths.

When the wavelengths change there is a concurrent change in the light's frequency. This means that in a rotating gyro one laser beam will exhibit an in-



INERTIAL REFERENCE UNIT

can't wait to get out in the garage and hook up that old Mac or 286 to some fiber-optic cables you've got laying around.

In normal operating conditions, the frequency change of the laser beam is incredibly small; it cannot be measured to such an accuracy, but the frequency difference between the two beams is easily and accurately measured using an optical means.

This is done by combining light from the two beams in a nearly parallel fashion such that the wave fronts of the two beams interfere with each the two beams are equal, the fringe pattern will be stationary. If the frequencies are different, the fringe pattern will move at a rate proportional to the frequency difference.

One of the corners of the gyro contains a partially silvered mirror and a corner prism which lets the two light beams mix together to form a fringe pattern on a detector. Photo diodes sense the fringe pattern rate and direction of movement and change the fringe pattern movement into a signal that is equal to the rotation rate of the gyro. The measured rotation rate is integrated with time to calculate the attitude of the airplane.

Thus, frequency difference between the laser beams becomes a measure of rotation rate. Any difference in frequency is sensed by the photocell detector at the end of the light paths.

When the IRU is static, scatter from the mirrored surfaces can cause the opposing beams to lock together in a dead band around the zero-rate point until rotation of the unit reaches a certain rate. This condition is called laser lock-in or beam coupling. To prevent a loss of information at low rotation rates, a piezo-electric dither motor vibrates the gyro assembly through the lock-in region. The gyro sensed signals that are caused by these vibrations, are decoupled from the gyro output to prevent errors during operation. The dither motor vibration can be felt on the IRU case and produces an audible hum.

INERTIAL NAVIGATION

Although it is used to calculate velocity and position, acceleration is meaningless to the system without additional information. For example, consider an accelerometer strapped down to the longitudinal axis of the aircraft and measuring a forward acceleration. Is the aircraft acceleration north, south, east, west, up, or down? In order to navigate over the surface of the earth, the system must know how this aircraft acceleration is related to the earth's surface. Because accelerations are measured by accelerometers that are mounted to the three axes of

It gets easier to understand now. I know you the aircraft, the IRS must know the relationship of each axis to the surface of the earth. The laser gyros make the measurements necessary to describe this relationship in terms of pitch, roll, and heading angles. These angles are calculated from the angular rates measured by the gyros through an integration - similar to the manner in which velocity is calculated from measured acceleration.

> For example, suppose a gyro measures a yaw rate of 3° per second for 30 seconds. Through integration, the microprocessor calculates that the heading has changed by 90° after 30 seconds.

Given the knowledge of pitch, roll, and heading other and form a fringe pattern. If the frequencies of that the gyros provide, the microprocessor resolves the acceleration signals into earth-related accelerations, and then performs the horizontal and vertical navigation calculations.

> Suppose the gyro signals have been integrated to indicate that the aircraft's heading is 45° and the pitch and roll are both zero. The only acceleration measured has been in the longitudinal axis and it has been integrated into a velocity of 500 miles per hour. After flying at a constant heading and attitude for one hour, the microprocessor has integrated the velocity to determine that the aircraft has flown to a latitude and longitude that is 500 miles northeast of the original location. In doing so, the IRS has used the acceleration signals in conjunction with the gyro signals to calculate the present position.

ALIGNMENT

IR alignment basically consists of determination of local vertical and initial heading. Both accelerometer and laser gyro inputs are used for alignment.

The IR has to establish the level (North/East) plane and the direction to True North with extreme accuracy with only 3 inputs: your estimate of location, gravity, and the Earth's rotation. The alignment computations use the premise that the only accelerations during alignment are due to the earth's gravity and the only motion during alignment is due to the earth's rotation.

Leveling of the IR (vertical velocity) and altitude are calculated using the acceleration that is measured perpendicular to the earth's surface. This local vertical is used to erect the attitude data so that it is accurately referenced to vertical.

This is essentially the same as getting the pendulum on your clock to hang perfectly straight down. Every time you move it, the smallest error has it oscillating. Unfortunately the pendulum length for an inertial is to the center of the Earth (thus the natural Schuler frequency of 84 min for pendulum oscillations). However, an inertial accelerometer cannot distinguish between gravitational force and actual aircraft acceleration. Consequently, any ac-

INERTIAL REFERENCE UNIT

celerometer that is not perfectly parallel to the means that the alignment can't ever find True North earth's surface will measure a component of the earth's gravity in addition to the true aircraft acceleration. Therefore, the IRS's microprocessor must subtract the estimated local gravity from the measured vertical acceleration signal. This prevents the system from interpreting gravitational force as upward aircraft acceleration. Since there is always some error, there is always some Schuler oscillation.

Once vertical is established, the laser gyro sensed earth rate components are used to establish the heading of the airplane.

True north and present position latitude is calculated. After the ADIRU has measured these values and the present position (latitude and longitude) is entered, the ADIRU completes its alignment to true north, both the vertical reference and the heading determinations are fine tuned for maximum accuracy and is then ready to navigate.

Earth rate sensing by the laser gyros allows the IRU to determine initial latitude but it cannot calculate its present position longitude.

This gyro-determined latitude is compared to the crew entered latitude to make sure its calculation of latitude is correct. Crew entered longitude is compared to the last stored longitude. These comparisons must be favorable to complete the alignment period.

When both ADIRUs are in ALIGN mode, the position you enter goes to both ADIRUs. If you make a wrong entry, you can enter the data again. The ADIRUs use the last data entry that you make.

NAV MODE

The gyros measure the motion of the aircraft with respect to the earth, plus the motion of the earth with respect to inertial space. The earth rotates with respect to inertial space at a rate of one rotation per 24 hours as it spins from west to east on its own axis, plus one rotation per year as it revolves around the sun. The sum of these two rates is equivalent to an angular rate of about 15 degrees per hour. (North Pole, earth rate is zero, azimuth rate of 15°/hr. At the Equator, earth rate is 15°/hr and azimuth rate is zero. In the middle earth rate varies as the cosine of the latitude.) The microprocessor compensates for this rate by subtracting this value, which is stored in memory, from the signal measured by whichever gyro or gyros are pointed eastward. Without this earth rate compensation, an IRS operating at the equator would mistakenly think that it is upside down after 12 hours of navigation. At other places on the earth, the system would develop similar errors in pitch, roll, and heading. If you input the wrong latitude, the IRS will compute the wrong earth rate value (deg/hr). The wrong earth rate

well, since the Earth rate compensation doesn't work; the ALIGN lights would continue to flash.

The major effect imposed by the earth's spherical shape is somewhat similar to that caused by the earth's rotation. As an aircraft travels across the surface of the earth, its path becomes an arc due to the shape of the earth. Consequently, the gyros particularly the pitch axis gyro - measure a rotational rate, because traveling in a curved path always involves rotation. This rate, called the transport rate, does not describe rotational motion of the aircraft with respect to the earth's surface. Therefore, the IRS must calculate how much transport rate is being measured by the gyros, and subtract that value from their measurements.

INS errors continue to diverge with average amplitude increasing exponentially.

A close observation of the individual IRS position on the POS REF page will show that occasionally they will drift slowly apart, and then move back together again over a period of time. This can be due to the Schuler-tuning of the IRSs.

The basic design of any inertial system (INS or IRS) would have it maintain a reference to a fixed point in space. However, in navigating around the Earth, there is a problem that a straight line is not really that; it must constantly curve downward to follow the curvature of the Earth. With the gyroscopically stabilized platform of the INS, the platform tilt is constantly biased to allow for this. With the strapdown IRS, an equivalent bias signal is applied to the readouts of the IRUs.

The Schuler-Tuning signal has an 84 minute sinusoidal cycle and will cause slight position oscillations (around 1 nm) during the cycle. While all IRUs are subject to this effect, individual IRUs will not necessarily be at the same point in their cycles, with the result that they may drift apart at one stage of the cycle and back together again later.

After a full 84 minute cycle, the IRUs have the ability to introduce a bias signal to compensate for Schuler drift and this aspect of IRU performance will be gradually refined on longer flights as the flight progresses.

There are many other effects (such as coning, sculling, size effect, Coriolis effect, etc.) that are compensated for in commercial inertial reference systems, and even more in systems used in military applications. These effects have not been considered in this discussion because they get more and more complicated as higher precision is demanded, yet do not appreciably increase understanding of the strapdown nav principles.

DUAL FMC CONFIGURATION

DUAL FMC CONFIGURATION - B737

A dual FMC configuration meets the "sole means of navigation" requirement. Redundancy - two FMCs; Integrity - the FMCs can successfully determine how much error exists in the position. The U7.2/8.1 is the first Smiths software certified for "sole means".

A dual configuration will allow use of Precision RNAV airways - 2 nm in width and FMS approaches in a non radar environment.

A dual FMC configured FMCS has the same interfaces as a single FMC system except for the Intersystem Bus (ISB). The operation of these interfaces is different in that the dual FMCS must direct the data to 2 FMC's. This direction is determined by the setting of the 3 position FMC switch. It can be set on NORMAL, BOTH ON L, or BOTH ON R.



FMC switch in NORMAL

In the NORMAL position the FMC switch designates that the left FMC drives FCC-A, the autothrottle, the left EFIS map, the left autopilot, both CDU's, and tunes the left radio receiver. The right FMC drives FCC-B, the right EFIS map, the right autopilot, and tunes the right radio receiver. The guidance / map position and velocity are a weighted average of each FMC's data. CDU keypress events are passed from the left to the right FMC through the ISB. Composite navigation is enabled and N1 limits are provided by the left FMC. A change in the switch results in the disengagement of LNAV and VNAV, and a resynchronization attempt via memory copy if currently in single operation (for dual installation).

The FMCS will select the combination of available sensors that provide the best valid data for updating the estimate of the aircraft state (position and velocity). In the dual configuration with the FMC switch in the NORMAL setting only, a second aircraft state is calculated in each FMC by combining both FMCs error estimates and applying that to the estimated aircraft state. This is called the *composite navigation solution*. Both single and dual systems select and tune stations based on the current aircraft position and the navaid position obtained from the navigation data base. Dual systems require that at least one navaid is not shared between FMCs so there is navigation independence. This is a requirement for primary means navigation.

FMC switch on BOTH ON L or BOTH ON R

With the FMC switch set to BOTH ON L or BOTH ON R the dual FMCS operates just like a single FMC installation. Both FCCs, EFIS maps, radio receivers, CDUs, and autothrottle are driven by the selected primary FMC. So the primary FMC is providing the guidance commands and map display data. The secondary FMC remains synchronized with the primary FMC. A change in the switch results in the disengagement of LNAV and VNAV.

Intersystem Bus

The dual FMC FMCS includes an Inter-System Bus (ISB) to communicate between FMCs.

Ground Start-up

The ISB maintains uniform configurations and synchronization. This is done by comparisons performed at start-up and in flight. At start-up, it does a cross compare of the OFPs and data bases. If an OFP mismatch exists, the primary FMC will display the crossload page. This page provides for the crossloading of OFPs. A different crossload page is displayed for a data base miscompare. The data bases that are compared are contained in the following list: Nav and Performance data bases, QRH takeoff speeds, ACARS datalink configurations, Supp data bases, and software options data base.

If the Supp data base exists and does not compare to the other FMC's Supp data base, the first FMC to be powered-up will automatically crossload its data to the other FMC. If the first FMC has no Supp data base and the second FMC does, the second FMC's data is crossloaded to the first powered-on FMC.

FMC configurations are also compared at startup. If a mismatch exists, the primary FMC displays an appropriate BITE page to help isolate the miscompared data. If the mismatch is not resolved before the BITE pages are exited, the secondary FMC conditional-fails. A conditional-failed FMC does not transmit valid data on its output channels.

The primary FMC also checks the status of the secondary FMC and automatically crossloads pilot entered data as required to maintain synchronization between the two FMC's. Some of these procedures are performed by maintenance.

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Downmode to SINGLE FMC OPS

follow this procedure.

Downmode to SINGLE FMC OPS due to a miscompare or communication bus failure is not an FMC failure. The FMC FAIL annunciation does not display. This gives you independent operation of the FMCs...with one being in the standby mode (hot program pins, performance factors and status are spare) in case the other one fails. The downmode to single can be caused by miscompares of .5% on N1 targets, small differences in Distance-To-Go to the next waypoint, differences on airspeed targets, altitudes, etc. The FMC is quite capable of predicting the values well within the tolerances given equal inputs. Without equal inputs, or in the case of a spurious input, the outputs vary. If the outputs vary enough for a period of time within which they should have equalized, the master FMC, normally the left, divorces the right FMC; the right FMC is brickwalled. The brickwalled FMC no longer takes part in guidance or Map position.

Dual integrity is still available but you should verify the other FMC is operating.

If the downmode to single ops occurs during taxiout, place the FMC switch to BOTH ON RIGHT. If the CDU LEGS pages and the EFIS/ND Maps display correct information, the right FMC is operating. Switch to BOTH ON LEFT and again check the flight plan and EFIS/ ND Maps for proper information; continue in the BOTH ON LEFT OF BOTH ON RIGHT mode.

If the downmode to single ops occurs while On Demand Dual Synchornization airborne, occassionally accomplish the reasonableness check (BOTH ON RIGHT and LEFT) comparing each waypoint (sequence, course and distance) and crosstrack error (PROGRESS 3/3).

Even though one FMC is brickwalled, they continue to update. If the FMCs come to an agreement and return to work together the DUAL FMC OP RE-STORED message signals that you can return to NORMAL.

The fault is recorded in the maintenance records of the FMC. Maintenance will be able to do a data dump to disc and possibly identify the miscompare. In-Flight Restarts

If an in flight restart occurs while radio updated If the FMC FAIL annunciation displays, do not navigation is being performed, the normal operation continues. If necessary, the flight plan and performance data may be re-entered and activated. At that point, all guidance commands are output normally after having been NCD (no computed/return data).

> Also after an in flight restart, the OFP, data bases, compared. Differences in the OFP, data bases, program pins or performance factors cause single FMC operation annunciation and failure of the secondary FMC. The Supp nav data base automatically crossloads the same way as on the ground, if a miscompare exists. The primary status is also automatically crossloaded to the secondary FMC.

On-Going Dual Synchronization

The primary FMC transmits all CDU keypush events to the secondary FMC. This communication insures that the secondary FMC is synchronized to the pirmary within 200 msec. of a keypush event.

Each FMC can detect differences between itself and the other FMC with respect to flight plans, performance data, and current aircraft state. If a difference is not resolved via synchronization, the primary FMC announces single FMC operation and the secondary FMC is conditional-failed. Failure of the remaining FMC will not result in loss of both guidance displays.

When synchronization cannot be maintained in flight, the SINGLE FMC OPERATION message will be displayed in the CDU scratchpad. To restore dual operation, move the position of the FMC switch from NORMAL to BOTH ON L - hesitate momentarily, and move to NORMAL. This will result in a memory copy operation from FMC-L to FMC-R. (A movement of the FMC switch in the other direction will result in a memory copy from FMC-R to FMC-L.) If resynchronization is successful, the message DUAL FMC OP RESTORED will be displayed.

ACARS Operation in a Dual FMC Configuration

In a dual FMC installation the primary FMC receives and originates all FMC ACARS messages. The secondary FMC ignores ACARS messages from the ACARS MU. Uplinks received by the primary FMC are transmitted to the secondary FMC via the ISB. Each FMC processes the uplink information independently.

ALIGNMENT CONDITIONS AND INDICATIONS

The IRU has two power sources; one 115 VAC, and the other a 28 VDC. Either is sufficient for operation but in most installations, 28 VDC is a back-up source.

Three types of errors may build up in the IRU.

- 1. Present Position displacement error;
- 2. Velocity errors;
 - a. Ground speed error
 - b. Acceleration error
- 3. Attitude errors (pitch, roll, heading).

Quick alignment re-sets the first two errors (if present position is entered). A full alignment corrects all three errors.

Full alignment of the IRS requires approximately 10 minutes.

NG models when above 60° latitude, it is recommended to leave the mode switch in the ALIGN position for 15 minutes to force the most accurate alignment. Note: only Boeing incorporates the ALIGN position.

Some models incorporate a "variable alignment" mode. With this IRU, the farther from the Equator, the longer the alignment takes. Two minutes at the equator to seventeen minutes at 82°N. Business jets and air transports using the advanced IRS have this feature.

During alignment, the system determines: 1) level attitude based on gravity, 2) true north, 3) aircraft heading and, 4) aircraft latitude based on earth rotation. Present position latitude and longitude must be manually entered during alignment, and becomes the navigation starting point as the IRSs determine subsequent airplane position during flight.

There are no IRS outputs during alignment. In NAV mode, the IRS uses a stored magnetic variation table to generate magnetic heading, magnetic track, etc. After the alignment period, the entered latitude is compared with the IRU computed latitude. A difference exceeding tolerances in latitude sine and cosine will cause the ALIGN annunciator to flash after the ten minute alignment period has elapsed.

Prior to removing power from the airplane, turn the mode selector switch on the MSU to OFF and wait until the ALIGN annunciator extinguishes. Failure to do so will prevent the IRU's from storing the current present postion in nonvolatile memory, and at the next start-up, the ALIGN annunciator will flash when present position is entered. Present position must then be re-entered to stop the ALIGN annunciator from flashing.

When the motion has stoped, the IRS automatically re-starts the alignment. No operator intervention is required.

Magnetic variation between 73° North and 60° South latitudes is stored in each IRS memory. This data is accessed using present position and combines with true heading to determine magnetic heading. If operated outside the latitudes of stored data,the IRS will set magnetic heading to **no** computed data and continue to provide true heading to the EHSIs. Installation of the True Heading Reference switch allows the use of the EFIS and autopilot in these regions.

Because it is important that the IRUs have adequate airflow for cooling, the IRS activates the ground crew call horn if the Equipment Cooling Blower fails (light on overhead) on the ground. This most commonly is caused by loss of AC power. The IRS continues to operate on 28 VDC. On aircraft with Honeywell IRSs, the horn is de-activated after the IRS mode select switch is turned OFF and the ALIGN lights extinguish (30 sec.). The IRS can run for hours on no cooling air; cooling is specified because of possible effect on long term component reliability.

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FMS CONFIGURATION

FMS Certification:

FMS Software is certificated to Level C as defined in RTCA DO-178B, based on a safety analysis of the consequences of incorrect/misleading performance or information from a malfunctioning system and it's detectability. Nowadays, as FMSs are dabbling more and more in performance parameters that can be more critical from a safety standpoint (e.g. computation and dispalyof V-speeds on an EFIS airspeed tape) at least some of the software is required to be developed to Level B.





CRT Color Gun Failure:

Boeing uses CRT displays that have reversion modes when failed or partially failed. Each basic color has its own gun. When there is the loss of a gun (basic color) in the CRT, the whole display would still be intact with all symbols/annunciation present, except the colors will no longer be true. The display unit will revert to monochorme.

If green were lost, the FMA would still be visible to the pilot, except it will no longer be green.

Three types of CDUs may be utilized in many combinations for any given airplane type.

The CDU, the MCDU (multi-function control display unit) and the FANS MCDU (Future Air Navigatioin System CDU).

All three CDUs provide a bisic interface to operte the FMCS, while the MCDU and the FANS MCDU provide a broader rnage interface to both the FMCS and connected sub-systems within the FMS.

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POS INIT

TEMPORARY

TYPES OF ALIGNMENT

This material comes from an article presented by David Hooper at the 1995 FMS User's Conference.

FULL ALIGNMENT (10 min)

OFF - thru ALIGN to NAV (enter POS) A *Full alignment* is recommended for every initialization - time permitting (at least every 18-24 hours) or if the route to be flown is over an area of poor or no radio updating. A *Full alignment* takes approximately 10 minutes.

Item # Description

- 1 Defines a new reference for True North
- 2 Establishes a new starting position to navigate from.
- 3 Sets internal velocities to zero (define)
- 4 Flushes all navaid update bias
- 5 Flushes TOGA FMC Position Update bias
- 6 Establishes a new leveling or vertical reference.
- 7 Performs a self-test of system including operational on DC power.
- 8 Performs the Lat/Lon self tests.

HIGH LATITUDE ALIGNMENT (17 min) *

OFF - stop at ALIGN (enter POS), wait 17 minutes then - NAV Same as a *full alignment* but leaving the mode select switch in ALIGN for 17 minutes gives additional time to measure True North due to the speed of earth's rotation at extreme latitudes.

QUICK ALIGNMENT (30 sec)*

NAV - ALIGN (enter POS) - NAV

A *Quick alignment* is not recommended when departing for a route that offers poor updating. A *Quick alignment* compares the entered Lon to the LAST POS Lon \pm one degree and compares the entered Lat to the LAST POS Lat \pm one-half degree.

- Item # Description
- 2 Establishes a new starting position to navigate from.
- 3 Sets internal velocities to zero.

ABBREVIATED QUICK ALIGNMENT (30 sec)*

NAV - ALIGN - NAV

An *Abbreviated Quick alignment* is accomplished without lat/lon entry. Good when short of time. IRS position is not changed. It starts where it left off.

Item # Description

3 Sets internal velocities to zero.

	N	MALF	UNCTION CODE TABLE (dis	olay se	lector in HDG/STS)		
01	ISDU FAIL	02	IRU FAILURE	03	EXCESSIVE MOTION	04	ALIGN FAULT
05	L DAA FAILURE	06	R DAA FAILURE	07	ADC DATA INVLD	08	ENTER PPOS
)9	ENTER HEADING	10	ISDU POWER LOSS	18	NO ADR DATA	19	IR PROG PIN INVLD
20	ADR FAIL	21	ADR PROG PIN INVLD	22	TAT PROBE SIGNAL FAIL	23	AOA SIGNAL FAIL
24	NO AOA REF SIGNAL	26	NO BARO 3 REF SIGNAL	27	NO PITOT ADM DATA	28	NO STATIC ADM DATA
29	NO BARO 1 DATA	30	NO BARO 2 DATA	31	NO IR DATA	32	PITOT ADM DATA INVLU
33	STATIC ADM DATA INVLD	34	BARO 1 DATA INVLD	35	BARO 2 DATA INVLD	36	BARO 3 SIGNAL FAIL
37	IBU DATA INVI D	38	AIB/GND LOGIC INVLD				





- Wait for both ALIGN annunciators to go
- OFF before moving aircraft.
- If the airplane is moved during alignment, bring the aircraft to a complete stop; position the MSU select switch to OFF (wait 30 sec. for ALIGN
- to go out) and reaccomplish alignment.

Much of this material comes from an article written and presented by Captain David Hooper.

The IRS conducts certain tests on the Lat / Lon coordinates entered during alignment; they are the Latitude and Longitude Comparisons and a Latitude Sine/Cosine Test.

1. Longitude Comparison - Entered Longitude vs: LAST POS Longitude

The IRS conducts a Longitude Comparison immediately after it has been entered. To pass, the entered longitude must not be more than one degree different from the LAST POS longitude.

 Latitude Comparison - Entered Latitude vs. LAST POS Latitude

The entered latitude must be within one degree of the LAST POS latitude.

If either of these comparisons fail, the FMC message ENTER IRS POS will appear and an ALIGN annunciator flashes. Any subsequent entry must also pass or override the comparison. A subsequent entry of correct data passes the comparison test. A subsequent entry of incorrect data identical to that which causes the FMC message to appear overrides the comparison test and causes the flashing ALIGN annunciator to go steady. It is possible to enter a srong longitude, override the warning with a second entry, and suffer severe navigation problems. For this reason, it is recommended to use a nav database starting position such an the ARP or GATE if available rather than manually entering coordinates if operating in DME-DME environment.

A proper entry may fail the *Comparison Test* if a replacement IRS has been installed, though boxes that leave Minneapolis are now nulled out to eliminate this problem.

It is unlikely that an airplane will be moved far enough to a location 1 degree different than the LAST POS; 1 degree latitude change is 60 nm and 1 degree longitude will be 60 nm x $\cos(lat)$. 2. Sine / Cosine Latitude Test At the end of alignment, the entered latitude

must pass a *sine/cosine comparison test*.

If the entered latitude passes the *sine/cosine comparison test*, alignment is completed.

A flashing ALIGN annunciator at the end of alignment indicates that the entered latitude has failed a *sine/cosine comparison test*, and that entry into the NAV mode is inhibited. Additional latitude entries are still allowed until the test passes; however, new latitude entries must also pass the *comparison test*. If two consecutive, identical latitudes are entered and the *sine/cosine comparison test* fails, the flashing ALIGN annunciator goes steady and the FAULT annunciator illuminates.

One correct latitude entry passes the *comparison test* and turns the warning annunciator OFF. If the mode select switch is set to ALIGN, the ALIGN annunciator remains illuminated. If the mode select switch is set to NAV, the ALIGN annunciator goes out, and the IRS enters the NAV mode if the 10 minute align mode is complete.

If the pilot has not entered latitude and longitude by the end of the alignment, the ALIGN annunciator flashes, and the IRS inhibits entry into the NAV mode until data is received.

CAUTION In the case where two airports are close together with similar ICAO identifiers, take great care in entry of the REF AIRPORT. Example: Santa Ana (Orange County, California) is 66 nm northwest of San Diego. **KSNA** N33°40.5 W117°52.1 N32°44.0 W117°11.4 KSAN Anytime you get a message during alignment, don't "blow" it off. It's a wake up call. The IRS will accept this wrong position if entered a second time. If you're flying a non-EFIS airplane, the

round dial HSI will not supply any hints of a bad position. If you're flying an EFIS airplane and have the habit of always entering the runway or some point around the airport to help with situational awareness, you will notice it is not in the viewable area of the EHSI Map. You may get a second chance when the RTE entry doesn't match the IRS position.

Astronauts and Engineers: Sine / Cosine Comparison Test

Just prior to entering the NAV mode, the sine of the computed latitude is compared to the sine of the entered latitude and must agree within \pm .15 and. The cosine of the computed latitude is compared to the cosine of the entered latitude and must agree within \pm .012.

CREATED (FIXED) WAYPOINTS

To explain Created waypoints, we'll use part of a route heading east from Los Angeles. Eastbound on J 169 and approaching Thermal, ATC says, "Junkers 13, after Thermal proceed to Momar intersection, then direct Blythe, as filed".

You type MOMAR into the scratch pad, Line Select Key (LSK) 2L of the LEGS page, (behind Thermal) and the message NOT IN DATA BASE appears. You need to create a waypoint!

Created waypoints can be defined on the REF NAV DATA page or on the RTE or LEGS pages. Both methods have advantages and disadvantages. Both methods store in the Temporary nav data base. Using the RTE or LEGS pages is the quickest.

On the RTE or RTE LEGS pages, created waypoints (max-20) can be keyed into the scratch pad by any of the following four ways (4th is on the next page).



Also known as the Along Track Offset

- It is a pilot defined point at a given distance before or after an existing flight plan wpt on the existing flight plan course.
- This example uses the same example found in the Downtrack Fix procedure, except that the arc is gone because the Along Track Offset **must use a waypoint in the flight plan.**
- The distance specified must be within the distance to the preceding or next wpt.
- A Conditional wpt may not exist at either end.
- Entries not meeting these criteria result in the INVALID ENTRY message.
- Ref: Advanced Techniques.

Situation: You are proceeding east at FL 370 direct to College Station for the CUGAR 4 arrival. 90 nm west of CLL, ATC : "Northrop Gamma, cross 10 east of College Station at and maintain FL180".



NOTES:

- If the created wpt was to have been on your side of the wpt, you would have used a minus (-) sign.
- Positive values are assumed by the FMC and "+" signs need not be entered.
- There can be no wpts between the reference (host) wpt and the position of the Along Route Wpt. In this case, entries exceeding "-90" or "+23" would result in an INVALID ENTRY message.

May 98

HEADING VS TRACK

This material is under development, but important enough that I though it should be included in it's orginal form. Thanks to Captain Andre Berger for researching this topic.

When a flight segment is labeled "hdg", or when a textual description of a published route (SID, STAR, ...) reads to turn to a published "heading", do you have to correct for wind (1)?

ICAO (2): SID: Yes. STAR: Yes. Enroute: Your choice: yes or no.

FAA:

SID: No, must not! STAR: No (but you are allowed to correct for wind if RNAV equipped) Enroute: Your choice: yes or no

(1) When ATC instructs you to fly a heading (e.g. runway heading, radar heading) you must not correct for wind.

(2) See Pans-Ops 8168. Not all ICAO states follow these rules exactly, minor variations exist.

Note on Jeppesen charts: if the radar vector symbol is printed on the chart, you must not correct for wind.

FMS heading legs:

The leg can be a track or a heading leg depending the coding done by the NAV database supplier (Jeppesen, Racal, Swiss Air ...). The supplier of the database delivers what is requested by the customer. Most legs outside the USA are coded as track.

.....

One of the important things to understand is that Jeppesen accurately produces a standard graphic format of government source information for every country in the world. They will not change the label of "hdg" to "track" until the procedure designer who is responsible for the SID and STAR makes a change to the label on the procedure that he/she designed.

This is important because the person who designed the SID or STAR procedure coordinated the intent with air traffic control. Even though PansOps has revisions, not all countries apply the new specifications at the same time. If the chart says "heading", there is the likelyhood that the controller in that country expects the pilot to fly a heading - not a track.

When Jeppesen receives a revision from the government source that changes the label of "hdg" to "track", Jeppesen does the same.



ARINC 424 PATH TERMINATORS

- AF DME arc to a fix
- CA Course to an altitude
- CD Course to a distance
- CF Course to a fix
- CI Course to an intercept
- CR Course to intercept a radial
- DF Direct to a fix
- FA Course from a fix to an altitude
- FC Course from a fix to a distance
- FD Course from a fix to a DME distance
- FM Course from a fix to a manual termination
- HA Terminate hold automatically at altitude and fix

- HF Terminate hold automatically at fix after one circuit
- HM Terminate hold manually
- IF Initial fix
- PI Procuedure turn
- RF Arc to a fix
- TF Track between two fixes
- VA Heading to an altitude
- VD Heading to a distance
- VI Heading to intercept next leg
- VM Heading to manual termination
- VR Heading to intercept a radial

CONDITIONAL WAYPOINTS



In addition to the types of waypoints discussed so far, (Fixed and Floating), the system implementation takes into account in its profile predictions, the existence of points of importance to the vertical performance calculations called Phantom waypoints. These points are like floating waypoints in that they occupy positions dependent upon the aircraft operating state and external variables such as wind. Phantom waypoints influence the system only by their "presence" being accounted for in time and distance predictions.

Phantom waypoints	Displayed on Map	Phantom waypoints	Displayed on Map
SPD RESTR on CLB pg	No	SPD RESTR on DES pg	Yes (decel pts)
Crossover CAS-M on clb	No	Crossover M - CAS on des	No
T/C	Yes	T/D	Yes
E/D	Yes	Tropopause breakpoint (U10.5	5) No
		100 12° 4.0 to	

CONDITIONAL WAYPOINTS (Continued)



Defines a heading leg (LAS280) terminated when crossing the 280° R from LAS VOR. If only 2 letters make up Remember: the ID, the third character 3 digits means will be a dash. a radial.

Conditional wpt



Defines a heading leg terminated when reaching 4 nm from the LAS VOR. If only 2 letters make up the ID, the third character will be a dash.

Offset.

FMC created wpt

	A computer created wpt located 5
SEA-05	nm from the stored reference wpt of SEA. The DME portion of this
	convention is sometimes violated.

Database supplier wpt

TNV21 D194A F096M	A Jeppesen data base entered wpt.
-------------------------	-----------------------------------

WAYPOINTS

WAYPOINT BYPASS

The flight plan may occasionally contain waypoints connected by a leg of short length and a significant change in direction. This would most likely occur as part of a departure procedure. The *predictions* algorithms of the 737 FMCs prior to U10 use 210 kts as the starting point for climb predictions. That means that all turns are predicted at a minimum of 210 kts. There is then a canned acceleration assumption built into the FMC.

If FMC computations determine that normal turn construction between legs cannot provide a continuous path (combinations of airspeed, short leg length, and a significant change in direction), the FMC will bypass the affected leg (DEF in this example) and use an alternate turn construction to intercept the leg going to the subsequent waypoint. On the CDU, the word BYPASS appears above the speed and altitude for the waypoint.

When the active waypoint is bypassed, the waypoint remains active until passing abeam. For non-EFIS aircraft, with the HSI switch in NAV, the course pointer points to the next leg direction, while the waypoint bearing pointer continues to point to the active waypoint.

May 01

If elimination of the bypass is desired, consider entering a speed restriction at a wpt prior to the BYPASS. 210 kts is the lowest speed U8 and lower will allow. U10 is changed to allow entries (targe speed, SPDREST, and wpt speed restrictions) as low as 100 kts. The slowest speed that predictions will actually use is Vref (40) + 20.

DELeting one of the waypoints, or proceeding DIRECT TO or INTC LEG TO a downpath waypoint will also solve the problem.

Any mandatory altitude-crossing restriction for the BYPASS waypoint is still observed, based on passing abeam the waypoint.

Prior to U10, if a double BYPASS condition occurs (bypass of two consecutive legs), then a DISCO is inserted just prior to the first by-passed waypoint, DEF in the example. U10 will by-pass three consecutive wpts before a disco is inserted.



NOTE: ABC is not a *Flyover* waypoint. *Flyover* transitions require the aircraft to pass directly over the waypoint's geographic position. In general, they occur most often in terminal area procedures (SIDS/STARS), and are rarely encountered in the enroute phase.

WAYPOINTS

FLY-OVER WPT vs FLY-BY WPT

Pilot defined wpts will be *fly-by* wpts.

Dec 02

If a wpt must be flown over, such as D5 SEA in the example below, some adjustment in the definition may be required to meet the clearance.

Note: ICAO charting convention for a *fly-over* wpt is a circle around the fix. Boeing does not presently support this convention.

Example: In the ELMAA 7 Departure from Seattle, Washington, ATC wants you to *fly-over* a point 5 nm south of the SEA VOR on the 158° radial; then, a 92° turn to 250° is required.

Database defined wpts can be coded to either fly-over or fly-by a point. In this case, the departure is in the database and D5 SEA is coded as a fly-over wpt.

The default is fly-by if this attribute is not specified by FAA or other AIS because it results in a shorter flight path that is more economical to fly.

If the pilot defines this wpt using the the PBD formula SEA158/5 the airplane will turn prior to crossing the 5 DME wpt. This can be checked prior to takeoff by viewing the route in the PLAN mode. You can see that the wpt is not going to be crossed.

One work-around is to create the wpt a \checkmark mile or two further south. The angle of the turn will dictate the size of the adjustment.



On the A320, fly-over waypoints appear with a small triangle symbol on the MCDU, so you know that wpt is different than a fly-by waypoint! "C'est automatique!" Also, there's a triangle key on the MCDU keyboard that may be used to "force" the airplane to fly-over a wpt (if needed) to comply with an ATC clearance. - G. Bleyle





DENTIFIERS

IDENTIFIERS

The following is provided as background information to improve your understanding of waypoint identifiers used by the FMC. Some of the information only applies to a few areas of the world.

Coded waypoints by Jeppesen (lat/long entries) actually are measured to 100th of a second which is about 1 ft. Consider the coded gate position of N2120<u>12.06</u> W15755<u>30.18</u>.

The FMC displays these coordinates as N2120.2 W15755.5; an accuracy of 1/10th of a minute. (To convert, divide the $\dots \underline{12.06}$ and the $\dots \underline{30.18}$ by 60.) If you were to manually build a lat/lon wpt, the closest you can get is to the nearest tenth of a minute, which is about 600 ft.

Standard rules for naming waypoints (except for the SEA-05 format) are defined in the ARINC Specification 424-8 and used industry wide. Computerized nav system software limits wpt names to a maximum of five characters that are assigned according to the following rules.

 $\begin{array}{c} N \underline{21} \underline{20} \cdot \underline{2} \\ \text{degrees} \underline{-1} & | & - \\ \text{minutes} \end{array}$

APPROACH MARKER IDENTIFICATION

UN-NAMED TERMINAL AREA FIX, or BEARING DISTANCE WAYPOINT (formerly DME ARC WAYPOINT)

, MUSEL D	eparture - SN	A
ACT RTE	LEGS 1/4	
195°	2 NM	
(D194A)	/500A	
1832	11 NM	
MUSEL	/	



- TECHNIQUE -

Use the keyboard as an aid to convert letters to miles. Each row has 5 keys. See how easily \mathbf{R} is determined to be the 18th letter/mile.

Α	В	С	D	E
F	G	н	1	J
К	L	М	Ν	0
Р	Q	R	S	Т
U	V	W	X	Y
Ζ				

If the approach marker is named, the NDB ident now normally used. (Check with your database provider.) If it is unnamed and not an NDB, the letters OM followed by the rwy number are used.

This form of wpt naming is very common on SIDS, STARS, arc approaches, and FMS data base departures and arrivals. Jeppesen inserts a "**D**" as the first character - or an "**F**" if part of an FMS database procedure. In the case of the "**D**" format, characters 2 through 4 signify the bearing from a navaid on which the wpt lies; there are no rules as to which navaid. Consult the applicable chart to determine the origin of the bearing. In the "**F**" format, characters 2 through 4 are the bearing from the Airport Reference Point. The last character is the DME arc radius defining the position of the wpt on the radial. This arc radius is expressed as the equivalent letter of the alphabet, i.e., A=1 nm. B=2 nm. C=3 nm. D=4 nm, and so on. If the wpt includes a fraction of a mile, the letter is rounded up.

Example: ISNA194/1 = D194A

This convention takes more time to manually construct if not in the database, but is much easier to follow on the CDU than using the Place-Bearing/Distance method.

An unnamed wpt along a DME arc with a radius greater than 26 miles is identified as an unnamed turn point that is not coincidental with a named wpt.

A couple of examples are:

CPR338°/29 becomes CPR29 GEG079°/30 becomes GEG30

When there are multiple un-named wpts along a DME arc with a radius greater than 26 nm, the station identifier is reduced to two characters, followed by the radius, and then a sequence character. Examples are:

CPR134/29 becomes CP29A CPR190/29 becomes CP29B

May 01

CONDITIONAL WAYPOINTS

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IDENTIFIERS

COORDINATES



Examples:

N Lat W Long N46W050 coded as 4650N N Lat E Long N50E020 coded as 5020E

S Lat E Long S5 S Lat W Long S5

S50E020 coded as 5020S / S52W075 coded as 5275W

N Lat W Long N N Lat E Long N S Lat W Long S S Lat E Long S

N37/W125 coded as 37N25 N06/E110 coded as 06E10 S20/W125 coded as 20W25 S06/E110 coded as 06S10

COMPUTER CREATED WAYPOINTS

CCR	/	
20°	24NM	
ISYOH	/	-
354°	5.0NM	
ISY-05 -	/	
354°	10NM	
ELKOE	/ v od	

DUPLICATE IDENTIFIERS

COMPUTER NAV FIX (CNF)



Database contained Entry/Exit positions to Oceanic Control Areas are often defined by wpts which are "undesignated", made available as geographical coordinates expressed in full degrees.

The four digits include two for latitude and two for longitude. The first two digits of the ID are the degrees of latitude. The third and fourth digits of the ID are the second and third lon digits. The first lon digit does not appear in the ID.

Positions in the northern hemisphere use the letters "N" and "E"; the southern hemisphere use the letters "S" and "W".

The letter "N" is used for north latitude and west longitude. The letter "E" is used for north latitude and east longitude.

The letter "S" is used for south latitude and east longitude. The letter "W" is used for south latitude and west longitude.

Placement of the letter in the five character set indicates what the first digit of longitude is published as.

The letter is the last character if the *longitude is less than* 100° (above example).

The letter is the third character if the *longitude is 100°* or greater.

Occasionally a waypoint will exist that has not been assigned a name. The FMC recognizes the need for a *path* and *terminator*, and assigns a name. Since it is 6 characters, the pilot is unable to check its location in the nav database WPT IDENT.

Should application of these rules result in more than one wpt having the same identifier, the SELECT DE-SIRED WPT page appears. This page lists the wpts with the same name, along with information such as the lat/ lon, type of facility, frequency, etc.

Formerly unnamed positions on airways and terminal procedures in the US will be provided with 5-letter Computer Navigation Fix (CNF) names. Initally CNFs will be designated at unnamed airspace fixes or mileage break points on airways and routes that currently display an "x". Jepp charts currently have navdata identifiers consisting of 5 character alphanumeric names in brackets at these same positions.

CNFs are for reference to nav systems using navdate bases only. CNFs do not have any air traffic contro. functions. (ATC will not request that you hold at, report at, or otherwise use a CNF.) Do not request routing using a CNF either direct to ATC or in a flight plan. The new CNF names are depicted near the "x" in an italic type. Forexample, *JOSSY* identifies the intersection of J16 and J29 near Albany, NY.

IDENTIFIERS

FIR, UIR, CONTROLLED AIRSPACE

ACT RTE	LEGS	1/3
135°	7 NM	
BAROW		262/FL350
136°	24 NM	
OLINS		262/FL350
137°	159 NM	
NULEY		262/FL350
1380	11 NM	
FIR19)		mark of the
138°	59 NM	
ALARD		262/FL350

NAMED WAYPOINTS

National Flight Data Center is responsible for naming waypoints.

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For an FIR, FIR plus a numeric from 02 to 99 is used.

ATZ for Aerodrome Traffic Zone

CTA for Control Area

CTR for Control Zone

FIR for Flight Information Region [FIR19] on Jeppesen chart.

TIZ for Traffic Information Zone

TMA for Terminal Control Area

UIR for Upper Flight Information Region

One Word Names

Full name is used if five or less characters are involved.

Example: LOGAN

More than 5 letters:

Eliminate double letters.

Example: KIMMEL becomes KIMEL

Keep the first letter, first vowel, and last letter.

Drop other vowels starting from right to left.

Example: BURWELL becomes BURWL

Drop consonants, starting from right to left.

Example: ANDREWS becomes ANDRS

BRIDGEPORT becomes BRIDT

Multiple Word Names

Use first letter of the first word and abbreviate the last word using the above rules sequentially until a total of five characters remain.

Example: CLEAR LAKE becomes CLAKE Phonetic Letter Names

When an ICAO phonetic alpha character is used as a wpt name (Alpha, Bravo, Charlie, etc) the rules above are used.

Example: November becomes NOVMR.

When a double phonetic such as Tango India is used as the wpt name, use the rules established above under multiple word names.

When a phonetic alpha character followed by a numeric and/or other alpha characters (A1, A1N, B2, etc.) is used as the wpt name, it will appear the same in the database as shown on charts.

Dec 94
IDENTIFIERS

NON DIRECTONAL BEACONS (Marker beacons)

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PILOT DETERMINED WAYPOINTS

TERMINAL WAYPOINTS (Procedure Fix Wpts)

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At Jeppesen, most NDBs are identified by the use of the station identifier and loaded in the NDB navaid file. Example: Galveston NDB is GLS. Until recently, where more than one NDB navaid with the same identifier existed, only one was placed in the NDB navaid file; the other was placed in the wpt file - meaning it could only be accessed by its full name.

The suffix **NB** is used only for carriers wanting the NDB to go into the wpt file.

Entry into the NAVAID entry of the REF NAV DATA to obtain the frequency is impossible.

NDBs are packed as waypoints and do not show up on the EFIS Map when the NAVAID button is pressed. For the IL96 FMC, the pilot can manually tune them through the FMC (type in the frequency into the MCDU NAV RADIO page) and the FMC will automatically Route tune them.

Place bearing/distance. Place bearing/place bearing. Lat/Lon. Along Track (Route) Offset.

These rules are used in developing identifiers for wpts used soley in terminal area procedures. Such wpt identifiers will be unique only for the airport specified. A wpt identifier used in a terminal area cannot be repeated in that terminal area but can be used in an enroute area encompassed by the same geographical area code.

Runway Related - Single Approach Procedure for given runway.

The following 2-letter prefixes are added to the relevant runway number to make up an identifier when no named wpt has been established by the government source for the fix type.

A- (+ an alpha) step down fix.

BMxx is a back course marker.

CFxx is a final approach course fix wpt. Such waypoints are contained in certain ILS procedures to ensure alignment on the final approach course. They are located approximately 9 nm prior to glideslope intercept. Example 17L at old DEN below.



All Day Art in any March of Log and a Republic strategy of the solution of the

Runway Related - (Continued)

- FA--xx is a VFR final approach fix. Discontinued after U4.0. Six characters, it identifies the computed final approach waypoint for a runway. Such wpts are inserted when a runway is chosen from the ARRIVALS page. The wpt is located 8 nm from the runway threshold on the extended runway centerline. Wpt altitude usually must be specified by crew entry. If an altitude has been assigned, the path has been constructed beginning at a point 50' above the runway threshold extending upward to a point above FA--xx.
- FFxx is a final approach fix of an ARRIVAL procedure.
- GS-xx identifies the computed glideslope intercept point for an ILS approach. This wpt is generated by the FMC, and in software up to U6 is the end-of-descent point for a VNAV descent. If left in, will cause VNAV to disconnect in all software, but in U7.1 and up, can be re-engaged. Usually advisable to delete this wpt.

IFxx is an intermediate approach fix.

IMxx is an inner marker.

MMxx is a middle marker.

- MAxx is a missed approach point other than the runway.
- MA24B is a missed approach point on the nonprecision approach to RW24.
- MDxx is the minimum descent altitude.

OMxx is an outer marker.

RWxx is the runway threshold.

- RC-xxx U7 & up: is a computer generated (floating) rwy centerline intercept wpt.
- RX-xx U5.0 & up: runway extension. Distance from the runway can be entered up to 25 nm. Computer generated. Access the RWY EXT after choosing a RWY from the ARRIVALS page.

SDxx is a step-down fix.

TDxx is the touchdown point inboard of the threshold.

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inway	Related	- Multiple	Approach	Procedure for	
san	ne runwa	iv.			

2-letter prefix may change to allow different identifiers for the same wpt. The first letter identifies the type of fix and the second letter identifies the type approach.

Clxx is the initial approach course fix on the localizer in an ILS approach. (Jepp wpt) Usually 2 nm or more from the FAF.

CVxx is the final approach course fix in a VOR approach.

DVxx is the minimum descent altitude in a VOR approach.

FVxx is the final approach fix in a VOR approach. IVxx is the initial approach point in a VOR approach.

PVxx is the missed approach point in a VOR approach.

If the un-named turn point, intersection or bearing/ distance is co-located with a named waypoint or navaid on a different route structure (e.g. low level or approach), the name or identifier of the co-located waypoint is used.

Jeppesen constructs identifier codes for un-named turn points that are not coincidental with named waypoints by taking the identifier code of the reference navaid for the turn point (expected to be the nearest serving the airway structure) and the distance from this navaid to the turn point. If the distance is 99 nm or less, the navaid identifier is placed first, followed by the distance. If the distance is 100 nm or more, the last two digits only are used and placed ahead of the navaid identifier.

$\overline{\ }$	NAVAID	DISTANCE	CODE
	TNV	21	TNV21
	LEV	174	74LEV

Waypoints located at any of the types of facilities on the left will take on the official identifier of the facility in question.

MENU - U10 and up

You get to this page by:

- Press (MENU) key.

 Allows selection of system for which the MCDU will be active in providing the control / display function.

- Line select system to be made active.
- HOLD line sleected (LSK 6L) to suspend control of active system.
- _ LOGOFF line selected (LSK 6L) to terminate control of an active system.
- _ Note: HOLD and LOGOFF are operational for a any system except the FMC.

	MENU	te e en ennañ. Guides van 211	
\square) <fmc <act=""></fmc>		OP right LT and app
\square) <acars <hld=""></acars>		
	J <dfdmu< th=""><th></th><th>Returns to the</th></dfdmu<>		Returns to the
	in an iter in an		last FMC CDU
	- 1012H - 1012H		page displayed.
	GPS NAV	HOLD>	
ATT: THRE	<u> </u>		Logs off and stays
		LUGUFF>	on the MENU page.
	THE JEF HOMOSPHERE		-e Vana 1936 - Militer Militer (Militer Angel 1930)

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 UniorI.qued au germani 6602

*GPS NAV prompt allows access to IRS LEGS, IRS PROGRESS, and IRS WPT DATA. ANCDU required that is receiving valid IRS data.

INIT / REF INDEX

		Way 50
You get to this page by:		
 Press (NT) REF key. If on the ground and prior to alignment, If on the ground after alignment, PERF After takeoff, information on page 101 a INDEX prompt (LSK6L) of displayed p The FMC will determine which page to dis INIT REF key is pressed. 	, POS INIT page appears. INIT page appears. applies. page. splay (based on preflight status, flight phase, etc.) when	n the
NO	REQUIRED ENTRIES)[].] (4 ⁰ _
INIT/REF INDEX page provides access to:		
IDENT POS INIT PERF INIT TAKEOFF REF APPROACH REF OFFSET (U7 and up)	NAV DATA (SUPP - U4 and up) MSG RECALL (U6, 8, and 10) ALT DEST (U6, 8, and 10) ACARS (U6, 8, and 10) IRS NAV (-300/400/500 with ANCDU) * SEL CONFIG (-600/700/800) MAINT (on ground)	
ON GROUND: -300/400/500 INIT / REF INDEX 1/1 < IDENT NAV DATA > < POS MSG RECALL > < PERF ALT DEST > < TAKEOFF ACARS > < APPROACH IRS NAV > < OFFSET MAINT >	ON GROUND: -600/700/800 INIT / REF INDEX 1/1 < IDENT NAV DATA > < POS MSG RECALL > < PERF ALT DEST > < TAKEOFF ACARS > < APPROACH SEL CONFIG> < OFFSET MAINT >	
IN THE AIR: -600/700/800 INIT REF / INDEX 1/1 < IDENT NAV DATA > < POS MSG RECALL > < PERF ALT DEST > < TAKEOFF ACARS > < APPROACH < OFFSET NAV STATUS>	 Maintenance Built-In-Test (BIT). Displayed on ground only. Provides the major test interface for the automatic flight guidance and control system aboard the a/c. Maintenance pages are proved for recording the inflight history of the system with which the FMCS interfaces. This record is maintained in the FMC NVRAM. The data collected and held for the failure incidents of past nine flights plus current internal on-group faults. (A "flight" is defined as the period between squat switch and greater than 20 kts.) The FMCS records the reason and time of the failure, and the unit in which the failure water 	ns ided ems rding ta is of the ound ts

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The FMC needs continuous electrical power to operate. When electrical power is interrupted for *less than 10 seconds:*

- LNAV and VNAV disengage
- all entered data is retained by the FMC
- the FMC resumes normal operation when power is restored.

If power is lost for 10 seconds or more on the ground, all preflight procedures and entries must be done again when power is restored. If power is lost for more than 10 seconds in flight: • LNAV and VNAV disengage

• all entered data is retained by the FMC, and when power is restored the MOD RTE LEGS page is displayed with the scratchpad mesage SELECT ACTIVE WPT/LEG.

Astronauts and Engineers: Nav Database Management

When maintenance inserts a disc to change the Nav database, the old database is not actually removed. Certain data is "de-selected" and new data is inserted. Of course the sum of the old data and new data cannot exceed the card's capacity. For example, the practical limit of a 96k card is 94k. Some free space is required because the amount of new data is limited by the available free space.

DATABASE CROSSLOAD

You get to this page by:

- DATABASE CROSSLOAD page is displayed upon power-up if the nav data is different.







• SET IRS POS and box prompts are displayed when either IRS is in ALIGN mode and IRS present position has not been entered (on ground).

NAV, ATT, or OFF.

• SET IRS POS header and data clear when IRS is in



POS INIT

ATTITUDE (Not a normal mode)

When an IRS enters the ATT mode, ATT and HDG flags appear. The ALIGN light illuminates steady. After approximately 30 seconds, the light extinguishes and the ATT flag retracts from view. In the ILS and VOR modes, the HDG flags remain in view, and in the Map and Plan modes, the doghouse (heading pointer) is not displayed, until magnetic heading has been manually entered into the IRU. Since all navigation parameters are lost for the system in ATT, the ISDU displays are blank when either PPOS, WIND, or TK/GS displays are selected. (Position and ground speed information is lost.)

- This is a reversionary attitude mode to provide aircraft attitude and heading information after loss of AC power or certain IRS failures.
- Selectable on ground or in air.
- This "DG" type heading reference precesses (drifts). Therefore, new compass headings must be entered manually whenever compass card indications are unacceptable (up to 15°/hr).
- Try this as a demonstration so you'll be comfortable should you ever experience this type of failure. I'd recommend a "good weather day" and only with the IRU in front of the PNF.





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Dec 02

POS REF

- Data lines will be blank if the IRS (s) are not in the NAV mode.
- Current FMC System POSition and ground speed requires that at least one IRS be in the NAV mode, otherwise line 1 will be blank.



Astronauts and engineers: RAIM Prediction

RAIM (Receiver Autonomous Integrity Monitoring) prediction checks the availability of satellite coverage at the destination (5° above the horizon) at the predicted time of arrival. RAIM prediction can be done prior to departure or enroute. Systems such as the Universal FMS knows the precession of the GPS satellite constellation and computes the number of satellites that will be available overhead the destination at +/- 15, 10, 5 and 0 minutes. Local terrain can block satellite signals near the airport; RAIM predictions generally do not consider this problem nor does RAIM know if a satellite is out of service. RAIM can be accomplished when at least 5 signals are received and Fault Detection can be accomplished when at least 6 signals are received. The RAIM and RNP/ANP concepts are quite different and one cannot cover for the other. RAIM is a predictive concept that assesses the future integrity state (not accuracy) of the GPS navigation. RNP/ANP is a real time concept that uses sensor performance characteristics to assess the current accuracy (not integrity) of the state of the navigation. There is no RAIM prediction in the Boeing system and is unnecessary due to the ability to "coast" inertially if GPS signals are lost

temporarily. The Boeing system monitors the GPS and decides how good the ANP can get. All the pilot has to do is monitor ANP.

You get to this page by:

- POS INIT 1/3 go to previous page
- POS REF 2/3 go to next page.
- (U7.0 and up) NAV STATUS page POS SHIFT prompt (6R).

Displays the position differences of each sensor (IRUs, GPS, RADIO) relative to the FMC POSition. A dual configuration includes the left and right FMC positions on line one.

POS SHIFT allows the FMC POSition to be moved to any of the displayed positions by line selection and EXEC.

It is useful to make the POS SHIFT when you are having trouble getting an update and you think an IRS position is more accurate than the FMC POSition. A badly performing radio navaid can corrupt the FMC POSition such that subsequent valid navaid position reports are considered out-oftolerance and are ignored. The old Circular Error of Probability (CEP) which determined what updates were used, is opened up. If an update from two DME stations falls outside the error allowed by the CEP, which is just a little larger than the ANP, the FMC will not use that update. Opening the CEP will let the updates in to correct the position. The VERIFY POSITION message or IRSNAV ONLY in a region of normally good radio coverage, typically would be the first alert that the FMC POSition and some other sensor are in substantial disagreement. Use this page to evaluate the situation.

The nav filter is cleared and Ten Best List is rebuilt Relative Position lines (1-3L and 1-4R) display bearing and range from FMCS position to each available sensor.

Line selection arms the function to shift the FMC POSition to the selected position: highlights and freezes the selected position and illuminates the EXECute key.

EXECution shifts the FMC to the selected position and an UPDATE COMPLETE annunciation appears. Page change clears this message.

If an IRS position is selected, the FMC will use that IRS for reference until changed again or it is determined to be unreasonable.



May 01

POS SHIFT

POSITION SHIFT EXERCISE

The following exercise is helpful in understanding how the POS SHIFT feature works and how GPS and radio updating affects FMC position. Accomplish this exercise only when work load is low. Note for non-EFIS pilots: When the term *magenta line* is used, it is the same thing as the *course bar* when the HSI switch is in NAV.

- 1. Select the smallest range on the EFIS CP. Notice the magenta line (active route) is centered on the aircraft symbol.
- 2. Locate the POS SHIFT page. INDEX / POS / PREV PAGE
- Each sensor's position relative to the FMC position(s) is displayed in bearing and distance from FMC position. In the CDU below, IRS-L is .9 nm on a bearing of 068° from the FMC (off the right wing tip). IRS-R is 1.1 nm on a bearing of 129° (off the tail).

Use your center map or RDMI to help visualize this. The following lesson is best demonstrated when the sensor to be shifted to is off a wing tip.

Normally, the FMC POSition is a GPS updated position, not an IRU position. This *updated* position is more accurate than an IRU position.



- Select the sensor that you believe is most accurate by pressing the adjacent prompt Example: Select the left IRS by pressing LSK 3L. This arms the position shift. An armed shift state may be cancelled by pressing the CANCEL > prompt at 6R.
- Press EXECute. The FMC POSition shifts to the sensor position you selected.
- If in LNAV, The aircraft will turn to the left to get back on the magenta line.
- If in an updating environment, the FMCS will slowly go back to the GPS or RADIO position.

- 5. To keep the aircraft flying straight, line up the heading bug and press HDG SEL. This will stop the airplane from turning because the next two steps are going to reposition the FMC.
- Press the LSK adjacent to the left IRSs. Notice you could press CANCEL to back out of this.
- Press EXECute. Check the EFIS display. The FMC POSition has shifted to the selected IRS. Can you figure out why the magenta route appears off to one side?
- 9. The FMC will start updating right away because the GPS and/or DME systems are operating. Can you tell what stations the FMC is tuning? (NAV STATUS). Because the FMC POSition is biased to the sensor's position, it immediately starts to shift from the referenced IRS position to the position being calculated by those sensors. The magenta line will move back to where it was previously.
- 10. After the XTK ERR indicates approximately .2 nm or less, re-engage LNAV.

If all updating fails and the FMC position becomes unuseable (i.e., serious map shift), this is how you shift the FMC POSition to one of the IRSs.

Note: It is normal for the FMS POSition(s) and the positions of the various sensors to be slightly different. However, significant differences in position can be a clue to FMS nav error. For example, if the FMS-to-IRS position vector is significant and the same for *both* IRSs, it is quite possible the FMS has a position error. Why? Because it is usually unlikely that *both* IRSs will have significant drift in the same direction.



Dec 02

May 98

PUBS SUM

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ROUTE DISCONTINUITY

If the entered route does not form a continuous path of linked legs (TO entries) a ROUTE DISCONTINUITY will be inserted. A ROUTE DISCONTINUITY will also be inserted if the end of a leg is indeterminate due to impossible geometry of the path (too tight a turn and / or too high an airspeed), or when an added waypoint is not part of the existing active flight plan.

There are times when a ROUTE DISCONTINUITY is advantageous, such as reaching the end of an ATC clearance, or when manuevering around the terminal area with the runway at the top of the LEGS page, the runway may drop out! Insert a DISCO; then when on the maneuvering side of the runway, accomplish a DIRECT TO or INTERCEPT LEG TO the runway.

An occasional discontinuity may occur in a procedure (DP, STAR or approach), due to the methods used for coding the database.

This example depicts a route entry where the waypoint identifier (CUGAR) is not linked with CUGO1.

1	ACT RTE LEGS 1/2	din 1
)	81° 60 NM CLL .795 / FL330	
)	128° 3.4 NM CUG01 310 / FL180	
)		
)	CUGAR	
2	127° 11 NM HOAGI 250/10000	
וכ	RNP / ACTUAL 1.00/0.14 NM RTE DATA>	
		il er

Dec 02

A path descent is not available for a point beyond a ROUTE DISCONTINUITY.

ETA and estimated fuel calculations assume direct flight across the route discontinuity. If LNAV is allowed to fly into a ROUTE DISCONTINUITY, the AFDS will disengage to CWS (maintains heading).

A ROUTE DISCONTINUITY can also be caused by adverse wind effects on a conditional waypoint, as shown below. If normal procedures for correcting the discontinuity are unsatisfactory, consider DELeting the wpt or proceeding DIRECT TO or INTERCEPT LEG TO a downpath wpt.

This example could occur if you selected a SID and runway with conditional waypoints.



ROUTE OFFSET - U7.1 and up

You get to this page by: (not available for electrical-mechanical instrumented aircraft)

- RTE page OFFSET prompt (LSK 6R) when airborne (On ground, TAKEOFF> is displayed).
- INIT REF INDEX page OFFSET prompt (LSK 6L).
- Used to establish a parallel lateral path offset left or right of the active flight plan.
- An offset can be activated for the present leg or pre-planned to start and end on a downstream leg.
 The following legs are not valid for an offset: end of flight plan wpt, a DISCO, start of a published approach transition, an approach procedure, a data base DME arc, a heading leg, a holding pattern (except PPOS), CF leg with course change greater than 2°, non TF leg or FD/FC leg with course change greater than 135°, and a pre-planned termination wpt.
 An offset can be built while on the ground by accessing <OFFSET prompt from the INIT REF INDEX.



Dec 02





DEPARTURES



Since inertial systems accumulate position erplayed on the ground is slowly accumulating errors. In other words, as soon as the IRUs reach NAV (lights out), they start to drift slightly. Error rate history (last flight) can be checked on the IRS MONITOR page. It is common to see less than .5 nm/ hr. drift.

FMC System position follows the Referenced IRS), a significant error can build up after a long taxi. For example, being number 10 in line waiting for the Santa Ana, Ca. airport to open early in the morning produces a larger drift than taxiing immediately to the runway.

On the second occasion LNAV may identify the rors as a function of time, the position being dis- fix D194A just fine (one mile from the departure end of runway 19R). With a long taxi, it will probably be off, since the computer needs a minute or two to update its position after takeoff (assuming a good area of nav coverage).

A quick alignment with gate entry just prior to engine start will help. Yes, you're right. If your Since no updating occurs on the ground (the software allows Runway Position Update at TOGA, this discussion is irrelevant.

> LNAV accuracy is not guaranteed without updating. This presents a problem for U1.x software aircraft immediately after takeoff because of the lack of the Runway Position Update feature. For this reason, LNAV is not recommended for use until updating has begun. Place an HSI switch in NAV and examine the bottom of PROGRESS 1/2 for radio updating status.

> > Leading Edge Libraries ©



- This is an example of a PLAN mode being used in conjunction with two MANually tuned VORTACs, San Francisco (SFO) and Point Reyes (PYE)
- It is important to note that a manually tuned navaid is not raw data from the navaid, but computer data from the FMC. If an FMC position error exists, these green radials will also display erroneous information.
 - The FIX page is used to build the 4 DME circle from the San Francisco VORTAC.





-



PERF INIT

You get to this page by:

- ACT RTE page PERF INIT prompt (LSK 6R) on the ground.
- $\binom{\text{NIT}}{\text{REF}}$ key (on the ground and IRS initialized).
- TAKEOFF REF page (prior to PRE-FLIGHT COMPLETE) PERF INIT prompt (LSK 5L) on the ground.
- INIT/REF index page PERF prompt (LSK 3L).
- After a long-term power down, wait 15 seconds after applying power before entering PERF INIT data.
- Box prompts are entries necessary to compute performance targets.
- Dash prompts: The optional temp entry provides important performance enhancement for the MAX ALT calculation on the CRZ page if temps are above ISA.
 - Displayed value equals total of ZFW and FUEL
 - Entering either GROSS WT or ZFW causes display of the other.
 - The FMC will round off decimals for display, but uses the full number if entered.

CAUTION

Don't enter the ZFW in this line!

- Main purpose is to optimize ECON climb computations by adjusting the climb speed (slower in a tailwind, faster in a headwind).
- If no entry, FMC assumes climb winds to be zero while on the ground and actual wind in flight; ECON climb speed will not consider wind component.
- Must be entered on the ground to be effective.
- Propagates to the crz wpts if entered after route entry.
- Does not displace forecast winds.
- Will blank upon reaching cruise altitude.
- Ref: U4 Bug on next page.

- Refer to your specific airline SOP. Usually alternate plus reserves.
- RESERVES represent fuel reserves required at destination after normal flight completion.
- Used by HOLD AVAIL field of HOLD page.

TECHNIQUE U5 & up: Enter flight plan arrival fuel. Now, message USING RESERVE FUEL will remind you if/when the predicted arrival fuel is less than flight planned.

- PERF INIT 1/1 TRIP / CRZ ALT GROSS WT /00000 CRZ WIND FUEL - -° / - - -DEL 18.3 ISA DEV ZFW - - -° C T/C OAT RESERVES - - -° C COST INDEX TRANS ALT 18000 TAKEOFF> <INDEX
- TRANS ALT may be manually entered.
 Displayed in feet.
- May change with selection of SID.
 When passing through the Transition Layer, vertical position shall be expressed in terms of Flight Levels when climbing.
 - TECHNIQUE -
 - After entering an estimated ZFW to check arrival time, the PERF INIT page does not offer an ERASE prompt, but the LEGS page does.

• RTA function adjusts Cost Index to meet arrival times.

• Ref: Cost Index chart, CRZ section.

have on the equation.

engineering department.

• Ratio of other operating costs compared to the cost of fuel.

The lower the index, the more influence fuel price has on the speed schedule. The higher the index, the greater

influence time related costs (i.e. maintenance and crew)

• 0 causes ECON speed to be Max Specific Range (min fuel)

in zero winds. 200/500 results in minimum flight time.

requirement defeats cost studies if computed by your

· Adjusting CI to meet operational schedule or ATC



from takeoff to level-off. An EFIS display will actually show a drift to the down wind side, known by some pilots as "la courbe du chien". On U4, top-of-climb wind should not be entered to avoid this problem.

Mathematicians: Temperature Conversion To calculate ISA at specific altitudes. ISA at 15,000 is -15°C. It decreases 2° per 1,000 ft. Example: Calculate ISA at 30,000 ft, $30,000 - 15,000 = 15,000 \times 2^{\circ}$ per 1,000 = 30°. $-15^{\circ} + -30^{\circ} = -45^{\circ}$

 ISA, save F

 flight time by using

 ISA

 ISA

 FLA: 220 -20°F/-29°C

 FL 220 -31°F/-35°C

 FL 250 -31°F/-35°C

 FL 270 -38°F/-39°C

 FL 270 -38°F/-39°C

 FL 280 -42°F/-41°C

 FL 290 -45°F/-43°C

 FL 310 -52°F-47°C

 FL 330 -60°F-51°C

 FL 350 -67°F-55°C

 FL 370 -71°F-57°C

 FL 410 -55°C

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LIMIT key.

You get to this page by:

ACT PERF INIT page, N1 LIMIT prompt while on the ground (U10.1 and up)

NO REQUIRED ENTRIES

- Provides manual override of automatically controlled N1 limits.
- N, for the individual thrust limits, based on present conditions and bleed air configuration.
- Making a selection in flight causes the cursors to move to the displayed value. That selection is then displayed on the FMA/TMA.
- Current N, limit values are displayed for all phases of flight except TO:
 - CON Max continuous thrust GA - Go-around
 - CLB Climb
- CRZ Cruise

U3.0 & up Takeoff Profile option reg'd for Thrust

· Indicates where the takeoff N, automati-

 Allows entry of the altitude in feet AGL. • Default is 1500 FT AGL (ICAO "A") for the ORIGIN airport but may be overwritten.

Reduction ALTitude (T/R ALT).

cally transitions to climb N₁.

U10: Moved to TAKEOFF REF 2/2.

- Normally, N, limits are AUTOmatically specified by the FMC. However, a pilot selection of other limits is allowed. If the AFDS commands an N₁ limit, any manually selected limit is automatically replaced by the AUTO selection when the A/P next changes vertical modes.
- The <ACT> prompt indicates which set of N1 values are currently being used by the system.
- The only time a pilot may need to select an N1 limit is during an engine out situation. One could accomplish the same thing on the ENG OUT, CLB or CRZ page. If a manual selection is made, automatic selection resumes when the autopilot changes autothrottle or pitch modes.
- It may also be useful during a situation where you've encountered mountain wave or a hold at cruise altitude; an extra 2% N1 is available by changing to the CLB limit.

T/BAIT-
1100 FT
91.7 / 91.7%
89.5 / 89.5%
89.5 / 89.5%
87.5 / 87.5%
CLB-2 >

Takeoff Bump Thrust (TO-B) is available when increased thrust is needed for takeoff above the normal max takeoff thrust setting. When TO-B is selected, takeoff thrust is increased to the N1 bug. It applies only to takeoff rating; max climb, max continuous and go-around thrust ratings are not affected. TO-B will be displayed on the FMA.

· Header changes to 26K BUMP.

cally select TO-B.

U10.1 & UP - ON THE GROUND Header changes N1 LIMIT 1/1 to 26K BUMP N1 SEL / OAT - - - /0000°C when TO-B is selected. < TOCLB > with BUMP OPTION < TO-1 N1 LIMIT 1/1 SEL / OAT 26K BUMP N1 < TO-2 ---/+15°C 102.5 / 102.5 without BUMP OPTION 26K < TON1 LIMIT 1/1 24K DERATE < PERF INIT SEL / OAT RED 24K N1 < TO-1 +120 / +61°F 89.1/88.2 /15 22K DERATE 24K < TO-2 <TO <ACT> CLB > 26K BUMP 22K DERATE TO-B <ACT> CLB-1> < TO-1 Selects Takeoff Bump Thrust limit. 20K DEBATE < PERF INIT < TO-2 <SEL> CLB-2> • When TO-B is selected, assumed temp (SEL) thrust reduction is not available. · Takeoff data uplink may automati-< PERF INIT TAKEOFF >

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N1 LIMIT

REDUCED CLIMB

- Two Reduced Climb selections are available.
- Reduced thrust takeoffs lower EGT and extend engine life.
- Since climb power will not be greater than takeoff power, a reduced takeoff thrust may result in a reduced climb thrust. Reduced CLB-1 or CLB-2 is **automatically** selected when a large assumed temp is selected on the TAKEOFF REF page which results in a takeoff N_1 less than the CLB limit. OAT entry on TAKEOFF REF page is required.
- Use of reduced climb thrust reduces engine maintenance costs but increases total trip fuel.
- If CLB-1 or CLB-2 is selected, the N1% for CLB and the N1 cursors still display values for full rated climb.



CLB-1 approximates 3% N₁ reduction to 10,000' (± 8% reduction in thrust) and the provides a gradual thrust increase until normal climb N1 limit thrust is reached at 15,000'. After selecting CLB-1, actual N₁ setting can be read on CLB page. N₁ gauge cursors stay at full rated limit. CLB-2 approximates a 6% N₁ reduction to 5,000' (\pm 16% thrust reduction) and then provides a gradual thrust increase until normal climb N₁ limit is reached at 15,000'. After selecting CLB-2, the actual N₁ setting can be read on the CLB page. N₁ gauge cursors stay at full rated limit.



PERF LIMITS

You get to this page by:

- PERF INIT 1/1, go to NEXT
- $\binom{[NIT]}{REF}$ key (on the ground and IRS initialized, $\binom{NEXT}{PAGE}$).
- RTA PROGRESS page, LIMIT prompt.

The RTA function defaults to flaps-up minimum maneuvering speed and VMO for airspeed limits to meet a specified arrival time. This page allows customization of the operating speed limits to restrict the target speeds the FMC will use in the RTA or ECON mode. Speed restrictions may be entered individually for each phase (climb, cruise, descent) of flight.

The values on this page have no effect on a manually entered speed or LRC.

The default settings essentially provide no restrictions on the Cost Index driven flight profile optimizations, which are always constrained by low and high speed performance limitations associated with buffet margin restrictions.

Both CAS and Mach must be entered. The slower of the CAS or Mach entry will command the speed bug. If the slower entry is the CAS entry, it is displayed as Mach.



Above 5,000', but more than 2,000' below T/C (cruise) altitude, the temperature used for predictions is a linear interpolation between current temperature and the pilotentered T/C temperature. This often results in a non-standard temperature lapse rate. When the aircraft is within 2,000' of T/C (cruise) altitude, the current temperature and the standard lapse rate are used for predictions.

All other flight phases use current temperature - pilot entered value is not used.

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saves editing the DES page if

enroute while flying ECON with

cruise altitude is changed

a CI entry above 54.



TAKEOFF REF

You get to this page by:

- PERF INIT page TAKEOFF prompt (LSK 6R).
- ACT RTE page TAKEOFF prompt (LSK 6R) on ground and PERF INIT completed.
- INIT/REF index page TAKEOFF prompt (LSK 4L).
- TAKEOFF REF page automatically changes to CLB page after takeoff (U10.3 & up)



TAKEOFF REF

May 01



Astronauts and engineers: Runway Update

Runway update reduces Position Uncertainty (PU, now known as Actual Nav Position) from .4 nm (normal Radio PU) to .1 nm. The FMC can do a VOR/DME update after takeoff, however, contaminating a good FMC POSition. This will be fixed in U10.

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see if / which RED CLB setting has been automatically chosen.

TAKEOFF REF

TAKEOFF SPDS or ACARS option

You get to this page by:

- PERF INIT page TAKEOFF prompt (LSK 6R).
- ACT RTE page TAKEOFF prompt (LSK 6R) on ground and PERF INIT completed.
- INIT/REF index page TAKEOFF prompt (LSK 4L).


TAKEOFF REF

Apr 03



The runway coordinate in the FMC Nav database and EFIS Map runway symbol is the *landing threshold*. This landing threshold may be at the beginning of the prepared surface or at the official displaced threshold as shown on the runway diagram chart.

If you depart from any position that is not coincident with this landing threshold, you will introduce an FMC position error. If the takeoff point is ahead of the landing threshold, a TO SHIFT entry will ensure that the airplane symbol on the EFIS Map updates to the actual aircraft position when TO/GA is pressed. Failure to do this incurs a map error. A negative value cannot be entered in the TO SHIFT field, so a departure from a displaced threshold will induce a map error.

This requirement is more critical where the distance from the landing threshold is large and LNAV is used shortly after takeoff. For takeoffs at

max weight in areas of significant terrain and subsequent to engine failure, a map shift error resulting from non-use of the TO SHIFT function may be critical.

The displaced threshold for RW25R at Los Angeles is abeam taxiway F. If departing from the beginning of the prepared surface, you'll introduce a 1000 ft error in the FMC position because you cannot enter minus 1000 into the TO SHIFT field.

At Newark's runway 04L, the displaced threshold is 2500 ft from the landing threshold! This graphic shows the landing threshold as you'd see it out the left window as you're holding short. When TOGA is pressed, the virtual runway will jump up under the airplane symbol, displaying the error. 2.5





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LEGS May 01 You get to this page by: TECHNIQUE Consider having this page LEGS key. displayed during takeoff. RTE DATA page LEGS prompt (LSK 6R). SELECT DESIRED WPT page. NO REQUIRED ENTRIES Modifications to the flight plan can be made which involve only a portion of a route segment or procedure (such as a single leg change). Waypoints can be entered or deleted. 10.2 allows max of 99. 10.3 & up allows up to 150 - Speed / Altitude constraints can be entered or altered. (Altitude entries may not be allowed for waypoints with cruise altitude displayed. Entry formats of 200, FL200, - Box prompts della identify Route Discontinuities. or 20000 are all acceptable. U10. LNAV can be armed on ground. At 50 ft RA LNAV engages. • Altitudes suffixed with the letter "A" are altitudes to be Great Circle distance Manual entries enter the flight flown *at-or-above*. to go to the active wpt. plan on the LEGS page as DIRECT • Suffixed with "B" are at-or-U3.0 and up routing (Great Circle course) below. Leg length in tenths of between waypoints. • While at-or-above or at-ora mile if the leg length • If an entry requires an airway, below altitudes form is less than 10 miles. (Example: J 2), use the RTE page. restriction for the descent they are not used as the end ACT RTE LEGS • The course above the active wpt 1/3 of descent point. Without an 7 NM is the course the airplane needs PIONE .745 / FL286 end of descent point there is to fly at that exact location. RUSTT 25 NM 310 / FL199 no path built for the PATH • When flying direct to a wpt, the 258° CIVET 8 NM descent mode. The FMC Great Circle track changes due 250/14000 17000 will revert to SPD descent. 250° BREMR 12 NM to variation and convergence. 250/12000A Two altitude values identify 250° 6.5 NM ARNES 240 / 10000 11000 an altitude window or block Page one displays RNP / ACTUAL - EXTENDED crossing restriction. the active wpt in 1.70/0.25 DATA > \square · Manual entry of block reverse video altitude is not allowed. highlight. At normal lat/lons, All courses

displayed courses

• If true course/hdg.

have the suffix T

D344L

D288L

12.0 ARC

(249°T).

is displayed, it will

are magnetic.

- FMC will chose the altitude within the block based on the restriction down-route.
- Two ways to check this advisory altitude: DELete Line 3 - do **not** execute. If the small font altitude is within the window, it is an accurate prediction. If lower than the bottom of the window, then it will cross at the bottom of the window. Same for high side. Or, place CIVET in the FIX page and press the <ABM prompt. Check predicted ALT.

Astronauts and Engineers: Color CDUs

Is one type of screen required to produce color?

Answer: No. Color is a characteristic of the CRT rather than the method used to create the image. Color CRTs can be raster, stroke or hybrid. A hybrid CRT is used in some of applications. This type draws the raster image and then uses the time required for the electron beam to return to the top of the screen (fly-back time) to write characters and symbols. This is, as you can imagine, a short time and capability is usually expressed in terms of the inches of character/symbol that can be drawn. It is used to brighten and highlight symbols for increased daylight readability. With the new LCD displays there is no problem with reverse video or color.

displayed after

line one are initial

tracks outbound -

from PIONE in this

1/3

250 / 6321

200/1500A

example.

ACT RTE LEGS

U10.0 and up

followed by ARC, then direction L or R.

An arc can be flown. Arc distance,

• Prior to U 10, the

737 uses a raster

allows for reverse

video highlighting.

LCD is an option.

such as on the 757/

screen which

After U10, the

A stroke screen

767 produces a

slightly sharper

character but does

not allow reverse

video highlighting.



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SPEED AND ALTITUDE LINES

- For speed and altitude lines, keyboard entries are permitted for climbs and descents only, not for cruise legs.
- Minimum speed values permitted are 210 knots for climb wpts and 150 knots for descent wpts.
- Speed entries on the LEGS page must be followed by the slash key (/).
- Manual Mach entries are not allowed.



Apr 03

GRADIENT PATH or VERTICAL ANGLES - U7.1 & UP

VNAV can be used allowing approaches to be flown using vertical angle (Gradient Path) guidance.

The Gradient Path (GP) is defined in the data base and is assigned to a waypoint. It defines a VNAV path between that waypoint and the waypoint preceding it.

A good example is the Gradient Path for an ILS in which the Vertical Angle would typically be

around 3°. This angle is displayed on the LEGS page above the speed / altitude line for the associated waypoint. There are three GP legs in this example.

A modification to the route such as entering another wpt may destroy the vertical angle by converting the inserted leg

to an open idle descent vertical path. (An Along Track entry does not destroy the Gradient Path.) General rule: Don't make changes to a database approach unless you are sure of a mistake.

Vertical Angles may be expected in any approach ending at RWXXX or MAXXX (Missed Approach point). The end of descent point will be RWXXX or MAXXX, and the E/D altitude will be either the Threshold Crossing Height (TCH typically 50 feet above the touchdown zone elevation) or the altitude specified at MAXXX, the MDA.

Prior to 10.3, VNAV will disconnect when passing the GS-XXX point, but it can be re-en-gaged.

If VNAV PATH is active when a gradient path leg becomes active, the PATH mode will remain active, but VNAV will follow the vertical angle rather than the idle thrust descent path. If the gradient path leg becomes active during a VNAV SPD descent, the VNAV mode will change to PATH automatically, and there will be no SPD > prompt on the DES page.

Software 10.3 & up improvements:

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(1) VNAV will not disengage at the GS-XXX point unless APP (glideslope) is armed,

(2) GP now displayed to nearest hundredths,(3) Edit rules have changed to maintain GP

through various edits, which includes insertion of wpts into a gradient leg and deletion of altitude restriction on gradient leg.

Approach Phase

MCP *flyaway* logic is enabled when the nav environment is approach, a path exists in front of the airplane, and the MCP al-

titude is more than 250 ft from the airplane altitude, or has moved within the last 1.5 seconds. The MCP altitude can be dialed above the airplane altitude (i.e., missed approach altitude) and the airplane will stay in VNAV, continuing the descent to the restriction on the LEGS page (i.e. minimums).

Integrated Approach Nav

Improvements include LNAV and VNAV scales on the ADI where loc and glideslope scales traditionally have been found for an ILS approach. The white hollow diamonds are anticipators. The magenta diamond is where the airplane acutally if flying (also called flight technical error). RNP limits are the short lines while ANP is displayed by the moveable (breathing) bars.



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LEGS 1/2 ACT RTE 2.7NM 133° 180/ 3000 MORRY 133° 4.9NM POPPA 180/ 3000 2.2NM GP3.00° 133° **GS-13R** 180/ 2300 \square GP3.00° 133° 151/ 2300 HODAX 133° 5.1NM GP3.00° \square RW13R 132/ 646 RTE DATA> <INDEX

RNP and ANP - U7.1 & UP

LEGS

In the past, navigation has not been an exact science. Just a few years ago celestial nav was sufficient to navigate the North Atlantic. In unconfined airspace, position accuracy can be sacrificed.

A certain amount of error in position has always been accepted. Error is the difference between a specific value and the correct or standard value. As used here, it is related to lack of perfection. RNP/ ANP with GPS updating is "primary navigation".

Greater accuracy can be attained as technology advances, but at a price. Placing satellites in orbit, upgrading FMCs, writing procedures and training flight crews is a major undertaking.

Precision RNAV is under development, which will allow for more tightly controlled airspace – airways ± 2 nm wide. Aircraft capable of Precision RNAV will be allowed preferential treatment such as optimum altitudes and routing. However, Precision RNAV requires a high degree of nav accuracy.

RNP

The concept of Required Nav Performance (RNP) defines the capability necessary for an aircraft to navigate in a particular airspace segment. This value tells the pilot what level of accuracy is required for the particular LEG being flown. The active level of RNP is expressed in nautical miles and is displayed on the ACT LEGS page and the POS SHIFT page. RNP is defined in the nav database according to the present route segmentor can be entered manually. RNP is larger where some navigation error is allowed, such as at cruise altitude, and smaller in the approach environment.

Navigation environments are defined as Oceanic, Enroute, Terminal, and Approach, with increasing accuracy required for each subsequent definition.

Any /E or /F airplane can fly a procedure requiring an RNP of 1.0. The only requirement for a non-GPS system is that radio updating is allowed to continue. Do not place both nav switches in MANUAL. This should be considered in the "radio setup" of your Descent or Approach Checklist. A /G airplane is approved to .3 or less (check you ops specs).

ANP

Actual Nav Performance (ANP) is the degree of current navigated position accuracy, or how good your present position is. It is the degree of accuracy that the FMC will guarantee based on the type and amount of updating that the FMC has experienced (GPS, DME-DME, VOR-DME, or IRS NAV ONLY)

ANP represents an estimate of the 95% containment radius of the FMCS position. You could think of it as representing the Position Uncertainty (PU) of the FMC position, though this term is no longer used. It means that the system is presently unable to verify position any more accurately than that amount - with some level of confidence (95%). If you imagine a circle around the cockpit having the radius of your present ANP, that is where the FMC System position thinks it is located.

ANP has nothing to do with RAIM. It takes four satellites to resolve GPS position. RAIM is an integrity check and needs an additional satellite to provide integrity. If you hold five satellites the system samples four of the five satellites and compares the position with the position it computed with a different set of four satellites. The system cycles through all of the satellites in this manner. If there is an errant satellite it will be discovered and discarded. If the number of satellites gets down to four, integrity is lost, not position. Experience has shown that there are seven plus satellites in view nearly all the time. Even then there is no loss of RAIM annunciation in the cockpit because ANP does not slew immediately to a number in excess of RNP. In the overwater realm one can be without RAIM for nearly an hour and still be within the RNP.

If the ANP exceeds the RNP, a warning is tripped and a message is displayed. VERIFY POSITION in the s/p if the default RNP of .5 is exceeded, or UNABLE REQD NAV PERF-RNP on the EFIS Map if a manually entered RNP such as .3 is exceeded.

With later software RNP values may be entered manually and will appear in large font; this procedure is required if the default RNP does not match the RNP displayed on the approach plate.

Inclusion of this new parameter leads to the necessity of additional CDU messages and are defined in the Message Section. Ref: UNABLE REQD NAV PERF-RNP and VERIFY RNP.

RNP Default Value:

Enroute Oceanic = 12.0nm/400 ft vertical. Enroute environment and no radio updating; i.e., FMC knows it is in an area where no navaids exist from which to update. Enroute Domestic = 2.0nm/400 ft vertical. Not in Approach or Terminal environment but in area of radio updating possibility. Terminal = 1.0nm/400 ft vertical: Below 15,000' and not in the Approach environment. Approach = 0.5 nm/400 ft vertical: For a/c with GPS and either IAN or NPS the default approach RNP is 0.3nm via SW Options disk (OPC).

ALTERNATE ROUTES

- Alternate routes may be added after the destination runway without changing the FUEL and ETAS.
- Special wpts such as ETPs are very useful when placed in the LEGS page in this manner. The wpt symbol will display on the Map but will not interfere with the flight plan track nor will it take up a line on the PROGRESS page, possibly interfering with position report data.
- The LEGS page and / or the RTE page may be used.



MISSED APPROACH - U7.1 / U8 and up

- The guidance function includes the provision to execute Missed Approach (MA) procedures in U7.1, U8, and up. Lateral and vertical guidance is provided throughout the procedure.
- Though U6 may contain MA procedures, speed and altitude assignments on the MA routing do not propagate to the CLB and CRZ page.
- U7.2/U8 and up has the ability to contain Missed Approach procedures in its data base and is able to execute the procedure.

U1.x to U5 To engage VNAV after a missed approach, you must enter a new destination, route and cruise altitude. This will re-activate FMC performance data for VNAV operation. Minimum plan for all software requires Origin, Destination, and one TO waypoint.

5.0 NM		
	150/3018	
0.1 NM		
	150/3000	
5.3 NM	GP 3.0° 137 / 1830	
5.2 NM	GP 3.0° 137 / 148	
21.8 NM	200 / 2000	
AL	- EXTENDED DATA>	
	5.0 NM 0.1 NM 5.3 NM 5.2 NM 21.8 NM IAL	5.0 NM 150 / 3018 0.1 NM 150 / 3000 5.3 NM GP 3.0° 137 / 1830 5.2 NM GP 3.0° 137 / 148 21.8 NM 200 / 2000 IAL EXTENDED IM DATA> IZ 1 and up

NITIATION OF THE MISS

- The FMCS will initiate a MA procedure automatically under any of the following conditions:
- 1. Go-Around method: While in descent and a Go-Around is initiated by any of the following:
 - a Activation of TOGA,
 - b Below MCP altitude, Go-Around Thrust Limit selected (GA on N1 LIMIT page) while in N1 auto throttle mode (typical captured ILS mode);
 - c Below MCP altitude, Go-Around Thurst Limit selected, vertical rate exceeds 600 fpm, and flaps retracting from 30-15 or 15-1 (manual throttle push on a Go-Around).

Predictions for MA wpts will not be generated until the missed approach procedure is initiated.

- 2. *DIR TO method:* When a DIR TO a wpt in the Missed Approach (other than the MAP) is selected. Any descent altitude constraints remaining in the approach will be deleted and be replaced with predicted values.
- 3. Sequencing method: While on approach, the last flight plan wpt prior to the MA is sequenced, that is flown by, and the next wpt is a MA wpt.
- To engage VNAV, the MCP altitude must be reset from the DH/MDA to a higher altitude.

- A speed and altitude entered on the MA route LEGS page will propagate to the CLB and CRZ page.
- Down route predictions do not take this speed into account and it does not propagate to cruise wpts that may exist down route.



U7.1 and up -

• If the FMC transitions onto the MA via the *Go-Around method*, the new CRZ ALT will be the highest of:

- 1. The highest constraint in the missed approach routing;
- 2. The default value of 1500' above the ARP;
- 3. The MCP altitude.

• If the FMC transitions onto the MA via the DIR TO or Sequencing method, the new CRZ

ALT will be set to the highest of the following:

- 1. The highest constraint in the missed approach routing;
- 2. The default value of 1500' above the ARP.

- U7.1 and up -

- In the example below, the original flight plan was DFW to IAH. We've executed the MA at IAH and we are flying direct to COSBI, a wpt in the MA procedure.
- When the missed approach procedure is initiated, the DESTination airport will also be set to the ORIGIN airport.
- This allows the pilot to select a SID to exit the terminal area or another approach.







	e Lalor tanket anno 1 anno 1 an	PADD-select and outside the ministere
ADI DH REF	EXP HSI RANGE VOR/ NAV ILS 80 160 320	TFC switch displays TCAS on EHSI Map.
200	FULL VOR/ ILS MAP 40 FULL 20 - TFC	(Optional equipment)
	PLAN 10	• PLAN displays a static map which
	BRT WXR	is oriented to true north. The top
RST		same as in the Map mode.
BRT	VOR/ADF NAV AID ARPT RTE DATA WAT	planned route by using the LEGS MAP CTR STEP line select key.
06		• Weather radar and TCAS display data is inhibited.
	line for guille vester un	Built

If the FMC detects a failure of an EFCP, the FMC will continue to output map data to the respective EHSI at the 40 nm range Map switches add background data/symbols to Map and center Map modes, can be displayed simultaneously, and are removed by a second push of the switch. - energizes radar transmitter and displays weather radar returns in WXR MAP, CTR MAP, expanded VOR and expanded NAV modes. VOR/ADF - displays VOR and/or ADF bearing vectors extended from the nose of the airplane symbol to the tuned stations. Useful for checking FMC POSition for shorter ranges. displays all FMC database navaids if on map scales 10, 20 or 40 nm. NAVAID displays FMC database high altitude navaids on map scales 80 nm and above. displays all airports which are stored in the FMC database and ARPT which are within the viewable Map area. RTE DATA - displays altitude constraint, if applicable, and ETA for each active route wpt. WPT displays the waypoints in the FMC database which are not in the flight plan route if the selected range is 40 nm or less.

Situation:

You are level at cruise altitude and cleared direct to your destination, McAllen, Texas (MFE). The ILS approach to runway 13 has been selected from the ARRIVALS page.

7 AUT	TIL LLUO	112
212°	155 NM	
MFE		/
THEN		
ROU	TE DISCONTIN	UITY
GS13		150/2000
134°	3.2 NM	BYPASS
MISSI		/ 1950
134°	4.3 NM	GP 3.00°
BW13	Same Same	/ 170
BNP / ACTI	141	
A 00 10 00 1		DTE DATA >

ATC cleares you direct-to MISSI. You accomplish a direct-to and execute. The FMC, because the leg inbound to MISSI was a 3° *gradient path*, now builds a 3° path from MISSI to your cruise altitude.

ACT	RTE LEGS	1/2
214° MISSI	164 NM	GP 3.00° 155 / 1950
134° RW13	5.4 NM	GP 3.00° / 170
134° (1500)	0.2 NM	/15004
314° MISSI	5.7 NM .	· · · / 2000A
HOLD AT		

And there is no DES NOW prompt. If VNAV is selected, the airplane will descend at 1000 fpm until it intercepts the 3° path. So what to do? Go direct to the GS--13 wpt for proper descent planning.

JUUNT PA	IH DES	1/1
E/D ALT 170	ат м 155 / 1 9	1881 50
TGT SPD 740 / 300	то 1747.9z/7	T/D 6NM
SPD REST 240 / 10000	WPT / MISSI / 1	ALT 950
	FPA V/B 0.0 1.3 1	v/s 130
< ECON	PAT	H>
< FORECAST	R	ΓA >







RTE DATA

You get to this page by:

Apr 03

RTE LEGS page, EXTENDED DATA prompt (LSK 6R)

NO REQUIRED ENTRIES

RTE DATA page displays additional RTE LEGS data for corresponding waypoints.

String Josep 1 marchest with holding inventor spot abre have what neuritar, an AS [211173 property was added to US, 116, and UFO to surveyou the wind using at abreast polyne. In the original Sight plan. If you do not have the ABBANETS fraund, you will want to events therein points and re-marc "investigat wind data for covery modificant.



Astronauts and engineers: Winds - Climb Phase

For pre-flight climb winds, the FMC starts with a zero wind at takeoff and linearly interpolates the climb winds to the top-of-climb (T/C) wind value. The T/C wind value is equal to the CRZ WIND entered on the PERF INIT page or zero if a wind was not entered. It uses this approximation to determine the distance to climb to the cruising altitude and ETAs. Ref: U4 bug on page 7.2. Some computer-based flight plans use an average wind from the last wpt to the T/C wpt. If yours does this, do not enter this averaged climb wind on line 2R of the PERF INIT page, but go to the next cruise fix. (The temperature in this row may be generated in the same way.)

If the pilot loads the winds in the LEGS - EXTENDED DATA page(s), leaving the CRZ WIND on the PERF INIT page blank, the FMC considers the T/C winds to be zero until nearing the planned cruising altitude.

After takeoff, the FMC updates the predicted climb wind profile by using the FMC computed actual wind for the current altitude. The actual wind at the current altitude is linearly interpolated to the T/C wind. The predicted distance and ETA to climb to the cruise altitude are then modified accordingly. Obviously, it is essential that the wind value be as accurate as possible to give you the most accurate ETA's and fuel predictions.

Improved graphics

This is an example of the RTE DATA page as viewed in flight. It is useful in entering forecast true winds and carrying out position reports to ATC.

If any or all of the wpts for which a manual wind entry is made are deleted, the corresponding wind entries are also deleted and the wind is propagated from the last entry to forward wpts.

However, current wind is still used for predictions and is blended with the manual entry over a 100 mile distance.

Since doing a direct-to will delete interim wpts that have wind entries, an ABEAM PTS prompt was added to U6, U8, and U10 to preserve the wind entry at abeam points to the original flight plan. If you do not have the ABEAM PTS feature, you will want to create abeam points and re-enter forecasted wind data for correct predictions. ——U1.5 and down -

- Winds propagated from PERF INIT page are large characters.
- As aircraft nears each wpt, wind prediction display changes to match actual winds.
- Manual entries (272/72)do not propagate down the route. An entry must be made at each cruise wpt.

- Winds propagated from PERF INIT page are small characters.
- Manual entries are large.
- · All propagated entries are small.
- As aircraft nears each wpt, biased values are not displayed, though the FMC is blending winds just as on older software.



Astronauts & Engineers: WINDS - CRUISE PHASE

The winds used for predictions during the cruise or RTA phase of flight are the actual winds and the forecast winds assigned to the cruise waypoints. Forecast cruise winds default to the CRZ WIND entered on the PERF INIT page if not entered on the RTE DATA pages. If entry is not made on either the PERF INIT page nor the RTE DATA pages, the actual wind will be used. Entered winds should be periodically checked and updated to ensure accurate predictions.

In flight, the system computes wind from current groundspeed and TAS for its current System winds. For downtrack route predictions, linear interpolation between the present System winds and the next applicable crew entered wind is used. When the aircraft is within 2000' vertically and/or 100 nm laterally from a point at which predicted winds are defined, the System modifies the predicted wind at that point based on current wind and distance to that point. This avoids step change transients in the wind conditions and results in smooth performance predictions.



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ENG OUT CLB

You get to this page by:







3000 ft AFE at zero maneuvering speed.

May 01

OPTIMUM ALTITUDE

The FMC displays OPTimum altitude for each of the three normal cruise modes: Constant or Fixed-Mach (ACT M.XXX CRZ), LRC and ECON.

There exists for each weight, an optimum altitude, increasing with decreasing weight.

The *fixed-Mach* and *LRC optimum altitudes* are calculated to yield maximum nautical miles per pound of fuel. These optimum altitudes yield the greatest fuel mileage for the aircraft weight, so always favor higher altitudes. The 737 FMC will display an OPT altitude for a CAS entry, but it does not have a database to support this display.

The ECON OPT altitude is based on minimum *cost* per nautical mile calculated by the entered Cost Index. The OPT ALT will decrease with high CI entries because ECON is looking for higher ground speed (lower altitude equals higher TAS).

Fixed-Mach and *LRC* yield different OPT altitudes than ECON OPT altitude because they do not consider cost optimization calculations found in CI.

Though not a rule, optimum altitude provides at least a 1.4g or better buffet margin. (1.5g equals 47° bank to buffet onset. 1.4g equals 45°)

If one climbs above optimum altitude and remains at best range speed for the lower altitude, L/D is influenced unfavorably and the engines must broduce more thrust to support the aircraft at the greater angle of attack (alpha) and accompanying increased drag. There is an added penalty because the airplane is flying slower than required and induced drag has greater influence on total drag than does parasite drag for a limited range of alpha. This effect can be minimized by flying at a faster speed (reducing alpha).

By increasing speed (thereby adjusting alpha) you will minimize these penalties (not always attainable because of transonic drag rise, etc.). To compound the problem, climbing the heavy weight higher than required (higher throttle settings for a longer time) decreases cruise fuel, which decreases range. Bleed requirements also increase at high altitudes.

If one cruises lower than optimum altitude without changing speed, L/D is also unfavorably influenced. However the penalties are somewhat less pronounced because the aircraft is faster than required (lesser alpha) and even though the drag condition is not optimized there is a lesser penalty (parasite drag has a lesser influence than induced drag for a limited range of alpha, which is part of the reason for the greater margin of error below optimum altitude. And since cruising flight has begun prematurely (shorter climb), available cruising fuel is increased, thus increasing range (a condition negated eventually by the penalties of cruising too low). The penalties for cruising too low can be minimized by reducing speed to between MRC and LRC for the new and lower altitude.

A climb above *optimum altitude* may be desirable for more favorable winds or ride comfort as long as you do not exceed Max altitude.

Some approximate cruise fuel penalties are:
2,000' below Opt. alt. - 1% increase in trip fuel.
4,000' below Opt. alt. - 4% increase in trip fuel.
Cruise speed of M.01 above schedule - 1-2% increase in trip fuel.

increase in trip iu

BUFFET MARGIN

The higher the airplane flies above the Optimum altitude, the more the buffet margin is reduced. This is graphically displayed on the speed tape.

Before accepting a clearance to cruise at MAX ALT, determine that it is, and will continue to be, acceptable as the flight progresses under projected conditions of turbulence and temperature.

The maneuver margin is stipulated by either the FAA, CAA, or Europe's Joint Aviation Authority and is selected by a program logic pin. The value of the FAA maneuver margin to initial buffet is CDU enterable from 1.15g (1.2g in U6.2) to 1.6g. The CAA maneuver margin limits are fixed at 1.3g. (Ref: PERF FACTORS). 1.15g is about 30° bank to buffet onset; 1.2g is about 34° bank to buffet.



Certain factors such as ATC clearance, temperature, weather, or wind conditions may require the crew to operate very near the Max altitude. The most critical situation is a 737-800 or 900 at high altitude in warm air; the airplane is thrust limited.

MAX ALTITUDE

Max altitude is limited by three factors.

- 1) Max certified altitude structural capability of the aircraft to withstand the pressure difference between the inside and the outside air.
- 2) Aerodynamics, or high and low speed buffet limited altitude. High speed buffet is caused by supersonic airflow over parts of the wing. Low speed buffet results from an increase in angle of attack to the point where the airflow separates from the wing.
- 3) Thrust limited altitude based on a residual rate of climb of 300 fpm in the climb but changing to 100 fpm at cruise.

MAXIMUM RANGE CRUISE (MRC)

This is the speed at which max fuel mileage occurs. MRC is displayed in the ECON mode when a zero is entered as the Cost Index, but the calculation is affected by winds. You can check your Max Range Cruise speed on the ground - complete the PERF INIT page with a CI entry of zero (no wind); or at cruise altitude with no tailwind (headwind is ok). It will be approximately .02 mach less than LRC.

To fly at max range an airplane must operate continuously at the OPTimum altitude. Older generation aircraft have a hard time operating at MRC in the higher altitudes because of the frequent power changes needed to maintain the target speed. The B737 autothrottle system allows operation at MRC but be careful; when you are near the bottom of the thrust/speed curve you are in the speed instability region. It is also useful to operate at MRC when you are expecting a holding clearance down route or when ATC has requested slowest possible speed.

LONG RANGE CRUISE (LRC)

Since older generation aircraft had problems maintaining MRC, the industry adopted a speed slightly faster than MRC called Long Range Cruise. It has been arbitrairly chosen as 99% of the SR of MRC. Flying LRC reduces the number of power adjustments necessary to maintain proper speed, but results in 1% fuel mileage penalty.

For cruise within 2000 ft of optimum altitude: (3-4-5) LRC approximately .743M 700 LRC approximated by .78M. 800/900 LRC approximated by .79M.

ECONOMY CRUISE (ECON)

ECON takes hourly maintenance and crew costs into consideration and balances them against the cost of fuel. ECON speeds are derived from the Cost Index entered on the PERF INIT page. A low CI entry indicates fuel is the most important variable while a high CI would indicate time is the most important consideration.



AUTOTHROTTLE

The autothrottle uses the FMC gross weight to establish a target N1 for cruise at the selected airspeed. It then checks the FMC gross weight against a weight computed using the angle of attack (AOA) data. If the weights differ significantly, the target N1 setting may be hung up at the wrong value which will result in a slightly different airspeed than selected.

TEMPERATURE

The effect of air temperature on range may be negligible but if the temperature is above ISA the thrust will decrease. To maintain the original Mach number, the thrust must be returned to its original value; this means the throttles must be advanced, increasing the engine RPM and specific fuel consumption. However, by maintaining a given Mach under increased temperature conditions, the TAS has increased due to the higher local speed of sound, counteracting the increased fuel flow.

WINDS

Wind is a factor which may justify operations off Optimum altitude. The Wind Trade Table in the back of the book presents the wind gradient required to justify operation above or below Optimum altitude in order to maximize specific range but is very difficult to use.

The CRZ page can be used as a Wind Trade table by entering the desired CRZ altitude and predicted wind at that altitude. Check SAVINGS and FOD.

Under normal situation, allow approximately 300 feet between the airplane and Max altitude.

TIME ITEMS

Airplane operating costs are affected not only by fuel burn but by flight time. In fact, certain categories of costs are directly related to flight time, so that a reduction in flight time of say, 5% will result in a 5% savings for that cost category. These costs are time related costs and are the key to determining the best speed at which to fly for minimum cost. Cost Index documentation recommends cost considerations that are variable and directly related to flight time. It helps to think of C.I. as a measure of the effect of time on the operating costs. Items such as aircraft ownership, hull insurance and landing fees are considered fixed costs and not time related. Direct operating costs affected by flight time are: crew costs (cockpit and cabin), leasing, and variable maintenance costs (airframe material, engine overhaul, labor), expressed in dollars per flight hour. Fuel used is expressed in cents per hour.

Line AB represents crew and certain maintenance costs decreasing as speed is increased.

FUEL USED

Fuel cost is expressed in cents per pound. It should reflect the price of fuel used on a particular leg or the average price for the routes over which the airplane flies. Determination of fuel price is usually a simple process, but can become complicated when prices change at various airports, or when tankering is used.

Line CD represents fuel consumption increas-

So Cost Index is defined then, as a ratio between time-related inflight costs and fuel cost.

Cost Index = Time Related Cost (\$ / flight hr) Fuel in cents / pound

Units of currency per flight hr Cost Index = (Units of currency per lb) x 100

Cost Index is the relative importance of time cost compared to fuel cost.

TIME + FUEL

The TIME + FUEL line takes into consideration the ratio of these two curves and produces one specific Cost Index or ECON speed for that flight leg. If you fly slower or faster than this Official Cost Index, you will increase your cost of operation.

A low Cost Index could mean high fuel costs or the need to increase your RESERVES fuel.

A high Cost Index could mean high time-related costs or a need to get there fast.

Cost Index does not need to be accurate. Using a Cost Index that is reasonably near the correct one is sufficient.

Currently, few airlines actually do the true calculations required to produce an accurate Cost Index.

Will one value of CI approximate LRC for all weights and altitudes? No.





SAMPLES

Included below are comparisons between ECON, LRC and a Manually entered cruise.

TGT SPDs, OPT and MAX displays are accurate representations.



I make two assumptions. The Autothrottles are on and you are ahead of schedule.

(3-4-5) LRC will slow up a little for a tailwind and speed up in a headwind; it's calculatinging ground mi. per lb rather than air mi. per lb.

(NG) LRC does not adjust speed for headwind or tailwind conditions.

TECHNIQUE

To get the best fuel mileage, you have to learn how to cruise between MRC and LRC, or even at MRC. That means you have to know the values for these speeds. This isn't easy because both computers modify the MRC speed in a tailwind or headwind.

Here's a technique to help learn this subject. First, you must have no winds entered on the PERF INIT page. After the PERF INIT page is complete, (use the planned ZFW if necessary) with zero entered as the CI, go the the CRZ page and record the ECON cruise speed. This is your zero-wind MRC speed at your present weight.



If you're sitting in a (3-4-5), press the LRC prompt and record that speed, too. Now you have zero-wind MRC and LRC, at your present weight.

At cruise altitude...

If you're in a headwind, fly MRC; that is, fly ECON with a CI entry of zero. CI zero in a 100 kt headwind is still slower than LRC!

If you have a tailwind, don't allow a TGT SPD that's lower than the zero-wind MRC you recorded at the gate; this will lower your Specific Range (fuel mileage). U10.7 software will correct for this malfunction of flying slower than MRC in a tailwind.

If you're flying LRC in a (3-4-5), be aware the LRC speed will adjust for winds. If you're in a headwind, you'll fly faster than the zero-wind LRC; you will burn a little more fuel and get there quicker. It's ok however, to fly a little slower than LRC so if you have a tailwind, LRC is a good choice, as long as you don't fly slower than zero-wind MRC!

Airspeed Analysis (typica	al -700)	Airspeed Analysis (typica	al -800)	
Gross Weight	126.0	Gross Weight	145.0	
Cruise Altitude	FL390	Cruise Altitude	FL370	
_RC	.786	LRC	.794	
OPT ALT	FL390	OPT ALT	FL358	
MAX ALT	FL410	MAX ALT	FL383	
Cost Index zero (Max range)	.77 (238 kts)	Cost Index zero (Max range)	.775 (250 kts)	
1.3g Buffet boundary (Low / High)	213/255	1.3g Buffet boundary (Low / High)	230 / 267	
Engine out speed	231 kts	Engine out speed	242 kts	
Best Spd in Hold	218 kts	Best Spd in Hold	231 kts	
Airspeed ind yellow arc/pole	208 kts	Airspeed ind yellow arc/pole	223 kts	

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EFFECT OF WIND ON RANGE

CRZ

The effect of wind is to change the ground speed, thus changing the time to travel a given ground distance, effectively traveling a different air distance. (Still-air distance equals ground distance.)

Wind does not influence fuel consumption or altitude, only max range.

Since only max range is influenced by wind, we can adjust MRC airspeed. We minimize the loss in a headwind by increasing the MRC speed by the magnitude of the wind factor. A Cost Index entry of zero will automatically take care of this calculation.

When zero wind conditions exist, a straight line from the origin tangent to the curve of fuel flow versus velocity will locate maximum range conditions (Line AB)

> FUEL FLOW REQ'D LBS

You can use Cost Index Zero to calculate a windcorrected MRC. A headwind increases MRC. The stronger the headwind, the higher the cruise mach.

HEADWIND

VELOCITY

С

VELOCITY, KTS

Because ECON reads the wind and LRC does not, ECON with a CI that approximates LRC (such as 30) nay provide a slightly more *fuel* economical cruise mode in a tailwind situation because it's flying slower than LRC.

To pick a CI that approximates LRC, first check the LRC speed after the PERF INIT page is filled out. Don't enter ANY winds, either on the PERF INIT or on the RTE DATA pages. Now, enter a CI that is close to the LRC value. It is not possible for one CI to match LRC There is no aerodynamic justification for increasing LRC or any other speed in a headwind. There is some justification in reducing LRC slightly in a tailwind, but be careful; if fuel is the main driver, do not fly slower than MRC. Contrary to popular belief, you do NOT want to fly slower than MRC, even in a tailwind.

> Specific Range is the measurement of the aircraft's fuel mileage in NAM per lb of fuel. $SR = \frac{TAS}{FF}$

Using different ingredients, SR can be expressed in terms of ground speed. $SR_G = SR\left(1 + \frac{V_W}{a_0 M \sqrt{u}}\right)$



Max range, no wind, occurs at a velocity corresponding to the tangent point of a straight line drawn from the origin to the curve; this is not L/D max, but slightly faster. With winds, the max range speed is determined by locating the new origins on the abscissa corresponding to the head/tailwind velocity and drawing tangents to the same curve. In the case of a headwind, this will locate maximum range at some higher velocity and fuel flow. The range will be less than when at zero wind conditions but the higher velocity and fuel flow will minimize the range loss due to the headwind. (Line CD)

under all weights and altitudes. Next, enter the forecast winds. The ECON based cruise speed will change accordingly.

If you use this technique in a headwind you may want to pick a lower CI as the goal in fuel conservation is to fly somewhere between MRC and LRC.

Note: Using ECON is this manner is another way of choosing a cruise speed with fuel mileage being the main driver. It defeats the real purpose of the concept of Cost Index - choosing a cruise speed taking into consideration time related items *and* fuel cost, but is a useful tool in flying close to or at MRC.

TYPICAL COST INDEX

Cost Index of zero = Max Specific Range Cost Index of 200 (3-4-5)

500 (6-7-8-9) = Minimum Time

As these costs change due to change in fuel, crew or maintenance costs, the operator can change the (lower speeds) and steeper as CI increases. value of Cost Index accordingly, to optimize the performance of the sytem and the aircraft for current increases to decrease time costs. This results in a economic conditons.

ECON climb trajectories are steeper at low cost index values and flatter at high cost index values.

At a Cost Index of zero, the ECON climb is near the max rate of climb. This decreases the time to climb and minimizes the time spent at climb thrust (high fuel flow).

ECON descent trajectories are flatter at low CI

To summarize: As Cost Index increases, speed shallower climb, steeper descent, less overall time, a higher overall fuel burn, but lower relative cost at the specified CI.



CRZ

HOW TO USE COST INDEX

Many factors need to be considered before choosing a speed schedule.

- Is my company's speed schedule fuel or time constrained?
- · Can I meet the schedule requirements?
- Can I maintain the ATC clearance?
- Do I have enough fuel?
- What's my decision going to cost the company?

COMPANY CALCULATED COST INDEX

ECON speeds are computed to minimize the cost factor which is defined as the sum of hourly operating costs and mx costs related to the cost of fuel. True ECON flying means management must do the analysis and compute the actual cost. The CI will change with fuel cost or lease/maintenance variables. I'll call this the Official Cost Index or Official ECON operation.

If you then change your Cost Index (increase or decrease) the cost of that flight will increase. If you don't fly that OPT ALT, your cost will increase.

If you are on time or early, fly the Official Cost Index.

NO COMPANY CALCULATED COST INDEX

Most airline flight plan speed schedules have no correlation to the assigned Cost Index. In these cases, the FMC will match the paper flight plan's fuel burn and ETA data only if the pilot manually enters a speed schedule equal to the paper flight plan speed schedule. Make sure you enter the winds!

If you don't have a Cost Index that was arrived at in a scientific manner, you're simply using Cost Index as a means of choosing climb, cruise, and descent speeds. There's no science to it since you are not taking into consideration all the costs involved.

SUMMARY

For domestic operation, schedule normally drives choice of cruise speed more than cost of operation. Remember, anytime you get away from an *Official Cost Index*, you're through with the science - i.e. ECON flying based on the ratio of time costs to fuel cost.

TECHNIQUE -

If you don't have an *Official ECON operation*, follow these steps.

- During preflight, enter your own personal Cost Index because the boxes must be filled. If fuel mileage is an issue (fuel-over-destination is too low or fuel is expensive), the CI entry should be from 10 to 20. This will put your speed between LRC and MRC (chart below). If time is the issue, use a CI of 40 or above.
- Fill out the RTE and PERF INIT pages to include wind at TOC and temperature.
- Go to the CRZ page and enter a cruise altitude as close as possible to the displayed OPT ALT. (Don't make a temp entry on the N1 LIMIT page yet.)
- Now go to the LEGS RTE DATA and enter the forecast winds from the flight plan. Your flight profile is now just about as efficient as possible!
- Airline ops: prior to take off or during climbout, check the ETA. If you are on-time, don't make any changes. If early or late, manually enter speeds sufficient to calculate an ETA to get you there at the desired time. Remember, higher speed or lower altitude requires more fuel!
- This discussion does not address operational factors such as gate problems if too early.



THRUST vs SPEED CURVE

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CRZ

You get to this page by:

CRZ key.

Automatically displayed at top of climb when an active climb page is displayed.

OPTIMUM ALTITUDE

- Optimum altitude increases as weight is reduced.
- For an optimum range flight path, an aircraft must climb as it burns off fuel weight.
- Optimum altitude display may be used during preflight, climb, or cruise to evaluate altitude choice.

· Fixed mach and LRC optimum altitudes are based on maximum TECHNIQUE Change Thrust Mode to CLB nautical miles per pound of fuel. • ECON OPT ALT is based on cost. Example: the higher your CI entry, - if you are cruising above **OPT** alt the more important ground speed becomes over range (fuel mileage). So an ECON OPT ALT will decrease as the CI entry is - if you are cruising slower increased (higher TAS). If speed (time) is more important than fuel, than LRC you're not interested in stepping, so you should fly the displayed - if you are cruising in OPT ALT for your CI entry. Does that make sense? mountain wave or If you're interested in fuel mileage, OPT ALT calculation is your best turbulence tool for evaluating step climb. - if you are holding at high • You could consider an LRC derived OPT ALT calculation to be a little altitude inaccurate because of where the calculation comes from in the FMC. - or any other time you feel To get an accurate OPT altitude for your weight and speed, manually like it; it's a good idea. enter a speed equal to LRC, or select ECON with a low CI (< 20). • OPT ALT is not constrained by the minimum cruise time criteria as • TGT SPD becomes active at is TRIP ALT on the PERF INIT page, therefore don't use it for shortlevel off and is reverse video trip altitude selection. highlighted or magenta. · Enter CAS or Mach. ACT M.800 CRZ 1/1 Trailing zeros not req'd for CRZ ALT OPT/MAX STEP Appears at level off. FL365/382 \square \square Mach entry. FL370 Displayed when TGT SPD TO T/D • ECON TGT SPD increases in .800 1919.1z/ 1313NM more than 100 nm headwind and decreases in ACTUAL WIND TURB N1 from T/D and no 88.4/ 88.4% 277°/ 62 tailwind. STEP TO altitude is FUEL AT KEWR • If operating near max \square 18.9 entered. altitude, TGT SPD will be Always displayed \square <ECON ENG OUT> reduced with EAI and / or when less than 100 WAI on. \square <LRC RTA> nm from T/D. Limit 340/M.82 less 5 kts. • Speed Propagation (option) -U4.0 & up Provides advisory When a manual speed is Line selection will display data and cannot be entered on the CRZ page, it the RTA PROGRESS page. coupled to the AFDS. propagates to the DES page. • Reference TURB N1 thrust setting for • If you are cruising at an altitude below 10,000 ft, sudden entry into turbulence. the CRZ target speed will default to 240 kts. Cannot be commanded to the autothrottle. To enter 250, you must first delete the 240 SPD REST • The speed range between high speed and from the DES page. low speed buffet reduces with increasing load factor, aircraft weight, and altitude. ACT ECON CRZ An aircraft at MAXimum ALTitude that is CRZ ALT OPT / MAX 9000 weight limited can have very little speed M.760 PATH DES TGT SPD range for initial buffet when turbulence E/D ALT 240 causes an increase in load factor. 1997 TGT SPD To increase buffet margin, descend .760 / 300 approximately 2000' below MAX ALT to SPD REST increase the speed range for initial buffet. 240 / 10000 Leading Edge Libraries ©

MPORARY	CRZ	
	STEP	ТО
As weight is reduced, fuel	mileage, or "miles per ga	d.", increases. At some point, it becomes more
economical from a fuel iss	ue, to climb to a higher a	ltitude.
May help to monitor wind	s during climb-out and cr	uise. Compare to flight plan winds.
• The STEP TO prediction	differs with the chosen	• In the author's opinion, the STEP TO feature
cruise mode - ECON, fixe	ed mach, or LRC.	should not be used. It will advise a climb when
% of SAVINGS (or penalt	v) will be shown along	it is actually too early. The NOW prompt
with the ETA and distan	ce to the STEP POINT.	appears when MAX ALT equals entry in 1R.
• Eucl at destination reflect	ts STEP TO entry.	• It is not impossible or necessarily unsafe to
• 115 0 and up: When the st	en altitude cannot be	climb to MAX ALT, however it is not normal,
achieved within the cruis	se segment of flight	and should only be done in certain situations
LINARI E is displayed in t	he STEP POINT field	such as when faced with the choice of a very
UNABLE is displayed in t	ne STEP POINT neid.	low altitude over a long period of time.
U4 and below	17. KB 17. KB - 199	
Enter max certified	• Enter STEP TO altitud	e.
altitude into LSK 1R.	• If past STEP POINT, it	will show NOW as long as savings are positive.
MAX ALI FL will appear	• Blank when within 11	0 nm of top-of-descent and when RTA mode is
in s/p. This is the aero	active (step evaluation	n not available) because changes toward the later
limit, i.e., the 1.3g buffet	portion of the flight w	ill have very little effect on economy of operation
boundary. It is not the	• May be transferred to	s/p for entry at 1L.
thrust limit altitude	STEP POINT changes to	to T/D when within 110 nm of predicted T/D poin
which may be lower.	• To clear entry from 11	R, simply DELete.
Arrival fuel predicated		1/1
on continued flight per	CRZ ALT OPT/MAX	STEP
the displayed cruise	FL330 FL355/370	FL370 • Normany displays ACTOAL the
and planned descent	M. 800	NOW I If the wind at the STEP TO altitud
modes and the ACTive	TURB N1 AC	TUAL WIND In the wind at the STEP TO attitud
route and that the sten	FUEL AT KEWR	SAVINGS
(if entered) will occur	15.9	0.5% plan of ask ATC). Changes
at the point computed.	<econ< th=""><th>ENG OUT></th></econ<>	ENG OUT>
	<lrc< td=""><td>R • A step climb performed late in the en-</td></lrc<>	R • A step climb performed late in the en-
		route segment will not have a significant
	137 8 151	effect on total trip cost or fuel. A step
TEC	HNIQUE	trade for these reasons is more effective
So how do you step-climb	the 737?	earlier on in the cruise segment.
• Don't use the STEP TO for	eature.	• Other reasons for step-climb such as fo
• (NG) Check the SAT on	PROGRESS 2/4. If the	ride comfort may still be effective late
ambient temp is $ISA + 1$	0 or more, enter that SAT	into the cruise segment.
line 3R of the PERF INIT	page.	• On the ND Map, a green donut with S/
This may affect the MAX	ALI calculation.	will be displayed at this point.
• Climb when the MAX AL	1 is approx. 300 it above y	your L
desired altitude. In this e	example a climb to FL3/0	272 and yet mountaining that a street by an
would commence when	the MAX ALT is approx. FI	LOID. HILL HILL HILL HILL HILL HILL HILL HIL
• If you climb too soon, th	e engines will run at a hig	sui 191 school guianti qu'adquoir quine abodDi-
(high fuel flow) and you	in nave less protection fro	(3-4-5)
burret boundary until the	the MAX ALT will increase	ACT LRC CRZ 1/1
• To predict a step-climb,	The WAX ALT WIT Increase	CRZ ALT OPT/MAX STEF
It approximately every	Ititude on the CP7 none w	
• After entering the new a	intude on the OHZ page yo	ETA M.743 1648.3z/ 958NM
may also enter the estim	hated wind and check new	
and FUEL AT destination	before executing.	ΔCT FCON-CR7 1/1
• If the MAX ALI display i	s infinited by the certified	TALT CRZ ALT OPT/MAX STEE
ceiling, climb to the cer	tified ceiling when the OP	TCT SPD FL404/410
is approximately (3-4-5) 1,000 ($1NG$) 700 feet less	M.782 1921.6z/1254NM
the MAX ALL.		

Situation:

You have just depareted Houston Intercontinental, destination San Pedro Sula, Honduras, in a -900. You are flight planned for FL330 on UB 753.

ATC: "Columbia STS107, climb and maintain FL290, company traffic above you at 330. Can you make FL 370?"

You're interested in arriving over San Pedro Sula with as much fuel as possible; because of the heavy payload, your planned fuel-over-destination is at a minimum.

Displays MAX altitude. Checking the MAX altitude ACT M.780 CRZ 1/1 on the CRZ page, you notice CRZ ALT FL290 OPT/MAX STEP FL362/372 \square \square FL 370 is possible, but let's TGT SPD TO T/D do some investigating. \square .780 1800.6z/ 736NM \square ACTUAL WIND 287°/ 53 TURB N1 84.4/ 84.4% \square \square FUEL AT MHLM \square \square 12.2 \square <ECON ENG OUT> \square \square <LRC \square RTA> • Check the OAT on PROGRESS page 3, ask ATC if they've got someone at that ACT PERF INIT 1/2 altitude for a temp report, or check GW/CRZ CG TRIP/CRZ ALT \square 140.2/19.7% FL362/FL290 \square your flight plan for the temp at FL370. CRZ WIND 298°/ 64 PLAN/FUEL • In this case, it's ISA +15 at FL 290. \square e 122.4 • Go the the PERF INIT page and enter ZFW DAT J/6 123.0 the ISA + 15 at FL 370. 44°F -42°C RESERVES TRANS ALT (It's a good idea to have a temp chart \square 8.4 18000 with you at all times.) PERF INIT COST INDEX e \square **REQUEST>** 68 \square N1 LIMIT> \square <INDEX ISA · FL 220 -20°F/-29°C FL 250 -31°F/-35°C Now go back the the FL 270 -38°F/-39°C ACT M.780 CRZ 1/1 CRZ ALT OPT/MAX STEP CRZ page and check the FL 280 -42°F/-41°C FL290 \square FL362V355 \square MAX altitude. Surprise! FL 290 -45°F/-43°C TGT SPD TO T/D FL 310 -52°F/-47°C \square 1800.6z/ 722NM \square .780 ACTUAL WIND TURB N1 FL 330 -60°F/-51°C 84.4/ 84.4% 287°/ 53 \square FL 350 -67°F/-55°C FUEL AT MHLM \square \square -71°F/-57°C 12.2 FL 370 \square <ECON ENG OUT> \square To verify the FMC calculations by using \square <LRC RTA> \square your flight manual: • Check your weight by turning to the APPROACH REF page. APPROACH REF 1/1 Next, check your Altitude Capability GROSS WT FLAPS VREF chart, specifically, the Cruise Thrust P 146.3 15° \square 160KT Limit Altitude at ISA + 15. P 30° \square 151KT MHLM22 737-900 Altitude Capability LRC & M.79 \square \square 9200FT2004M 40° 141KT OPT ALT (ft) CRUISE THRUST LIMIT ALT (ft) WEIGHT ILS 22/CRS FLAP/SPD 110.70IRVM/219° \square \square 30/147 (1000 lb) ISA+10 ISA+15 WIND CORR 150 35000 36300 35000 E \square +05KT 145 35800 37000 35800 Leading Edge Libraries © 104



RTA CRZ - U4 & up

mation as the flight takes place. Speeds are auto- Cost Index than originally planned.

The RTA navigation mode is designed to assist the matically adjusted for inflight winds and route pilot in complying with a required time of arrival at changes by the FMC adjusting the Cost Index. If the a designated waypoint such as the final approach RTA is unobtainable under present routing and/or fix, holding fix or airport. After the appropriate environmental conditions, the FMC will so advise waypoint and RTA are entered, the FMC will com- by displaying an appropriate message. For the most pute a recommended takeoff time and speeds re- economical operation, the recommended takeoff time quired to comply with the RTA, and progress infor- should be met, as a later takeoff will result in a higher



CAUTION

VNAV cannot

be engaged.

ENG OUT CRZ

- Provides advisory data for three performance parameters; thrust, target speed, and altitude capability.
- If executed, all subsequent performance predictions are blanked.

If an engine fails while in cruise, a descent to a lower altitude and an adjustment in speed usually is necessary.

A driftdown profile, designed to minimize loss of range, is displayed.

Advance the thrust lever on the operating engine to max continuous thrust and start a descent to the engine-out cruise altitude. This will take quite some time, depending on starting altitude. During descent time is available to consult engine inop cruise data and establish a new plan. You have some alternatives:

- 1) Slow to, then descend at and maintain E/O TGT SPD (Max L/D). This results in max altitude capability, max range and minimum driftdown angle.
- 2) If not range or terrain limited, descend and maintain MAX ALT at single engine LRC. A higher speed will increase the descent angle but shorten the time exposed to single engine operation.



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CRUISE WAYPOINT - U1.x to U6

NOTE: This problem does not pertain to U7.0 and above.

When programmed with route and performance data, the FMC computes predicted route segments for the climb, cruise, and descent phases. This establishes the T/C and T/D points. Each waypoint is then assigned to the proper segment.

Once assigned, the waypoints remain in the respective phases unless basic performance data such as cruise altitude is changed.

Waypoints that are identified as cruise waypoints in the Smiths FMC are not allowed to have altitude restrictions entered by the pilot unless they are close to the top-of-climb or top-of-descent points. (U7.0 fixes this problem). On some versions of the Smiths FMC, the lower altitude restriction may be accepted while programming on the ground or early in the climb. Thus, if the pilot knows of probable ATC restrictions for a particular flight leg, attempt entry into the FMC at the gate.

Sometimes entering an altitude restriction on the waypoint before the one in question will allow the altitude restriction to be entered at that waypoint. It may be necessary to make an extra waypoint along the route to do this.




TEMPORARY





• The altitude trend vector will lie right on top of ELP if you dial in this rate of descent.

With the help of Dole, Padilla, Hurt, Perkins and others, let's discuss the Basics of Jet Performance.

The problem of efficient range operation appears in two general forms: to extract the maximum flying distance from a given fuel load, or to fly a specified distance with minimum expenditure of fuel. (Hurt)

The common denominator for each is the specific range, NAM/lb of fuel.

Turbojet engines are designed to operate at high rpm and will produce higher specific fuel consumption values at higher altitudes since an increase in altitude requires increased RPM.

Lower inlet temps at altitude results in decreased specific fuel consumption.

An increase in altitude will increase the proportion of velocity (TAS) to thrust and provide a greater TAS for the same thrust. At FL400 the TAS is twice the indicated airspeed!

There exists for each weight, an Optimum Altitude; it continues to climb as weight is decreased. Flying at Optimum Altitude will produce the best Specific Range at that speed.

If the airplane is flown at MRC and OPT ALT, the SR value is maximized. This is called the optimum altitude for max range. This speed is slightly faster than the corresponding speed for max endurance which is only a function of minimum lb/hr and is unchanged by wind.

When considering max range (or max fuel-overdestination) only MRC speed is increased in a headwind (Cost Index zero). From an aerodynamic study, no other speed should be increased in a headwind if max FOD is the objective. This is why flying ECON is not more advantageous than flying LRC from strictly a fuel standpoint.

Max altitude considers 3 things: max certified altitude, the high and low speed buffet boundaries, and the thrust limit.

The preceding paragraphs are important and mean that to operate in a fuel efficient manner, you don't just fly as high as the airplane is capable of reaching for your present weight (service ceiling). At heavy weights, the thrust requirements are such that a lower value of nam/lb will be obtained if flying above Optimum Altitude. The preceding paragraph states that you must operate close to Optimum Altitude for your chosen cruise speed schedule to realize best nam/lb.

The thrust of a turbojet/fan for a given throttle setting is directly proportional to the mass flow rate of the air through the engine. Consequently, as the density of the atmosphere decreases with an increase in altitude, so does the available thrust. Specific range (SR) is the nautical air miles per pound of fuel (NAM or nam). It is the measure of the fuel required to cover some air distance; the higher the SR, the more distance covered on a given quantity of fuel. SR generally does not include the effects of wind; as a result nam is used instead of nm. SR is a measure of aircraft efficiency, or SR = TAS / ff in pph

Since the gross wt will decrease along the flight path, the best specific range will increase along the flight path and the potential for the best mileage will be at the end of the flight when the aircraft is the lightest. (Hale)

Long Range Cruise (LRC) - corresponds to a flight condition where the SR is 99% of the SR at MRC; no rigorous analytical derivation is associated with this percentage. A 1% reduction of range is traded for 3-10% higher cruise speed and keeps the airplane in a more speed-stable area.

Cruise Schedules or strategies:

- 1. Constant Mach-constant lift coefficient. (cruise climb / block altitude profile). In order to keep the CL constant as the weight decreases, density (rho) must decrease so as to keep the ratio of the weight to the atmospheric density constant. Consequently, the aircraft will be in a continuous climb. Range factor is constant. If LRC is the chosen speed, you're accomplishing 99% max range in a speed stable environment. This is just about as good as you can do.
- 2. Constant altitude-constant lift coefficient. (variable Mach schedule) Ex: LRC flight. Since CL is constant, lift-to-drag ratio will also be constant. Airspeed must be decreased as fuel is used if CL is to be kept constant; thrust must constantly be decreased as the GW decreases.
- 3. Constant altitude-constant Mach. Ex: FL350 M.79. (hard altitude-hard airspeed) The two flight parameters of lift-to-drag ratio and the lift coefficient will decrease along the flight path. Thrust will be reduced along the flight path so as to maintain constant airspeed.
- 4. *Constant thrust.* The two flight parameters of lift-to-drag ratio and the lift coefficient will decrease along the flight path. Thrust is maintained and speed is increased (to the high speed buffet) as weight decreases. Such a condition might exist when time is more important than fuel.

In order to maximize the specific range at all points along the flight path, the lift coefficient must be kept constant at all times to be equal to the bestrange lift coefficient, which is a design characteristic. Therefore, best-range conditions can be applied only to the two constant lift coefficient flight programs, 1 and 2 above. (Hale)

CRUISE DESCENT vs. DESCENT NOW

ATC: "Ford-Stout, descend to flight level 310."

May 98

Here are two Cruise Descent examples; in the first, the top of descent will be reached prior to the new cruise altitude (poor pilotage); in the second, the new cruise altitude will be reached before the top of descent.





Dec 02





ATC COMMANDED SPEED INCREASE OR DECREASE





The energy compensated target speed is not allowed to fall below Block Operating Speeds which are computed as a function of flap position and gross weight.

1 1007 11	This becon of Environ eres					
POSITION	< 117.0	117.0 - 138.5	> 138.5	600/700/800		
0	210	220	230	VREF 40+70		
1	190	200	210	VREF 40+50		
5	170/180*	180/190*	190/200*	VREF 40+30		
10	160/170*	170/180*	180/190*	VREF 40+30		
15	150	160	170	VREF 40+20		
25	140	150	160	VREF 40+10		
30	C	ompensated VR	EF + VREF in	crement		

* U10.3 Increased Block Operating Speeds

ALTITUDE INTERVENTION - U6, U8, U10 (option)

The Altitude Intervention feature provides the pilot with the ability to perform the following operations using the Altitude Select knob and the Altitude Intervention pushbutton, both on the MCP.

1 Intervention of FMC Altitude Constraints during VNAV Climb or Descent:

Dec 02

To delete the next altitude constraint, the MCP altitude is set above/below (for climb/descent respectively) the next altitude constraint and the Altitude Intervention pushbutton is pressed. One constraint is deleted for each push. In climb, lowest constraint is deleted. In descent, highest constraint is deleted. This operation can be performed with or without VNAV engaged. An altitude constraint on a waypoint which represents a leg terminated at an altitude, cannot be deleted using Altitude Intervention.

If all FMC altitude constraints are deleted, the descent mode will revert to a VNAV speed descent.

2 Intervention of FMC Cruise Altitude during VNAV Cruise:

Set the MCP altitude above the cruise altitude and press the Altitude Intervention pushbutton. To do this in a climb, there must be no altitude constraints remaining in the climb phase. Attempting to raise the cruise altitude above the maximum allowable cruise altitude using Altitude Intervention will not change the cruise altitude and will result in MAX ALT FLXXX message. This operation can be performed with or without VNAV engaged. *Cruise altitude cannot be lowered using Altitude Intervention*.

If a lower altitude is selected, an early descent (DES NOW) will be initiated.

3 If the VNAV ALT option is enabled, resume a climb/descent after holding an MCP altitude while in climb/descent. (VNAV ALT is annunciated by EFIS symbol generator to EADI when level at MCP altitude not equal to FMC altitude.)

To resume a climb/descent (while in climb (or cruise)/descent, respectively) from altitude hold of the MCP altitude, the MCP altitude is set above/below, respectively, the hold altitude, and the Altitude Intervention pushbutton is pressed. This operation can be performed only with VNAV engaged.



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Intervention of FMC Airspeed Constraints during VNAV:

The Speed Intervention function, selectable by pressing the MCP IAS-MACH knob, is provided to allow a means of overriding the FMC's commanded speed. Selection of Speed Intervention mode will display current target speed in the MCP's speed window, automatically setting it to the commanded FMC speed. Changes to the commanded speed can then be made via the MCP IAS-MACH knob.

Pressing the button again blanks the speed window and returns speed to the FMC VNAV path schedule.

To resume former FMC speed:

SPD INTV switch Push

MCP IAS-MACH display blanks and FMC commanded VNAV speed is active.

Here is an example of a Speed Intervention command. ATC: "Boeing 40, I need Mach point seven six for spacing".



A couple of definitions:

- Strategic: a systematic application toward a long term goal.
- Tactical: involving actions of less magnitude serving a larger purpose, carried out with an immediate objective.
- The Speed Intervention feature is tactical in nature.

INTRODUCTION: DIRECT-TO

There are two kinds of direction on a sphere; a *great circle* and a *rhumb line*.

The arc of a *great circle* is the most direct route on the surface of the earth, and may be considered the shortest line drawn between two points.

A great circle track will appear as a straight line on a gnomonic projection; a chart on which neither meridians nor parallels of latitude appear as parallel lines.

In the illustration, a string is stretched over the globe from New York to London to obtain the *great circle* route. Three points are necessary; a wpt on each end (New York and London) and the center of the earth. Any plane passing through the center of the earth cuts the surface in a *great circle*. The Equator is a *great circle* as are all

meridians. The string makes an angle

of 54° true at the meridian of New York, about 90° true with the meridian of Iceland, and a greater angle with the meridian of London (112°). The direction of the *great circle* is constantly changing as we progress along the route, except if the two points are on the same meridian or both are on the equator.

A *rhumb line* is defined as a line which crosses all meridians at a constant angle. An aircraft that holds a constant true course of about 80° from New York will arrive at London, but will have to fly an extra 141 miles. A *rhumb line* is represented on the globe under the string and in the Mercator projection at the bottom of the page as the straight line. At latitudes within an area such as the United States, for distances of less than 1,000 miles, the saving in distance by way of the *great circle* is not a great deal. The advantage of shortest distance may give way to shortest time.

A small portion of the earth's surface may be represented on a plane surface with only slight distortion using Lambert projections (Sectional Charts); a long line east and west, for

example along the Canadian border, will display more dist o r t i o n (WACs and ONCs).

Great circle flying, like *great circle* sailing, is most advantageous when flying a long voyage east or west in relatively high latitudes.

Whether to fly the *great circle* route or the *rhumb line* was a major decision by the early Atlantic racers.

Ships could be found on the southerly course, which were used for weather reporting, in case of distress or to relay messages. Lindbergh flew the *great circle* track. He changed compass headings each 100 miles. Kingsford-Smith was the first pilot to conquer the two great oceans and the first to circumnavigate the world via the great circle route.

The FMS has robbed *great circle* flying of it's mathematical mysteries.

By the way, a minute (1') of latitude is considered a nautical mile, but because of the flattening of the earth near the poles, the length of a minute of latitude increases a bit. Minutes of longitude are never a measure of nautical miles except on the equator.



Any straight line on a Mercator chart is a *rhumb line*. The *great circle* route appears longer due to the fact that the Mercator projection distorts the areas in high latitudes. (1569 Gerardus Mercator, Flemish geographer)

INTRODUCTION: DIRECT-TO

A straight-line track drawn on a Lambert conformal conic projection does not cross all meridians of longitude at the same angle, as may be seen in this drawing.

A line has been drawn from San Francisco to New York. While it may not be apparent to the naked eye, the angle between this track and north is different at San Francisco than it is at New York. A protractor has been used to indicate this fact.

This track takes the true direction of 71° at San Francisco, and at New York the true direction is 100°. (New York is on the 74th meridian and San Francisco is on the 122nd.)

If the 29° difference between the initial and final track is divided by the 48° difference in longitude between the two cities, it will be found that each meridian on this chart leans toward or converges on the one next to it by $6/10^{\circ}$.

The line between San Francisco and New York represents the shortest route between these cities; it is to be thought of, however, not as a single track, but rather as a series of short tracks, each of which makes a slightly different angle with the meridian it crosses. If a pilot was traversing the country before the advent of RNAV, the navigator would, if there is no wind, shift the true heading of the plane $6/10^{\circ}$ every time he crosses a meridian. If he chooses to consider the long track as actually being a series of 16 tracks each crossing 3° of longitude, he may alter the true heading of the plane 3 x $6/10^{\circ}$, or, roughly, 2°, whenever the flight has progressed through 3° of longitude.

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Years ago, the general practice among navigators was to divide the entire track into legs covering approximately 4° of longitude; the track for each leg is measured clockwise from north at the central meridian. Thus an average track is obtained for the leg that, at most, will take the plane but a few miles off the main track laid down. Note should be made that this slight divergence will always be to the south of the main track in northern latitudes and north of the main track in southern latitudes.



Thanks to Capt. Dave Hooper for this technique.

- To turn smoothly to a new wpt, use HDG SEL and position the track line/track indicator above the next wpt/wpt bearing indicator. This takes some practice and a check for a crosswind. After the airplane rolls wings level, accomplish a DIR-TO.
- Be careful. If you use the HDG SEL trick first, then do the DIR-TO and press LNAV before you are on a track direct to the new wpt, the a/c will turn back to capture the curved magenta line. In other words, don't mix the two styles of going direct-to a wpt. Use one or the other.

TECHNIQUE

Use MCP HDG (with 10-15° bank) for initial turn to the wpt to reduce the bank; when the track is on the route press LNAV. LNAV bank angle is a function of TAS and the magnitude of the turn. (Big pilot complaint. Waiting for Boeing order to fix.)



INTRODUCTION TO INTERCEPTS

This lesson could not have been written without input from Dave Gorrell, Mike DeJonge, Jim Terpstra, and others.

There are a few ways to intercept a leg in the flight plan:

- 1 Allow the FMC to auto sequence; then engage LNAV no keyboard action is required.
- 2 Intercept a leg using the CDU; accept the course at LSK 6R if available, by making it big. The FMC will use the original great circle course between the two waypoints.

Back up the intercept by:

- 1 Tune a VOR and watch that VOR needle on the RDMI, or set the course bar and monitor the intercept with raw data using a VOR mode or, (EFIS) monitor the computed data by watching the airplane as it intercepts the green MCP course line.
- 2 Enter the anchor navaid in a FIX page with the outbound bearing; verify the magenta line passes over/near the green dashed FIX bearing line. This is FMC computed data, not raw data.

We used to navigate the airway system by following the outbound radial to the changeover point and then along the inbound radial to the next VOR. The FMC has made our workload much lighter during cruise, but many times, will display a different course than the chart.

The main reason for the difference between the mag courses on the Jepp chart and in the FMS is that Jeppesen publishes the FAA value for the airway which is the true course with the station declination of the VOR applied. The FMS computes the same true course as does the FAA, but the FMS will use the station declination if the intercept is to a navaid, or it will use it's own mag var model if the intercept fix is a waypoint. By the way, the IRU provides the mag heading and track to the HSI/Nav display, using it's own mag var model!

If you put a VHF navaid in LSK 1L, when you do an intercept-leg-to, the declination for conversion from true to mag comes from the nav database and will almost always match the chart, except for the effect of tenths of degrees. To make the problem worse, the FAA doesn't change the VOR declination until it gets at least 4° different than local magnetic variation. This means you could have a few degrees difference between the Jepp chart course and the FMS computed course.

Great circle effects also enter into the discussion. Consider the following example.

A Fokker VII has just departed Dallas-Ft Worth Intl (KDFW) and is being radar vectored to intercept the 070R from Ranger (FUZ) to Texarkana (TXK), where the inbound radial is 250.

"Fokker VII, fly heading 140 to join J42 to Texarkana".

FUZ is the active waypoint and the anchor for airway J42.

If an airway is loaded, the FMC just connects the waypoints with great circle courses; no declination is needed so none is applied, until the true is converted to mag for the CDU display. (Mag calculations are only for pilot consumption - CDU and EFIS displays)

As you fly on a heading closer and closer to the magenta line, eventually FUZ will drop out and the next wpt (TXK) will become active. It is at this point you engage LNAV. The magenta line remains in the place it was before and keyboard action is not required - you have to monitor the situation very carefully.

If you do an intercept to a wpt 160 nm down the road the course displayed in 6R may not match the chart because it retains the original course of the leg that connects the two wpts on the airway; press 6R to make it big and you will end up flying the airway.

If an intercept is necessary, use the DIR/INTC key, or for later software, accept the course that is displayed at 6R and make it big. The FMS will fly the shortest line between the two fixes - it's just that the numbers don't match.

Reality check: If you are departing Dallas-Ft Worth Intl you'll get a Departure Procedure that will have short legs (\pm 35 nm) and the great circle effect mentioned above will not occur.

So we have two reasons why the courses on the chart may not exactly match the CDU, mag var vs station declination, and great circle effects.



EXECute. Don't select LNAV until you've rolled out wings level on the intercept heading. Monitor your waypoint bearing pointer and course bar for "lead in". If intercept is greater than four miles, use PROGRESS 2/2 to show approximate distance to the intercept. With U7.2 and up, the XTK ERR will zero out when LNAV is engaged.

If within the LNAV capture criteria, LNAV remains engaged, otherwise LNAV disengages. With LNAV disengaged, manually select any desired heading on the MCP to intercept the flight plan leg to the wpt, then re-engage LNAV. NOT ON INTERCEPT HEADING is displayed when LNAV engagement is attempted and the present airplane track to the intercept waypoint does not allow for an intercept.

Enroute, it is predicated on course (track).

Only predicated on heading when on a *conditional wpt* HDG leg is active.

The PNF should back up the PF with raw data when doing an INTC LEG TO function.

INTC LEG TO - U3.0 and up



 An intercept anomaly exists in all EFIS software up to U7.4 / 8.4. This problem is fixed in U7.5/ 8.5 and is fixed in U10 and up.

After takeoff from El Paso, Texas on runway 08, ATC says: "Boeing 247, fly runway heading to join J183 to Pecos, then as filed."

- If you accomplish an intercept to PEQ, the magenta route will jump behind the airplane symbol, leading one to believe LNAV should/could not be engaged to capture J183.
- Here's what's going on. If the intercept course lies within 2 degrees of the *history wpt* (RW08 in this case), the magenta route will extend directly to the *history wpt*, jumping behind the airplane in this case.
- If LNAV is engaged, the magenta route will again re-position to appear ahead of the airplane symbol, and LNAV will indeed join the airway, but the EFIS display does not lead one to believe LNAV can be engaged.





- First check to see which wpt is active. If the downroute wpt is active you can arm LNAV as soon as you roll out.
- In this case, notice that ELP is still active. It's still in line 1 of the LEGS page and magenta instead of white on the Map. Don't do anything but fly the airplane in heading select.
- When ELP drops out, (auto sequences), arm LNAV. This will occur when the XTK ERR is around a couple of miles. On the non-EFIS airplane, first the course bar will swing to the outbound course; a few seconds later ELP will drop out.
- The airplane will intercept the airway and no further steps are required.
- The down side to this technique is that you must remember that you are in HDG SEL, and not set up to capture the outbound course in case you are distracted.

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DIR TO / INTC LEG TO

PATH CAPTURE, BANK ANGLE & VERTICAL GUIDANCE

Path Capture criteria

If the present aircraft track crosses the leg to be captured at an intercept angle of greater than 15° (8° U5.0) or less than 90°, the track will be maintained until the leg is captured by the lateral steering function. If, however, the predicted intercept point is so close to the leg's termination waypoint that a path cannot be calculated, a new path will be calculated direct to the waypoint (instead of maintaining present track). If the direct path does not allow calculation of an acceptable path, then the path capture will be turned over to the normal FMC steering function to steer to the flight plan path.

If the present aircraft track does not cross the leg to be captured or its backward extension, or crosses at a intercept greater than 45°, (30° U5.0) but the aircraft is within 3 nm of the desired leg, (check XTK ERR) then the path capture will be turned over to the normal FMC steering function to steer to the flight plan path.

If the intercept is less than or equal to 15° (8° U5.0) outside 3 nm, or less than or equal to 45° (30° U5.0) inside 3 nm crosstrack, then lower initial steering gains will be used.

If none of the above criteria is satisfied and an attempt to use the INTC function is made, the advisory message NOT ON INTERCEPT HEADING will be displayed and no MCP engagement of the LNAV will be permitted until a corrective change has been introduced.

U7.2 and up: After an intercept is performed and after LNAV is engaged, a dash-dot magenta line is drawn from the airplane symbol on the EFIS map to the solid magenta line; this is a capture path and the XTK ERROR is referenced to this new path.

Astronauts and engineers:

course displayed after the mod is EXECuted?

Before the mod is EXECuted, the course reflects the Great Circle heading from your current position to the entered waypoint. After the EXECution, the turn radius to the new heading is accounted for which changes the displayed course a few degrees.

Bank Angle

The bank angle is a function of TAS and the magnitude of the turn. If more than 50° of turn is required, the 25° maximum planned bank angle will be used. If only 20° of turn is required, the bank angle will be around 15°. If less than 10° of turn is required, the bank angle will be around 8° as a minimum. If unexpected winds are present, the bank angle may vary up to a max of 30°. This will also happen if LNAV engagement is delayed after the modification is executed.

It is common to see the 737 go to excessive (25°-30°) bank while "at altitude"; this is a major complaint of the line pilot. This problem may have been addressed in U10. Pilot reports are requested.

The bank control must remain under FMC control in order to meet airspace limitations established by the FAA and fly the computed path. Now, the first thing that has to be thought about is that the bank control must be consistent and work for all situations encountered during the flight. Inevitably there will be situations in which the FMC response differs from that which the pilot would have used. One area of frequent comment is roll control at altitude for small turns. The bank control continues to be improved as the designers are aware of the pilot concerns and are trying to make things better.

Vertical Path Control

Prior to U10.5: For path descent operation, the maximum descent flight path angle for predicting interception of the vertical reference path is 7° for aircraft operation above the airport speed restriction altitude plus 1,000' and 6° below this altitude.

10.5 & up: Max descent path angle corresponds to Vmo/Mmo minus 5 kts if above the airport speed restriction altitude and speed restriction plus 10 kts if below the airport speed restriction altitude. It is stil 6° with flaps down.

If the predicted late descent path with these limitations does not intercept the vertical reference path without violating an altitude constraint, a DES PATH UNCACIEVABLE or UNABLE NEXT ALTITUDE message is displayed on the CDU. Longitudinal steering also is constrained by these limits when vertical speed command to the AFDS is being generated.

The vertical speed steering commands at path Why does the course displayed for a DIR TO mod differ from the capture or at the vertical flight path transitions are acceleration-limited so as to produce a normal acceleration of not more thao 0.1g.



- A DISCO existing directly in front of the intercept wpt – box prompts appear.

If you are cleared to join an airway, ensure that an *anchor* to the airway is present in the RTE page. This is a sure way to avoid being off the airway, which could lead to a violation.

one degree.

the stored value:

prompts appear, or

Only 3 conditions require manual entry over

- The stored course is not the desired course, or

- The entry in 1L was not part of the route - box





Navigate to a No-name intersection using Place-Bearing/Place-Bearing wpt.

Clearance: "ANT-20, cleared to Sioux Falls via the Fort Dodge 360 radial and the Sious Falls 090 radial. Fly heading 330 to join the Fort Dodge 360 radial northbound."







ALTITUDE CHANGE POINT LINE

All gen 45 Eath Poly III

MOD

Flight plan modification is in progress. Displayed values on the DEST page may not be accurate for the active flight plan.

TO T/C

Top-of-Climb in an ACTive climb mode.

(PRC		1/2)	
FROM	ALT	ATA		
TRM	FL 330			
78°	DTG	ETA	FUEL	
BLH 82°	50	1845z	18.3	
	71	1853z	17.6	
KIAH	1075	2104z FU	8.3 EL QTY	
1840z/ 25 DME	БNM IRS (L)) DN	18.9 //E	
TRM A11	6.20	MZB A1	17.80	

TO T/D and address to a subsyster

Top-of-Descent

If no STEP TO entry exists on the CRZ page and a path descent is available. Does not re-compute on a MOD page.

TO T/D ADVSRY (Discontinued in U5.0)

An advisory to top-of-descent if no STEP TO entry exists on the CRZ page and a path descent is not available. Automatic initiation of VNAV descent is not available. Upon reaching T/D, message DES PATH NOT AVAILABLE appears and VNAV disconnects to ALT HOLD. T/D point computed using Spd Des parameters, i.e. 1000' above DEST airport.

TO STEP POINT

To the Step Point if a STEP TO entry exists for the CRZ page.

TO E/D

To the End-of-Descent wpt, for an ACTive Path Descent; blank for a Speed Descent.

 KIAH
 245
 2104z
 8.3

 TO T/D
 FUEL QTY

 2039z/
 135NM
 10.7

 DME
 IRS (L)
 DME

 ABI A113.70
 LZZ
 A112.50

 KIAH
 135
 2104z
 8.3

 - TO T/D ADVISORY
 FUEL QTY

 2039z/
 135NM
 10.7

 DME
 IRS (L)
 DME

 ABI a113.70
 LZZ
 a112.50

 KIAH
 1135
 2104z
 8.3

 TO STEP POINT
 FUEL QTY

 1859z/
 180NM
 18.7

 DME
 IRS (L)
 DME

 SJN a112.30
 TUS
 a116.00

 KIAH
 1135
 2104z
 8.3

 TO E/D
 FUEL QTY

 2039z/ 85NM
 10.5

 DME
 IRS (L)
 DME

 CLL A113.30
 LOA A110.80

RTA PROGRESS - U4.0 & up

This page shows the RTA PROGRESS page before an RTA WPT and time constraint has been chosen.

To use the RTA function, designate a single waypoint in the flight plan and specify a Required Time of Arrival at this waypoint. A speed schedule to achieve an RTA at some waypoint can be activated through this RTA PROGRESS page.

The target speed schedule to meet the RTA is derived by finding the ECON mode Cost Index that results in the desired ETA prediction. The FMC will choose a CI from 200 to a minus 40 in an attempt to meet the RTA. Speed limits are defined by the PERF LIMITS page.

Entry of an RTA WPT and an RTA time at that waypoint activates the RTA mode and overrides the previous performance mode. Supplementary computations also display the earliest and latest arrival times possible at the RTA waypoint - called the RTA WINDOW. If an RTA is entered outside the RTA WINDOW, a message RTA UNACHIEVABLE will be displayed. The accuracy of the RTA function relies heavily on accurate wind forecasting for the route of flight. Therefore it is recommended that you enter the best wind profile available on the PERF INIT page, if using RTA through the climb phase, and on the RTE DATA pages for RTA calculations in cruise.

On the ground, it advises of pertinent times such as recommended takeoff time to meet the RTA.

In flight, it provides advisory data on progress of flight when in the RTA mode.

After passing the RTA wpt, the message SELECT MODE AFTER RTA appears. Check the CRZ page and make desired speed change.

To get out of the RTA mode, DELete the wpt that you placed in 1L of the RTA PROGRESS page. You may be left with a Manually entered cruise speed, so check the CRZ page for desired speed.



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RTA PROGRESS - U4.0 & up



PROGRESS 3/3 (2/2 for U1.x)



WINDS

- FMC winds are relative to True north.
- The following assumptions are made:
 - 1) The aircraft is flying straight and level with small (cruise) angle of attack,
 - 2) Sideslip is assumed to be zero,
 - 3) Vertical direction is assumed to be level this can be the source of substantial errors when the aircraft is not in level flight.
- FMC velocity errors, IRU attitude errors, and air data (onside to master FCC) true airspeed errors will affect the calculated wind. With Source Select

switch in BOTH-L or NORMAL, same value displayed on each CDU.

- If an IRS wind readout (on the ISDU optional equipment) reads significantly different than the FMC winds, this may be the first indication of failure (IRS system drift or FMC failure).
- The ND winds are relative to the north reference displayed on the map (MAG or TRUE)
- In a dual FMS installation, the Captain's ND displays FMC-L calculated wind and the FO's ND displays FMC-R calculated winds.



TUNING STATUS AND UPDATE MODES OF NAVAIDS

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Radio update mode, navaid ID, freq, and tuning status along with the IRS in use are displayed on the bottom lines. Navaid ID and freq should never be blank under normal conditions. When possible, only DME information is used from each radio. Blank when not being used for updating. Facilities must be co-located (<.1 arc-min.) Best pair is re-evaluated each 2 min. with DME-DME and DME-VOR modes.



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The use of GPS data for navigation depends on the certification level, flight phase, and pilot inhibits (NAV STATUS page). The certification determines the following GPS ratings: Primary, Supplemental, and Advisory.

Primary: The GPS data may be used in all flight modes and on the ground.

Supplemental: GPS data may be used if checked against other sole means certified nav data sources. VHF is the sole means method while enroute domestic and in terminal areas; IRS is the sole means for oceanic. If VHF radio data is unavailable in terminal, approach, or enroute flight, GPS updating is allowed without affecting actual nav

performance. Otherwise, the VHF data is used as a check of the GPS data. In an oceanic environment, IRS data is used for the check.

Advisory: GPS data is only displayed for information.

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The GPS has 3 segments; the satellite, the user (aircraft), and the control.

The satellite segment is a group of 24 satellites orbiting at 11,000 nm above the earth; three are spares. Each satellite makes an orbit once every 12 hrs. The satellites continu-

ously transmit radio signals with nav data, range code, and the exact time. The GPS sensors require at least 4 satellites to be in view in order to calculate position. Use of a fifth satellite allows the sensors to use different combinations of four to verify the truth of the information. This important integrity check, known as Receiver Autonomous Integrity Monitoring (RAIM) is required in order for the FMC to use the GPS information. As satellite constellation geometry varies, the radius of position accuracy confidence varies also. Given this, the FMC will weigh the GPS information relative to the other available position sensors. Good satellite geometry results in an FMC position that is almost entirely GPS position; poor satellite geometry results in an FMC position that is a blend of radio, IRS and GPS.

The user segment is the GPS receiver unit on the aircraft. It receives of course, the GPS signals.

The control segment has control and monitor stations on earth that continuously monitor and track the satellites. The control segment monitors and corrects satellite's orbits and clocks. The satellites use control rockets to correct their orbits.

The control segment has one master control station and 5 monitor stations (Ascension, Diego Garcia, and Kawajalein Islands, Hawaii, and COS. The master control station is in Colorado Springs, CO and has an atomic clock that is the reference for the GPS.

Verification of the GPS satellite signals is required for any route in which GPS is the only source of navigation sufficiently accurate for the intended route. For RNP operations, availability of adequate navigation aides, or GPS satellite coverage must be assured for the intended route. Your dispatch office will provide you with this GPS prediction.

> GPS receivers use the principle of ranging to measure the distance between the receiver and the satel-

lites. The receiver always knows the location of the satellites in their orbits in memory.

The receiver measures the time it takes for a radio signal to go from a satellite to the a/c; it then calculates the distance to the satellite. The receiver uses 1-way ranging and must know exactly at what time the satellite sent the radio signal. The receiver compares

the satellite signal to a signal that the receiver makes at the same time as the satellite. The difference between the 2 signals (\wedge t) is the time the satellite signal took to get to the receiver. Each satellite has an atomic clock; all satellites have precisely the same time. The receiver calculates the accurate time from the difference between the receiver time and the GPS time.

To calculate the a/c position (lat, long, altitude) and \wedge tBIAS, the receiver must know the position of at least 4 satellites. The receiver then measures the distances to all the satellites at the same time and computes the nav solution.

The dual GPS sensor units are installed in the upper forward part of the fuselage near the two, nearly flush, GPS antennas. Position information is provided to each unit's onside FMC, just as the other position sensors currently on the aircraft (IRS, DME, VOR/DME, LOC/DME). The result is a very accurate FMCS.

Loss of GPS signal will turn the clock display, if in UTC, to dashes if the clock is in UTC mode. Loss of signal does not illuminate the GPS light on the overhead.

GPS RELATED MESSAGES

GPS Related Messages

IRS NAV ONLY is displayed when the ANP is larger than the default RNP. Default RNP numbers are automatically assigned by the FMC for the phase of flight (Ref: RNP-default values)

UNABLE REQD NAV PERF-RNP is displayed when the ANP is larger than the manually entered RNP (with GPS operations enabled, the FMC allows a manual entry of RNP on the ACT RTE LEGS page 1/

x or POS SHIFT 3/3). When on approach this message is also displayed in ambertext across the EHSI Map.

Note: Your SOP may not allow manual entry of RNP.

VERIFY POSITION is displayed when the difference between GPS and FMC position exceeds the RNP.

VERIFY RNP is displayed when the default (i.e. phase

of flight based) RNP changes and the manually entered RNP exceeds the new default RNP value.

VERIFY RNP VALUE is displayed when a manual RNP entry is greater than the default RNP value.

Astronauts & engineers: Best List and Class

From the best navaid list (10 navaids closest to aircraft's computed position), the FMC determines the best navaid pair as a function of the line-of-position (LOP) crossing angle. The crossing angle of the LOPs must lie between 30° and 150°. The best navaid pair is defined as the combination which produces a crossing angle closest to the ideal value of 90°. Reselection of a best navaid pair will normally occur after the selected pair no longer meets the range and geometry criteria. The closer to 90° the smaller the ANP. You can witness all this action by viewing the RDMI.

The FMC uses a coordinated search pattern. It constructs a rectangle about the a/c made up of 5 latitude bands - a band is 140 nm in width. It searches the rectangle in this manner - the first band to the north, then first to south, the second band to the north, then the second band going south, etc. All this searching takes time, and has caused problems with some U1.x computers. U1.6 will limit this search to 3 bands below 15,000'. This will shorten the search time, thereby solving this "restart" problem some operators are experiencing. Above FL180, only H class navaids are used. Above 12000' and below 18000' MSL, H or L class within 40 nm; 12000' and below, H or L class within 40 nm, or T class within 25 nm. U1.4 and U5.0 and up have increased these distances to 200 nm. On EFIS a/c, they can be identified up to 390 nm. Navaids of unknown class are used at any altitude. DMEs associated with ILS treated as L and used below 12,000' If one of the two DME receivers has been switched to MANUAL, the FMC will attempt to use the manually tuned DME station to 200 nm regardless of class, and to find a complementary DME station that provides an acceptable LOP crossing angle.

All of the above messages, with the exception of VERIFY RNP VALUE message, are *alert* messages when issued on the CDU scratch pod. and will be accompanied by an amber FMC annunciator on both pilot instrument panels. VERIFY RNP VALUE message is an advisory message and will not be accompanied by the amber FMC annunciator.

These messages can be cleared by the CLEAR key, or the condition being corrected. In addition,

> to avoid nuisance messages, all of the above messages are inhibited when one of the following is true:

> 1. VOR/LOC mode is engaged (another system is controlling the lateral path).

2. VOR/LOC mode is armed and LNAV not engaged (LNAV not used to capture VOR/LOC).

3. VOR/ILS mode is selected on one EHSI (Raw radio data displayed for position crosscheck).

Astronauts & engineers: XTK ERROR

XTK ERROR on the U1.x software references the leg without the turn. It's similar to the steam gauge HSI. As you approach an enroute navaid, you tune the next station and select the inbound course. Initially, the course bar is slightly off center. As you approach the center of the airway, the course bar centers. If you watch the course bar (non EFIS) you will notice that as you sequence fromone leg to the next, as soon as yu start the turn (in NAV), the HSI's course pointer switches to the next leg and moves slightly off center. If you check the XTK ERROR display on PROGRESS 2/2, you'll see it reflects the deviation of the course bar.

EFIS software does not work in this manner. The XTK ERROR will remain at zero because the FMC builds a curved fly-by course as it sequences each wpt. The curved magenta line reflects this design.

Astronauts & engineers: Correction Rates

The Best position is used to slew the System position. The final filter position correction is rate limited based on the phase of flight to insure smooth changes to the system position used for guidance.

Phase

Enroute

Terminal

Approach

These limits are:

Update Type Any update Any update Localizer update Manual shift

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Limit In NM / Min

0.5

2.0

8.0

No limit

	ACT	DTC	IFCC		1 / 4	
12	ACT	RIE	LEGS		1/4	
	146°	1	1NM			
1	AMIPI		en 19	792/F	L370	
18	148°	5	1NM			
	LULIS		h. 84	792/F	L370	
	149°	6	4NM			
	MTD	ත ගංගාවමා		792/F	1370	
	1570	2	5NM .			
	חוזוח	-	31111	792/F	1370	
	1570	1 2	0 1114	152/1	2570	
	15/°	12	O IN M	702/5	1 2 7 0	
	PENSO			19211	L370	
	RNP/AC	TUAL				
	2.00/2.	51NM		RTE D	ATA>	
	UNABLE	REOD	NAV	PERF-	RNP	

May 01

NAV STATUS - U7.0 & up

You get to this page by:

- POS SHIFT 3/3 page NAV STATUS prompt (LSK 5R).
- INIT REF page NAV STATUS prompt while in flight.
- PROGRESS 1/3 page NAV STATUS prompt (LSK 6R).
- NAV OPTIONS 2/2 page, then go $\left(\begin{array}{c} PREV \\ PAGE \end{array} \right)$ or $\left(\begin{array}{c} NEXT \\ PAGE \end{array} \right)$.

This information is common to both types of DME interrogators. • FAIL is displayed (small font) in GPS and IRS displays Small font displayed if tuned but • GPS display blanked if inhibthe ident field and frequency is not being received (no valid data). blank if no frequency being reited. · Large font displayed (no high-• (2) Dual FMC installation, indiceived or freq status is FAIL lighting) if being received but not cates that both IRSs(or GPSs) used in navigation solution. WARN. are being used in the nav solu-· Ident field blanked and fre-· Large font with highlighting if quency alone is displayed if no tion. being used in navigation soluident for the tuned frequency. tion. NON SCANNING DME · DME-DME updating For single FMS with stan-If the tuning mode is agility, NAV STATUS 1/2 dard or agility DME receivers then the agility tuned frequen-VOR - L ILS - R RBL A 115.70 ANP should range from 0.25 up QED A 113.6 cies and their corresponding DME - R DME - L to 0.35 or so, maybe even 0.40. identifiers are displayed simul-QED 113.6 RBL 115.70 This remains the same for a dual taneously. FMS with standard receivers. The data for the nearest sta-Agility Tuning For VOR/DME updating, the tion will be displayed above the NAV STATUS 1/2 range will be 0.3 to 0.6 or so VOR - L VOR - R other station. OAK M 116.8 depending on distance to the DME - R DME - L VOR.

SCANNING DME -

OAK

116.80

The FMC will generally be more accurate even if aircraft geometry does not change because the ability to acquire slat ranges for 4 groundstations instead of only 2 can reduce the uncertainty (ANP) by up to 30%. (Multiple observations of similar data reduces the uncertainty.)

A scanning DME receiver can monitor 5 DME stations at the same time. The 737 has two types of installations available, *single* and *dual*. Single scanning DME is usually installed with the older U3 thru U6 FMCs. This aircraft has 3 DME receivers, one for each pilot radio head and one for the single FMC to use for updating. On this installation, the FMC will use channel 2 and 3 for FMC autotune operation and 1, 4, and 5 are not used.

Expect ANP in the range of 0.17 to 0.25.

The last 4 channels do not display A, M, or P, since they are always automatic. The dual scanning installation is normally used with dual FMC installations, U7.2 or 8.1 and up. In this type of installation, there are only 2 DME receivers on the airplane. Channel 1 on each scanner is dedicated to the pilot radios, channel 2, 3, 4, and 5 on each scanner are available to the FMCs for use in radio updating.

OED

RBL

113.60 115.70

Expect ANP in the range of 0.13 to 0.20

Agility tuning and VOR/DME updating are inhibited.



The first is for the pilot, manually tuned to SEA. Manual tuning does not inhibit scanning DME ops.
The next 4 are reserved for the scanning DME. Each radio may pick up to 4 stations. The Primary FMC determines which ones to use, and allocates

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the stations for updating to both FMCs.

Displayed in order of the directed freq. number.

NAV OPTIONS - U7.0 and up

- REF NAV DATA page NAV OPTIONS prompt (LSK 6R).
- NAV STATUS page then (NEXT) or (PREV PAGE)

Allows inhibiting use of specific navaids in navigation solution.

Provides a means of selecting which sensors are available for the navigation solution.

• Allows entry of up to four navaids to be inhibited from position updating, (Auto, Procedure, or Manual modes).

- Overwriting or DELeting clears previous entry and removes previous inhibition.
- Selection automatically cleared after landing.
- VOR entries not allowed if VOR updating is OFF.
- The example shows an entry to inhibit the Mexico City DME from updating.
- LOC updating cannot be inhibited.



Astronauts & engineers: Localizer Updating

U5.0 and up: During final approach, the FMCS can use a manually tuned front course localizer and DME for updating. Localizer updating has priority over DME-DME updating. Localizer deviation may be applied in addition to the DME update. Note: An LDA cannot be used to update the FMC position.

The following criteria must be satisfied before the FMCS will use localizer deviation:

- The tuned ILS frequency matches the frequency in the nav database for the approach programmed in the LEGS page.
- Aircraft altitude must be less than 6000 above station elevation.
- Aircraft must be within 20 nm of the localizer antenna (Nav Data Base) for a front course approach (12 nm for a back course approach).
- Aircraft must be within 25 degrees of the localizer centerline.
- Aircraft track angle must be within 45 degrees of the localizer inbound course.
- Localizer deviation must be less than 1.25 dots after having been less than 2.0 dots for at least 5 seconds prior to the start of localizer updating.
- · LOC updating terminates when crossing over or abeam the runway threshold.

Astronauts & engineers: Bad Navaid List

The first operation in creating the navaid allocation list is identification of the unusable navaids. This is determined by identifying navaids that are giving bad or no data over 4 consecutive update cycles. This bad navaid list is shared by each FMC in the dual configuration. Each time an FMC finds a new unusable navaid, that update to the bad navaid list is transmitted to the other FMC. The bad navaid list is capable of containing the 10 most recent DME stations, or 5 most recent VOR/DME stations. Under some circumstances, the bad navaid list is purged so that nearby stations may again be selected and their validity rechecked. The bad navaid list is also purged whenever a navaid receiver is determined to be invalid. In addidition, the bad navaid list is purged on the ground.

NAVIGATION CHECK - Single FMC 737 - No GPS

Dec 95

Operating the FMS in areas where navaids have alignment errors can result in lateral navigation errors of significant magnitude. A map shift may be invisible and everything could look fine; it depends on the relative geometry of the aircraft heading vs. the nav error. One indicator of an invisible map shift

the display of the IRS indicator arrows both pointing the same way at the same distance. A map shift in a non-EFIS airplane would show up as a jump in the HSI course bar.

Characterization of facilities potentially radiating unvalidated or incorrect information

- a. Signals are sometimes radiated for test purposes (prior to completion of flight inspection).
- b. A suspect facility can be radiating *out of tolerance* with the ident not yet removed.
- c. A facility may be radiating *out of tolerance* during maintenance or installation, with no ident or a T-E-S-T ident. (The FMS does not check for a valid identification before use.) A facility will usually be NOTAMed if in maintenance. It may not be NOTAMed if it is related to a previously decommissioned facility, and the new facility has not yet been promulgated for service.
- d. The FMC data base may be incorrect because a facility has been moved to a new location, a frequency has been changed, or discrepancies exist in coordinate reference.
- The facility may be radiating, but is unmonitored (e.g. monitors have failed or are not attended). Integrity could be lost during this condition.
- f. A facility may be radiating bad azimuth information in certain quadrants, or along certain radials, even though commissioned and monitored.
- g. A facility may not be colocated. To be used for the nav solution, the VOR and DME facility must be colocated; i.e., the lat/long of the two must not differ by more than 0.1 arc-minute.

Recommendations

- a. Ensure a system exists at your carrier where problem navaids are flagged.
- b. Check NOTAMS for known navaid problems.
- c. When known facility problems exist, use this information to INHIBIT this particular navaid using the REF NAV DATA or the NAV OPTIONS page.
- d. If a faulty update has occured just after takeoff (example, VERIFY POSITION message with a map shift), navigate with raw data; you should not direct your attention to the computer while in this phase of flight.
- e. If known bad facilities are being automatically selected and used by the FMS, manually tune one side to force the system off a bad facility.
- f. The governing body should seek a better way to flag facilities that are radiating for maintenance or test purpose, or are suspect, to aid timely

airline and crew response.

- g. A search swath for NOTAMS should include navaids within 200 nm of course.
- h. Advise the governoring body and your airline immediately when known problems are found.
- i. Any time you receive the message VERIFY POSI-TION, be alert for a possible course deviation.

The IRS NAV ONLY message is quite common and normally indicates a lack of radio updating of the FMC POSition, not that the airplane is off course. The normal flight crew reaction to this message is three-fold. First ensure that both nav radios are in a configuration that will allow the FMC to auto-tune. Second, check the effectiveness of the updating by monitoring the RADIO position on the POS SHIFT page; if the airplane is operating in an unreliable navaid environment, consider shifting the FMCS position to the referenced IRS position - (L) on the PROGRESS, POS SHIFT, or NAV STATUS. An FMS can be forced off a bad facility by manually tuning a different valid facility on one side, thus forcing consideration of a new pair of facilities, but the most effective means of avoiding an unreliable navaid is to INHIBIT that navaid prior to entering its coverage. Finally, compare raw data position to the FMCS position.

If the navaids are questionable and in a radar environment, actual position should be confirmed with the controller. Use the most accurate navigation system available to ensure compliance with the desired/required navigation track. This may require the use of conventional VOR/ADF nav.

If one of the nav heads has been switched to MANUAL, the FMCS will attempt to use the manually tuned DME station and to find a complementary DME station that provides an acceptable crossing angle. It may result in a less desireable pair than it would have chosen. When this is not possible, the DME interrogator in the AUTO mode may operate in a frequency-agile submode in order to preserve the primary dual-DME nav solution. This is agility tuning.

Theoretically, agility tuning is as accurate as DME-DME tuning. Latency of data should be considered however, since it is held for five second intervals as the frequencies are cycled. Agility tuning is not desireable when both radios are available for DME-DME tuning, and pilot action may be required to force a radio out of the agility tuning mode and back to the DME-DME mode.

For example: Both nav heads are in AUTO. The First Officer's nav radio has been declared invalid three consecutively tuned navaids on that receiver all produced invalid data. The Captain's radio now agility tunes.

Action: If in a phase of flight that has a low work load and nav accuracy is not compromised, start your timer to check whether or not the invalid radio is reconsidered as it should be, within 8 minutes. If it is not, you can intervene manually, in two ways. The easiest is to dial a local VOR/DME in the FO's side (consider LOP) and press MANUAL on that side. This forces the FMC to reconsider this reciever. The second procedure is to dial 108.00 in the Captain's radio and press MANUAL. The First Officer's radio should start agility tuning. Press AUTO on the Captain's side. Both radios will now contribute to the nav solution in a DME-DME mode. If a position error existed, you will see the RADIO position on the POS SHIFT page settle down to around .1-.2 nm vector.

Note: It is impossible to manually check the FMC POSition accuracy within the req'd limits for an approach without RNP equipment.

In areas of questionable navaid integrity, check the FMS position for accuracy prior to entry into the teminal area.

Manual position check:

- a. Enter a VOR identifier into one of the FIX pages; preferably a navaid that's off to one side.
- b. Manually tune the same VOR and press the nav switch to MANUAL. Your SOP may require selecting a VOR mode and centering the course bar.
- c. Compare the RDMI pointer (or course bar) and DME to the bearing and distance on the FIX page. The DME of the FIX page will always be a little shorter than the DME on the RDMI due to the fact that RNAV distance is on the earth's surface and not slant range; the bearing should be the same. Practically speaking, the FIX page DME changes to the next lower number at the half mile; that is, when the distance changes from 25 to 24, you're 24.5 from the FIX. With practice you can tell if the error is less than a mile.
- d. If you are flying directly to the manually tuned station, as may be the case when using raw data as a back-up in mountainous terrain in South America, the EHIS Map distance may be compared to the raw data DME. You can get a very good accuracy check since both displays are in tenths of a mile. Again, allow for slant range.

The manual position accuracy check described above requires that your RDMI needles point to the tuned navaid, and not the active waypoint (an option). Choose a navaid that the FMC is using for updating (displayed on the PROGRESS or NAV STATUS page) and enter its 3 letter ID on a FIX page. Now compare the FIX page bearing *and* distance with the RDMI bearing and distance.

Map check: EFIS pilots have a very quick way of checking Map accuracy, however this method works well only if updating is occuring from navaids close to the aircraft (40 nm range). In the AUTO mode (or MANUAL with an entered VORTAC) press the VOR/ ADF Map switch. The strobes radiating from the vertex are raw data. The navaid symbols are computer generated from the nav data base. Strobes penetrating the center of the navaid symbols indicate an accurate Map.

When an FMC navigation error is detected, either assist the computer in correcting the error (POS SHIFT) or continue the flight using conventional VOR/ADF navigation procedures.

The FMC is designed to reject unreliable navaid data during FMCS position updating, even after takoff - one of the most vulnerable times. (The rwy update feature lessens the chance of this occurance). However, in certain conditions, especially during a VOR-DME update, navaids which are in error may satisfy the "reasonableness criteria" and provide the FMC with an inaccurate RADIO position. Trouble shoot by immediately checking the POS SHIFT page and performing a shift to the referenced IRS. Note the navaid that may have caused the problem and inform the proper authorities.

The single FMC is not certified as a *primary* means of navigation. It is certified to navigate accurately only in conjunction with an accurate VOR/DME environment. The dual FMC installation in U7.2/8.1 meets the criteria for sole means of nav.

If radio navaids are available:

- a. Ensure that one nav radio is in the AUTO tuning mode so that the FMC can update its position using the DME-DME method. PROGRESS 1/1 (6L and 6R) or NAV STATUS will indicate whether or not auto-updating is in progress.
- b. The radio updating that is underway should be of high quality. Using the POS SHIFT page, compare the FMC System position to the RADIO or DME/DME position. A figure less than .2NM is desireable
- c. Accomplish a *Manual check* prior to entry into the terminal area.
- d. You may compare the FMC System position to the IRS positions, but expect the distance to grow in an updating environment since the IRSs will drift as a function of time. You may use the formula 3 + 3T where T is time since last full alignment.

FLYING ROUTES WITH OCCASIONAL LAPSES OF UPDATING

The following procedure is designed for a single FMC installation for the 737 flying a route over an area such as the Gulf of Mexico, where the airplane is outside the range of radio updating for a short period of time.

PREFLIGHT

a. IRS Drift Rate Check:

If IRS drift rates for previous flights have been recorded in the log, verify that no two consecutive flights have a recorded groundspeed of 20 kts or more or that vector distances do not exceed 2 nm. The drift rates for the IRSs can be found by following: INIT REF INDEX / MAINT> / <FMCS / IRS MONITR>. Ref: IRS MONITOR

b. Pre-Departure IRS Checks: Go to POS REF 2/3. Check groundspeeds are less than 2 kts. and

ensure that the FMC POSition and IRS positions are all the same as the coordinate used for initialization. If not, do another full alignment. The author recommends using the actual gate position prior to flights intended for areas of poor nav coverage

because use of the POS SHIFT page may be required. If a manual entry is made the other pilot must verify the entry using a separate doucument.

ISLAND DEPARTURES

In cases such as an island takeoff, where only one navaid is available, there has been a history of problems with a VOR/DME update slinging the FMC off into large errors. In U6 software and below, sometimes these errors were too large for correction at coast-in. During Preflight, either inhibit that navaid or manually tune 108.00 in both receivers until more than 50 nm from the navaid.

PRIOR TO COAST-OUT

- a. Check for DME-DME radio updating,
- b.Perform a manual position accuracy check (described on page 13.12) prior to loss of navaid updating, except repeat the procedure for the other VOR.
- c. Verify IRS (L) is the referenced IRS line 4C in the graphic. If it is not, it has drifted out of tolerance and the FMC has chosen the right. The left is the referenced IRS at start-up.
- d. Record the offset distance each IRS is from the FMC POSition. This offset is the difference between that IRS and the FMC POSition. This is simply a way to monitor the operation of the IRSs and may assist in determining which IRS is the most accurate. If one IRS is several miles away from the FMC POSition during DME-

DME operation, take note. This may be an early indication of an errant IRS. You would not want to shift your FMC POSition to this IRS if the need arose.

e. If you're flying U7 software or above, note the RNP vs. ACTUAL data.

ENROUTE

a. FMC / IRS Comparison Check

When the IRS NAV ONLY message appears, check the offset from the referenced IRS again. Perform this check and at each subsequent waypoint while in IRS NAV ONLY. This is a quick and easy check and you will get a feel for how the IRSs are performing. With software versions 1.5, 1.6, and 5, the FMC will maintain this fixed offset from the referenced IRS. This

fixed offset, (2.1 nm in the graphic)

POS SHIFT will not change during flight in IRS NAV ONLY. This means that the FMC follows the referenced IRS until updating resumes. With versions 1.3 and 3, 4, 7, and up, the velocity errors are still active and the difference may continue to grow.

- b. Check the RNP vs. ACTUAL data. ACTUAL error will grow during periods of IRS NAV ONLY.
- c. During periods without Radio or GPS nav input, (IRS NAV ONLY), the only true way to perform an accuracy check is to compare the FMC POSition with some identified landmark, i.e., a waypoint you can see out the window. The IRSs are a good next choice, but as we know, they tend to drift. When you compare the FMC POSition to an IRS position, the FMC in LNAV will always pass over the waypoint whether it has a nav error or not. In extreme cases, consider ground mapping with the radar or a position check with ATC.

COAST-IN

- a. After the FMC has been auto-updating for a few minutes, go to the POS SHIFT page and note the offset that the newly updated FMC POSition is from the referenced IRS.
- b. Perform a manual position accuracy check as outlined on the previous page.
- c. If the offset seems greater than it should be, perform a POS SHIFT to your favorite IRS. The FMC will start updating if good navaids are present. Ref: POS SHIFT Exercise.

POSTFLIGHT

a. IRS Monitor Check

Check the IRS drift rates and groundspeeds. In airplanes that are used for overwater routes or those going to sparse navaid territory, record if SOP.

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IRS (L)

DUAL FMC - ETOPS QUALIFIED B 737

This section concerns the use of 2 engine aircraft during Long Range Navigation (LRN). This usually means Extended Twin Engine Operation (ETOPS) over water or land in areas where no suitable airports exist.

ETOPS, also referred to as Extended Range Operations (EROPS) is a term to describe Extended Range (ER) flights of twin engine aircraft. An ER flight is conducted over a route that as some point, is further than 60 minutes flying time at single engine cruise speed. The distance to an adequate enroute alternate airport from any point along the intended route must be covered within the approved diversion time using single engine cruise speed (still air and ISA conditions). Diversion times are approved by the governing body and range from a low of 60 minutes to 75, 90, 120, 138, and finally 180 minutes (3 hrs.).

The ETOPS segment of the flight is commenced when the aircraft is more than 60 minutes from a suitable airport. This is called the Extended Range Entry Point and will be defined on your Flight Plan (FP).

A flight leaves the ETOPS portion of the flight when within 60 minutes of an adequate airport. This is called the Extended Range Exit Point, and again, will be defined on the FP.

DEVELOPER DEVELOPER MIENT



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You are proceeding eastward at FL 370 direct to College Station for the CUGAR 4 arrival. 90 nm west of College Station, ATC : "Avro 642, cross 10 east of College Station at and maintain FL180".



Dec 93







FIX INFO



BEARING ENTRY

For a downtrack **bearing** fix in U5 and up, a slash is not req'd.

A bearing entry results in a green dashed radial line being displayed on the EFIS Map.

If more than one intercept point exists for a selected radial, the data is displayed for the one nearest the a/c.

The bearing data is magnetic.



FIX INFO

May 01

DISTANCE AND BEARING ENTRIES

This example depicts use of a FIX page to create a distance based wpt with a predicted altitude check,
and to create a bearing display for a special engine-out procedure.The departure is the PRADO from rwy 26 at Ontario, California.LEGS page after

selection from database. · After takeoff turn left to cross 6 nm northwest ACT RTE LEGS 1/3 of PDZ VOR at or below 4000'. 256° HDG 0.3 NM (1350)210/1350A • At 400 ft, select LNAV. Hand fly the airplane 126° PDZ 11 NM to the magenta line and engage the autopilot. 250/2700A • At 1000 ft AFE select VNAV; all altitude 1309 3.0 NM 250/4500 9000 WERLE constraints will be met. 1319 3.8 NM ARNEE 284/11000B Turn left 131° 6.8 NM within 1 nm NIKKL 297 / 6000A RNP / ACTUA EXTENDED 1.00/2.13 DATA > 078°. PARADISE 112.2 PDZ At or below 4000' The special engine out procedure is - 258° to hold east of Paradise on the 078° At or above 2700' WERLE radial, right turns. At or above 4500' At or below 9000' Display the hold radial for situtional awareness by entering the inbound ARNEE course of 258 on the FIX page. At or below 11000' NIKKL To THERMAN **FIX INFO** 1/2 (Thermal Transition) At or above 6000' RAD / DIS FR PDZ 322/9.0 RAD / DIS DTG ALT ETA • Build the 6 nm wpt northwest of Paradise 305/6.0 2328.9 z 5.3 6302 by entering "slash six" in the FIX page. 258 Place this wpt in the proper sequence in the LEGS page (PDZ01) and enter 4000B. LEGS page in process • Notice the predicted altitude of 6302 on the of being MODified. MOD RTE LEGS FIX page. If a reduced climb power is 1/4 256° HDG 0.3 NM selected (CLB-2), the intermediate level-off (1350)210/1350A will be more smoothly attained, such as 126° 5.0 NM PDZ01 250/5025 depicted on the LEGS page (5025) 126° 6.0 NM 33 PDZ 250/2700A <CTR> 3.0 NM 130° WERLE 250/4500 9000 0 1350F1 131° 3.8 NM ARNEE 284/11000B \square MAP CTR <ERASE STEP > TCAS 4000B PDZ01 If cleared to climb "unrestricted", delete 4000B at LSK 1R or the airplane will level-off if in VNAV. 078 PDZ 258 N ACT RTE LEGS 1/3 NERL 126 2.7 NM PDZ01 250/4000B 6.0 NM ARNEE 1269 6.0 PDZ 250 / 2700A 130° 3.0 NM WERLE 250/4500 9000 1319 3.8 NM ARNEE 284/11000B Leading Edge Libraries © 148





VNAV PATH CONSTRUCTION AND MISSED APPROACH POINT POSITIONS

Thanks to John Kasten and Jim Terpstra of Jeppesen for the text and to Jeppesen for the graphics.

General VNAV Path Rules:

VNAV angles are projected backward from 50 ft above the Landing Threshold Point (LTP) to the altitude at the FAF allowing capture of the VNAV path without penetrating below the intermediate segment altitude. VNAV Path determinations may be influenced by many factors, including the existence of a stepdown fix between the FAF and the LTP. VNAV angles are generally provided for straight-in landings only. The value of 50 ft above the LTP is a default value which may be adjusted to meet operational requirements.

VNAV Path Provisions:

When the civil aviation authority provides a VNAV angle, the specified VNAV angle or angles will be used.

When a civil aviation authority does not provide a VNAV angle, an angle will be calculated by a database supplier using the following criteria:

- VNAV to LTP+50: The VNAV angle is to be calculated to the FAF, using a point 50 ft above the LTP elevation, the FAF minimum altitude, and the distance between these two points.
- Guidance below MDA: VNAV Path is designed to provide vertical guidance below the MDA to the LTP +50 ft. Descent below the MDA is accomplished in VMC.
- Shallow Descent Gradient: If the calculated VNAV angle is less than 2.75°, it will be raised to a minimum of 3°. In some cases, this could mean that the pilot would maintain level altitude after passing the FAF until intercepting the VNAV path.
- VASI/PAPI: The VNAV angle should not be less than the angle of the VASI/PAPI. If the VNAV angle is less than the VASI / PAPI angle, the VNAV angle will be raised to a maximum of 3.77°. For 3-bar systems, the angle and the TCH for the upwind bars will apply.
- Step Down Fixes: If the calculated VNAV path from the LTP +50 ft to the FAF passes below the minimum altitude of any step down fix the VNAV angle will be increased to pass at or above all step down fix minimum altitudes. In some cases, this could mean that the pilot would maintain a level altitude after passing the FAF until intercepting the VNAV path. Note: Step down fixes are not included in the database.

VNAV Angle Raised Above FAF: When the VNAV angle is raised to the minimum of 3° or when the VNAV angle is raised to ensure clearance at a step down fix, the extended VNAV path will likely pass above the FAF minimum altitude. Coding Considerations for VNAV path for straightin:

VDPs: VNAV angles will not be less than the angle fro the VDP to the LTP +50 ft.

NDB vs ILS Approach Angle: When an NDB approach is coded from an LOM, the VNAV angle, the VNAV angle doesn't necessarily match the glide slope angle of the associated ILS. It is usually a slightly higher angle for the NPA.

General Rules for Missed Approach Point (MAP):

The MAP will be the MAP as shown on the nonprecision approach procedure by the civil aviation authority. Note: For coding purposes, the MAP will not be relocated to the point where the VNAV path intersects the MDA plane.

Location: If the intent of the procedure designer is to locate the MAP at the LTP and it is within 0.1 nm radius of the LTP, the MAP will be defined at the LTP. Note: If the source document states that the MAP and the LTP are not at the same location even if the distance is 0.1 nm or less, the MAP will not be placed at the LTP.

Identification: The FAA has issued a policy statement which clarifies the identification of fixes at LTPs.

Landing threshold points used as missed approach points will not additionally be given a wpt name.

- Wpt names currently assigned to landing threshold points used as missed approach points will be withdrawn.
- Missed approach points not at the landing threshold point will be given a wpt name.

Other Coding Considerations: The FAA has issued a policy statement which clarifies the identification of fixes at navaid locations.

Navaids used as fixes in GPS procedures will not additionally be given a wpt name.

Wpt names currently assigned to navaids used as fixes in GPS procedures will be withdrawn.

GPS procedure fixes not at a navaid location and not at the LTP, will be given a wpt name.

Along Track Distance (ATD) fixes do not have names and will not be named.





FAF to MAP at LTP with straight-in landing: If MAP is at LTP or within 0.1 nm of the LTP, MAP is at LTP.

A VNAV angle, calculated from LTP +50 ft to the FAF altitude, raised to an optimum angle of 3.0 or to an angle matching the VASI angle is provided.







FAF to MAP at LTP with straight-in landing: If MAP is at LTP or within 0.1 nm radius of the LTP, MAP is at LTP. A VNAV angle, calculated from LTP +50 ft to the FAF altitude is provided.



FAF to MAP at LTP via a stepdown fix with straight-in landing:

If MAP is at LTP or within 0.1 nm radius of the LTP, MAP is at LTP.

A VNAV angle is calculated from LTP +50 ft to the FAF altitude.

If the VNAV path would pass below the stepdown fix altitude, a VNAV angle is calculated from LTP +50 ft to the stepdown fix altitude and is provided for the complete final approach segment.

FAF to MAP at LTP via a stepdown fix with straight-in landing:

If MAP is at LTP or within 0.1 nm radius of the LTP, MAP is at LTP.

A VNAV angle is calculated from LTP +50 ft to the FAF altitude.

If the VNAV path would pass above the stepdown fix altitude, a VNAV angle from LTP +50 ft to the FAF altitude is provided for the complete final aproach segment.

FAF to MAP beyond LTP with straight-in landing:

If final approach segment crosses LTP or within 0.1 nm radius of the LTP, an LTP waypoint ([RW30] in illustration) is included in final approach segment coding prior to the published MAP.

A VNAV angle, calculated from LTP +50 ft to the FAF altitude is provided. Stepdown fix rules apply.

VNAV PATH CONSTRUCTION AND MISSED APPROACH POINT POSITIONS



Altitude assigned at the MAP wpt is computed using the calculated VNAV angle. The LTP is not included in the coding as a wpt.

No LNAV or VNAV is provided from the MAP to the LTP.

Stepdown fix rules apply.

FAF to MAP before LTP with straight-in landing:

The MAP is at the government source location. A VNAV angle, calculated from LTP +50 ft to the FAF altitude is provided. Altitude assigned at the MAP wpt is computed using the calculated VNAV angle. The LTP is not included in the coding as a wpt. No LNAV or VNAV is provided from the MAP to the LTP.

Stepdown fix rules apply.

FAF to MAP beyond LTP with straight-in landing. Final approach segment NOT within 0.1 nm radius of LTP: Where the final approach segment crosses the

Example Eight

VNAV 3

VNAV 3.30

Example Seven

MASON

MASON

extended runway centerline outide of 5,200 ft of the LTP, but with an offset of 500 ft or less at a point 3,000 ft or less fro the LTP. An LTP abeam position wpt ([AB29] in illustration) is

ncluded in the final aproach segment coding. The point is calculated at a location on the final approach track where a line from the LTP intersects the track at 90°. This point serves as a VNAV aiming point and facilitates VNAV down to the LTP.

The altitude for the abeam position wpt will be equal to the LTP +50 ft.



A VNAV angle, calculated from LTP +50 ft to the FAF altitude is provided with the abeam wpt information. Stepdown fix rules apply.

VOR

VNAV PATH CONSTRUCTION AND MISSED APPROACH POINT POSITIONS

FAF to MAP beyond LTP with straight-in landing.

Final approach segment parallel / near parallel to runway alignment: Where the final approach segment never crosses the extended runway centerline but is more than 0.1 nm offset from the centerline at a point no greater than 5,200 ft from the LTP.

An LTP abeam position wpt ([AB27] in illustration) is included in the final aproach segment coding. The point is calculated at a location along the final approach track where a line from the LTP intersects the track at 90°. This abeam point serves as a VNAV aiming point and facilitates VNAV down to the LTP.



The altitude for the abeam position wpt will be equal to the LTP +50 ft.

A VNAV angle, calculated from LTP +50 ft to the FAF altitude is provided with the abeam wpt information. Stepdown fix rules apply.



alignment criteria.

The MAP is other than the LTP and is coded. The LTP is not included in the coding as a wpt. No LNAV or VNAV is provided from the MAP to the LTP. (Note: Some FMS may provide lateral guidance based upon an extended inbound course through the MAP.)

A VNAV angle, calculated from the LTP +50 ft to the FAF altitude is provided.

The altitude assigned to the MAP waypoint is calculated using the calculated VNAV angle. Stepdown fix rules apply.





[MA230] VOR MA230 5.0 **Example Thirteen**

FAF to MAP other than LTP with circling-toland minimums, not aligned with the runway. The MAP is other than the LTP and is coded. The VNAV angle is coded from the ARP to the FAF altitude.

DES

INTRODUCTION

If you were to classify descent techniques based on throttle position, there would be two main techniques, *idle throttle descent* and *partial throttle descent*. The *partial throttle* can be further refined to constant angle.

Idle throttle descent:

Tools such as VNAV or LVL CHG will place the throttles at idle in descent. A point in space is calculated where the airplane can begin a long glide to a waypoint down route that contains an altitude restriction. The Smiths FMC can calculate this point very accurately. However, the classic (3-4-5) will fly a high speed VNAV PATH descent better than the Next Generation (600 thru 900). If a high speed descent is needed, VNAV PATH in the next generation airplane may result in VNAV DISCONNECT.

The *idle throttle* descent works best in a situation where the descent path is likely to remain free of ATC interference.

The biggest advantage of using this technique is that the computer calculates the T/D and keeps the airplane on the calculated path; this frees the pilot from making the T/D calculation and requires less monitoring during descent - desirable when you are fatigued or in a high workload environment.

Disadvantages of the *idle throttle* descent technique are steep and sometimes, changing deck angles, faster rate of change in cabin altitude, and no room to meet speed restrictions from ATC without wasting energy (speed brakes). Another undesirable result of using VNAV descent as a habit is that the pilot tends to become complacent in descent calculations.

Partial throttle descent:

Using the V/S thumbwheel (MCP), one can select a rate of descent that will maintain a constant angle. The throttles are kept slightly off the idle stops. The top-of-descent will occur earlier than the *idle throttle* technique because some power is used throughout the descent. The airplane is not in a power-off glide configuration. There is no significant fuel savings between *idle throttle* and *partial throttle* descent, especially if the speed brakes are used during an *idle throttle* descent.

The *partial throttle* descent works best in situations where ATC is likely to interfere with speed and/or heading commands, or if a high speed is desired. Other advantages are a more comfortable and constant deck angle, better control of energy or "mass management", resulting in a position to meet speed and route changes without using the speed brakes because your profile does not change. There's also less thermal shock to the engines and it offers a more gradual pressurization change for anyone on board with a head cold. The disadvantage to this technique is that it demands a higher level of monitoring and piloting skill.

Partial throttle-constant angle:

The *partial throttle-constant angle* descent technique uses 3:1 method to calculate distance to descend. This is described on the next page.



Minimum gilde angle at a given attitude is approximately the same for all weights. In this were zero, minimum gilde angle angle would be exactly the same for all weights and would occur by gliding at the maximum lift to drag ratio (Max L/D). The speed to maintain a minimum glide angle increases with weight. This is necessary since as weight is increased a higher speed is required to keep the same L/D ratio. Maximum rate of descent is obtained at the highest possible airspeed.

At any constant high speed, the rate of descent is higher for light weights than for heavy weights. The effect of adding drag by extending the speed brakes or lowering the gear is to increase the rate of descent.

INTRODUCTION

up this way.

Let's assume we're crusing westbound at FL350. There is no significant headwind or tailwind. The restriction down route is 250 kts and 10,000 ft at a waypoint named DAISETTA. It is found on the DAISETTA arrival into Houston Intercontinental from the northeast. If the airplane is cruising at FL350, we have to loose 25,000 ft and then decelerate to 250 kts. Required math:

· Divide the altitude that must be lost by one thousand, then multiply by three. $25,000 / 1,000 = 25 \times 3 = 75 \text{ nm}.$

Note: If you've got a tail wind greater than 75 kts, multiply by four.

- For the FMC geeks, from this top-of-descent point, the angle, or Vertical Bearing (V/B) to DAISETTA is approximately 3.1°.
- Let's use a descent crossover speed of 300 kts.
- In this example, a deceleration segment is required because the clearance includes a 250 kts speed restriction. The 737 requires slightly less than a mile per ten kts of airspeed to decelerate in no wind, so add 4 nm to slow from 300 to 250. Now the top-of-descent point (T/D) is 79 nm from DAISETTA.
- Just prior to reaching the T/D, we'll roll the thumbwheel over and smoothly start our descent. But what rate to select? Take the groundspeed, divide by two, add a zero and 10%.

Example: Ground speed of 440 divided by two is 220. Add a zero and 10% makes 2400 fpm. This is your initial V/S selection. Continually re-check your position during the descent (3:1 plus the decel segment of 4 mn). The rate of descent will decrease slightly in the lower atmosphere because TAS is slowing as the CAS remains constant.

But wait, it get's much easier if the V/B is set up on the DES page. It's at LSK 4R.

First, let me explain that lines 3 and 4 on the right hand side of the DES page don't have anything to do with VNAV PATH. These fields are used to display actual airplane Flight Path Angle and Verti-

The Partial throttle-constant angle descent is set cal Bearing with required Vertical Speed to cross the entry at LSK 3R. Dave Gorrell has named this the "angle calculator".

> If the LEGS page has the restriction of 10,000 ft at DAISETTA, the DES page will look something like the one on page 157. See how steep the V/B (think angle) is for an idle descent. (3.9°) .

> Let's set up for a constant angle descent similar to the 3:1 technique.

> We're going to use the V/B indicator to determine when to roll the nose over, but it does not consider a deceleration segment. If you need a decel segment, build a waypoint this side of the restriction using the Along Track Offset method (DAS/-4). It will appear as DAS01. Don't leave it in the LEGS page because it might confuse your teammate.

You've added DAS01 to the temporary database.

Manually enter DAS01/10000 in 3R of the DES page. Now you're looking at the angle (V/B) to that wpt 4 nm this side of DAISETTA.

When the V/B from DAS01 indicates 2.9°, smoothly dial the thumbwheel to that indicated by the V/S at 4R. This places the nose at a FPA of 3.0°, matching the V/B. It will be around 2200 fpm in light winds. (see CDU below)



Adjust the thumbwheel to keep a the airplane on a V/B of 3.0°. The V/S display at 4R is helpful, but learn to fly the FPA too. Don't forget to press the C/ O button to choose your crossover CAS.

As the airplane levels at 10000, dial the speed back to 250. You'll get a great deal of satisfaction from feeling like you're in charge, instead of feeling like the computer is flying.

Slam-dunk using the V/B

You're abeam the airport, any altitude, configured to flaps 1 and 190 kts. Winds are light. You've previously entered the runway waypoint and crossing height in 3R of the DES page. Abeam the runway, you're cleared for the visual. Set the MCP to 1000 AFE, call for gear down, flaps 10, check the speed at 190 kts, spin the thumbwheel, and press LVL CHG. When the V/B indicates 8°, turn to base leg. As you transition through the base leg, slow to 170 and configure to flaps 15; the V/B will be approximately 4.5°. As you turn to final, slow to approach speed and configure for landing. Expect the V/B to be approaching 3.8°. As you continue your descent to the runway you'll catch the desired V/B of 3°.

Т	E	M	P(DF	R	R	Y
	-			~			1 L



- DES key.
 Automatically displayed at top-of-descent when an active CRZ page displayed, path descent mode is available, and MCP altitude is set below cruise altitude.
- CRZ DES page PLANNED DES prompt (LSK 5R)

NO REQUIRED ENTRIES

- May be used during preflight, climb, cruise, or descent to evaluate or EXECute (for immediate or planned use) one of the standard descent modes.
- DES page defaults to ECON PATH DES.
- Three descent modes are available: ECON (PATH or SPD), Manually selected speeds, or RTA.
- Idle descent speed calculated to meet the first altitude constraint on the LEGS page.
- Target Mach highlighted above crossover alt.
- Target CAS highlighted below crossover alt.
- During descent, CAS will increase and at some point equal and exceed the active Mach. Crossover will then occur. In this example crossover will occur when M.745 is exceeded by CAS of 295 kts.
- ECON descent Mach is set equal to the final ECON cruise mach. The ECON descent CAS values are derived as a function of CI entry.
- VNAV PATH is not suppose to exceed the barber pole; however during the time it takes to pitch up, you may exceed the limit enough to set off the clacker.
- U10.2: Reverts to LVL CHG 7 kts prior to VMO/MMO. 10.5: 1 kt. prior to VMO/MMO.
- Max: 12 kts below VMO/MMO.

E/D ALT is the last of the

a discontinuity:

or FAF for a non

precision approach,

following not preceded by

- glideslope intercept point

for precision approache

- lowest altitude constraint

- threshold crossing height

Also known as airport speed restriction.

• The FMC assumes value of 240 kts below 10,000' (10 kt margin).

During approach phase, displays XXX/

FLAPS, where XXX is the appropriate

including the runway

threshold altitude,

for the runway, or

(MA-XX) altitude

constraint.

- missed appraoch point

- AT XXXXX
- For a PATH DES: displays the next wpt which has an altitude restriction. Propagated from the LEGS page.
- Blank if no downpath altitude restriction.
- Blank for SPD DES.

TO T/D

- With E/D altitude entered: PATH and SPD DES display ETA and distance to T/D.
- With no E/D altitude entered: PATH DES is blank SPD DES displays ETA and distance to T/D based on SPD DES criteria.
- TO T/D ADVISORY displayed for U1.x
- Blank if distance greater than 999 nm.
- If an intermediate level-off has occured, displays values for the upcoming intermediate T/D point. TO T/D-XXXX

ECON PATH DES 1/1 E/D ALT AT DAS 250 / 10000 10000 TO T/D TGT SPD .745 / 295 1318.5z / 5 NM SPD REST WPT / ALT DAS / 10000 240/10000 FPA V/B V/S 0.0 3.9 2508 SPEED >

- Prior to top of descent

< FORECAST

Input for V/B calculator.Wpt and altitude

- constraint propagates from LEGS page.
- Manual entry permitted
- A manual entry does not drop out after wpt is
 sequenced - must be manually deleted.
- U10.5 Allows entry of destination runway. TCH fills in automatically.

Intended for early descents (prior to T/D). Execution of DES NOW (formerly called CAPTURE) causes the DES page to become ACTive. An early descent at 1000/min will commence at the TGT SPD until intercepting the computed path. Three things remove this prompt; FMC already in descent, active leg has a GP angle, or there is no hard alt constraint between you and the next GP angle.

DES NOW >

flap maneuvering speed.

PATH DES

VNAV PATH uses idle thrust and pitch control to maintain a vertical path, similar to a glideslope in 3 dimensions, except there is no ground-based beam. The TGT SPD is used for "planing purposes" only. There is no attempt to maintain the TGT SPD unless the airplane gets too slow.

VNAV PATH descent is slaved to the Path. It is the pilot's responsibility to control the speed. If unforecast winds are encountered you may have to intervene. Throttle up if a headwind lasts longer than expected or dive and/or apply speed brakes if a headwind component is less than predicted.

VNAV descent is automatically initiated at T/D if a lower MCP altitude has been selected. The computed profile terminates at the altitude restriction on the LEGS page. A path can be computed **only** if a mandatory "at" altitude restriction is specified.

Example: HOAGI at 10000 ft.

- For ACT SPD and PATH DES, present vertical deviation from the computed vertical path appears after top-ofdescent.
- Blank if DES not active.
- Updates to the computed path are performed periodically during stable state conditions, or whenever an entry is made, and every 15 sec. in early (DES NOW) or late (> 750' above path) descent.
- Pressing VNAV or LNAV from OFF to ON may produce an updated display.
- Do not use after an intercept to a wpt on the runway centerline unless LNAV is engaged; VERT DEV is referenced to the lateral path that existed at the time of execution.

VNAV PATH, SPD, and the RNP

Picture yourself in LNAV and VNAV, descending early (DES NOW) out of cruise altitude per ATC instructions. You're coming downhill at 1000 fpm.

ATC: "Barnburner 502, turn right 10 degrees, vectors for descent."

You press HDG SEL and if you're in a U4 or lower machine, VNAV disconnects. A U5 to U10.3 FMC will revert to VNAV SPD DES at some point!

With U7.1 and up, you will maintain VNAV PATH until the XTK ERROR exceeds the RNP. With 10.3, VNAV PATH will revert to VNAV SPD when XTK ERR exceeds two times the RNP. When the XTK ERR exceeds the RNP, PATH reverts to SPD. If you perform an INTC LEG TO function while in descent, PATH will revert to SPD because the XTK ERR is probably greater than the RNP. The PATH> prompt will reappear when the XTK ERROR is less than the RNP. For smooth operation, engage V/S while monitoring the VERT DEV in this situation.

U7.2 and up: After the intercept function is performed, engage LNAV. A dashed magenta line extends to the intercept route and VNAV PATH can now



Astronauts & engineers - Modification During Descent

The flight plan modifications entered and executed during the active descent result in the FMC flying the old flight plan until it completes path predictions for the new flight plan. The FMC will fly the old flight plan for no more than 60 seconds while waiting for the new path predictions. If after 60 seconds path predictions for a new flight plan have not been completed, VNAV disengages. This is to protect against possible violation of new constraints in the new plan. Failure to complete path predictions within 60 seconds can be a result of multiple bypasses in descent or insufficient time between crew-entered modifications.



Astronauts & engineers - Descent Path Construction For path descents, a speed profile is first predicted and stored by waypoint. In this context, "waypoint" can include fixed and floating lateral waypoints, as well as phantom waypoints associated with the vertical plan. Each pair of consecutive waypoints forms a segment of the descent speed profile, with a stored speed for each waypoint. When the speed changes in a segment, a gradient is calculated and used to change the target speed linearly as a function of the distance between waypoints. The most significant application of this gradient, in path descents, is in the deceleration segments at 10,000 ft (deceleration to 240 kts to permit a 10 kt margin to the 250 kt restriction) and at approach altitude (deceleration fo flap extension schedule airspeeds).

As the descent profile is actually being flown, the vertical deviation from the reference path is used to adjust the target speed when the aircraft is above the path. This adjustment recognizes that excess energy is inherent in the aircraft position above the path, and compensates the target speed accordingly.

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PATH DES

May 98

Maintaining Vertical Path On a Heading Clearance

This lesson discusses the problem of maintaining the desired idle descent vertical path after ATC assigns a heading during descent.

A workaround is available under certain situations.

Assume you're 20 nm from the topof descent inbound to College Station and planning the COAST ARRIVAL to Houston, Intercontinental.

We'll use three different examples:

Example one keeps you on the active route; example two puts you on a heading that allows an interept to be built; and example three has you on a heading that does *not* allow an intercept.

COLLEGE STATION

D 113.3 CLL

Example 2 takes you off the active route but allows an intercept.

ATC: "Barnburner, fly heading zero nine zero, vectors for spacing, descend to Flight Level 240".

The workaround for U7.2 and up is:

- Dial 090 in the MCP and select HDG SEL.
- Set 240 in the ALT SEL and select V/S 1000 fpm.
- · Do an intercept to COAST on the 125 inbound course. When the airplane rolls out on the 090 heading, press LNAV. (A problem with this workaround is that you've entered a command into the FMC that may not match the clearance the intercept.)
- · After engaging LNAV, a dash/dot magenta line will extend from the a/c symbol to the solid magenta line. This is called the capture path. It requires LNAV to be engaged. VNAV PATH references this capture path.
- Check the DES page to ensure PATH is in title. If the title says SPD DES, check LSK 5R for the PATH> prompt and select it.
- After you're back in PATH, press VNAV. The airplane will now continue in a PATH DES.

81°-> COAST HOAGI Cross at 250 kt ACT RTE LEGS and 10,000 ft 1/2 89° 10 NM CLL .740 / FL219 23 NM 100 MACED COAST 280 / 12650 11 NM 125° 250 / 10000 HOAGI BANTY 125 Example 1 keeps you on the route that MACED Houston is in the FMC. 125° Intercontinental BANTY ATC says: "Barnburner, descend to RNP / ACTUAL Flight Level 240". 2.80/0.23 Press DES NOW (CAPTURE). VNAV HUMBLE D 116.6 IAH commands a 1000 ft/min descent until capturing the computed path to cross HOAGI at 10,000 ft. Example 3. ACT ECON PATH DES 1/1 ATC says: "Barnburner, fly heading one two five, E/D ALT AT HOAGI 250 / 10000 151 vectors for traffic, descend to Flight Level 240". TGT SPD There is no workaround in this situation because it's 1328.5 z / 50 NM .740 / 280 tough to build a route to keep the airplane in LNAV. SPD REST WPT/ALT HOAGI / 10000 250 / 10000 • A good technique is to use V/S, using the FPA, V/B, VERT DEV FPA V/B V/S V/S information on the DES page. This is an 29 2.8 2700 0 FT excellent skill to develop but takes practice. • Monitor your 3:1 altitude vs distance ratio to your SPEED > target (HOAGI). Leading Edge Libraries ©





DESCENT

DISCUSSION - The following is presented as an educational sample

If a restriction 35 nm from the airport does not exist, it might be useful to create one. Assign 250 kts / 10,000 to it. Forty out at 10,000 and no speed restriction works too. Make sure your wpt is measured from the runway, and not the Airport Reference Point! (El Paso's RW26 is a good example)

Normally, build a route to the FAF and enter the desired speed and altitude. Examine all intermediate predicted altitudes. Enter only necessary crossing restrictions. Try not to enter altitude constraints higher than those predicted, using instead the MCP as the altitude limiter.

You'll see techniques such as building a wpt 5 miles in front of the constraint but generally the 737 FMC does an excellent job at predicting the T/D point. It is only when unforecast winds enter into the equation that the path becomes too steep (exceeding predicted speed) or shallow (throttle up).

EFIS aircraft have provisions on the DES FORE-CAST page to enter lower-level winds. This creates several shorter linear equations, which results in a more realistic wind model than one created with one long linear equation as discussed on the next page. This allows the FMC wind model to be more accurate when coming out of the jet stream, which is when you should use these entries.

For aircraft without the DES FORECAST feature, the following technique can be helpful when the altitude restriction is combined with a speed restriction.

Before the top-of-descent is reached, check the actual wind at altitude and forecast lower level winds. If you are coming out of the jet stream and winds at lower altitudes are light, choose one of the techniques below.

Descending westbound out of the jet: Problem: as the headwind is lost, the aircraft will be in a position with lots of excess energy - high and fast.

OR]

OR

OR

Enter a wpt 4-5 miles prior to the first restriction and enter the same restrictions. As you loose the high headwind, delete the created waypoint (use V/S during re-computations).

Enter an altitude approximately 500 ft lower than the clearance. Protect yourself by entering the clearance altitude in the MCP. The MCP will act as your limiter.

Start the descent 4-5 miles early using LVL CHG. Keep the VERT DEV (line 4 on the DES page) around 1000' below your computed path. As you come out of the excessive headwind, you will close on your computed path. Transition to VNAV.

Descending eastbound out of the jet: Problem: as tailwind is lost, aircraft is in a position similar to starting down too early and will pitch up to maintain the path. Speed will drop off, and in newer software, throttles will come up, wasting energy. Example.

Start down a few miles beyond the computed descent point! The path will be captured, but with excess energy (exceeds the computed speed). As the high tailwind is lost, this excess energy will trade off.

This is a view of the DES page and airspeed indicators during a situation in which (left) the actual tailwind is less than (or headwind is more) and (right) actual tailwind is more than (or headwind is less) the FMC wind model. In PATH DES, the path is maintained at the expense of speed.



Dec 02

Astronauts & engineers

The path computation processing always proceeds by individual phases, even though a complete profile of takeoff, climb, cruise, and descent phases may be required. Phase by phase, profile predictions compute the required parameters at waypoints, leg by leg, and assemble the lateral and vertical segments into the flight plan navigation legs which are displayed on the CDU.

First step - **Cruise Prediction**: The sequence of waypoints in the computation process is in the normal or forward direction. Initially, the top of descent is unknown. The first cruise predictions are performed for a cruise without a T/D and terminate at an imaginary end of cruise. This is the first waypoint in descent which is allowed to have a speed and altitude restriction and is determined by a rough estimate of distance from the destination. This estimate is designed to ensure that the imaginary end of cruise will always precede the T/D.

Second step - Descent Prediction: For initial predictions of all descent modes, the path computation sequence begins with the last waypoint pair in the flight plan and preceeds backwards, to establish the location of T/D. To do this, the approximate location of T/D is estimated, without regard for speed or altitude restrictions, to obtain a speed schedule and path gradient in descent, and a final fuel -remaining estimate. Range in descent is first estimated from the altitude change in descent and an assumed flight path angle constant. Subtracting the range in descent from the total range provides the first estimate of T/D location. This allows for a "cruise with a T/D" calculation of fuel remaining and speed at T/D. Next, the estimated fuel remaining at T/D and wind profile are used to estimate descent range, speed schedule, path gradient, and final fuel remaining. This calculation of range is compared with the initial estimate to determine whether they agree within .5 nm. If not, the second calculation of descent range is used to make another estimate of fuel at T/D, and this new fuel value is used to make a third calculation of range. Then the full leg prediction is commenced using the last set of calculations, leg by leg, backward from the terminal waypoint. This determines a "descent T/D" and a value of predicted fuel remaining. Now the cruise prediction can be completed, forward from the imaginary end of cruise to "cruise T/D", giving another prediction of fuel remaining at T/D. The accuracy of the T/D location is tested by comparing the two values of fuel remaining. If the difference exceeds 1,000 pounds, the descent processing is repeated using fuel remaining and speed at T/D. Then the complete backward descent prediction is repeated using the new final fuel, speed, and path gradient. This process is repeated until predicted values of fuel remaining at "cruise T/D" and the "descent T/D" agree within 1000 pounds. The difference in the two estimates is added to predicted fuel remaining at descent waypoints.



The drawing above represents the FMC computed descent speed schedule and discusses some topics the pilot must consider prior to top of descent.

As you know, during a PATH descent the aircraft will sacrifice target speed to maintain the computed path or imaginary glide slope. The ability of the aircraft to maintain the target speed is completely dependent on the quality of information you supply the computer and how the FMC wind model matches the actual winds. As you may suspect, the actual winds do not always decrease linearly, as discussed on the next page. Instances where you descend out of the jet stream to light winds at lower altitudes do not fit the model. Another example is a descent out of light winds to tail/headwinds at lower altitudes.

By viewing the airspeed indicator during descent, you can tell how close the linear model(s) matches the actual winds. Of course it's too late at that time to design a smooth descent, so planning it required prior to top of descent.

If you are operating software at a level of U3 or above, the forecast winds at lower altitudes can be entered on the DES FORECAST page. This creates several linear equations instead of the single equation that U1.x operators are faced with.

Feb 92

LINEAR WIND DATA

The following data was constructed from linear equations using sample winds at different intervals to zero at the surface.

Comparing the computer generated wind model to forecast descent winds leads to a more precise

control over choosing top of descent; helpful when a speed restriction exists at the bottom of descent. The FMC wind model does not fit actual winds when descending out of the jetstream.

Auril 1	- book as	and a shore	LI	NEAR W	IND MO	DEL AN	ALYSIS		Clair and		112.11
	36x=175v	36x=150v	36x=125v	ax+by+c 36x=100v	=0 ax=b 36x=82y	36x=75y	36x=62y	36x=50y	36x=36y	36x=25y	36x=12y
	x=175y/36	x=150y/36	x=125y/36	x=100y/36	x=82y/36	x=75y/36	x=62y/36	x=50y/36	x=36y/36	x=25y/36	x=12y/36
Altitude						VIPAL DILLO	The second				
41000	199	171	142	114	93	85	71	57	41	29	14
39000	190	163	135	108	89	81	67	54	39	27	13
37000	180	154	129	103	84	77	64	51	37	26	12
35000	170	146	122	(97)	80	73	60	49	35	24	12
33000	160	138	115	92	75	69	57	46	33	23	ad 11
31000	151	129	108	86	71	65	53	43	31	22	10
29000	141	121	101	81	66	60	50	40	29	20	10
28000	136	117	97	78	64	58	48	39	28	19	9
27000	131	113	94	75	62	56	47	38	27	19	9
26000	126	108	90	72	59	54	45	36	26	18	9
25000	122	104	87	69	57	52	43	35	25	17	8
24000	117	100	83	67	55	50	41	33	24	17	8
23000	112	96	80	64	52	48	40	32	23	16	8
22000	107	92	76	61	50	46	38	31	22	15	7
21000	102	88	73	58	48	44	36	29	21	15	7
20000	97	83	70	56	46	42	34	28	20	14	7
19000	92	80	66	53	43	40	33	26	19	13	6
18000	88	75	63	50	41	38	31	25	18	13	6
17000	83	71	59	47	39	35	29	24	17	12	6
16000	78	67	56	44	37	33	28	22	16	11	5
15000	73	63	52	42	34	31	26	21	15	10	5
14000	68	58	49	(39)	32	29	24	19	14	10	5
13000	63	54	45	36	-30	27	22	18	13	9	4
12000	58	50	42	33	27	25	21	17	12	8	4
11000	54	46	38	31	25	23	19	15	11	8	4
10000	49	42	35	28	23	21	17	14	10	7	3
9000	44	38	31	25	21	19	16	13	9	6	3
8000	30	33	28	22	18	17	14	11	8	6	3
7000	34	29	24	19	16	15	12	10	7	5	2
6000	20	25	21	17	14	13	10	8	6	4	2
5000	20	21	17	14	11	10	9	7	5	4	2
4000	10	17	14	11	8	8	7	6	4	3	1
2000	15	13	10	8	6	6	5	4	3	2	011
2000	10	8	7	6	4	4	3	3	2		1
1000	5	1	A	3	2	2	2	1	1		0
000	0	0	0	0	0	0	ō	Ó	ò	0	0

HOW TO USE CHART

Situation: Path Descent westbound out of the jetstream. Headwinds at your Flight Level (350) are 97 kts.

Examine your forecast winds at lower levels. Let's assume your flight plan prints these winds at 14,000' at 20 kts on the nose.

From the table above, the FMC headwind component at 14,000' is predicted to be 39 kts.

You can therefore, expect to have excess energy upon your arrival into the lower atmosphere (indicated by the airspeed needle being above the bug). The excessive speed is required to stay on the path. It is no problem if you have no speed restriction awaiting you at the bottom. But if you must meet a speed restriction, consider a method of selecting an earlier T/D as discussed on page 92, or devise one of your own. (Just let me know if its a good one).

Rule of thumb: To calculate a linear wind at lower altitudes, divide your winds at cruise by 3 and add 10%.

TECI	HNIQUE
 Occasionally you'll find yourself in the position of instance where this is very common is on a PATH D suddenly being cleared direct to this waypoint! On a PATH DEScent, the FMC will prioritize path of speed restriction, here are two techniques that make square of the velocity (increased drag will increase) Leave the airplane in VNAV PATH. Since the air restriction on the LEGS page, all you need to do speed brakes until the actual CAS matches the Select LVL CHG and a high speed. This is called they will create more drag the faster you are transitioned. These techniques result in a steeper gradient be If you really need to descend fast, consider the wasting large amounts of pitching energy into is holding the plane up in a 1g maneuver. 	being on the computed vertical path but fast. One DES with a dog-leg to the restricted waypoint and over airspeed. If it becomes doubtful you'll make the e use of the rule <i>parasitic drag increases with the</i> energy dissipation rate.) rplane is slaved to the path to meet the altitude to is regain control of the speed; simply deploy the target speed. In <i>dialing in drag</i> . Use the speed brakes if necessary; aveling. eccause the CAS is higher. spiral where high speed drag can be retained while the turning. At 45° bank only 70% of the lift energy
Lets assume you are descending on an PATH DES v If ATC wants you to increase your speed in the des you to slow prior to reaching the level off altitud ATC: "Bellanca Airbus, increase your descent sp Select V/S. Turn the speed knob up to 320 kts. Indicator and keep the airplane well below the c in the DES page as this will throw out the shallor being slowed early. Now when ATC wants an early speed reduction, p but the excessive speed will trade off as the nose ri	Accent, but you anticipate the next controller will want be try this technique. Second to 320 kts for spacing'' (Autothrottles are on). Monitor the Path Deviation omputed path using the V/S wheel. Do not enter 320 wer path that we want to monitor in anticipation of ress VNAV. You'll get the DRAG REQUIRED message ses to capture the path.
TECI	HNIQUE
You're level at ten thousand feet indicating 250 kts thousand feet, upon reaching seven, slow to 210 k Here's a technique to use so you won't forget what Press the V/S button and dial a descent rate of 1500 kts in descent by making small adjustments to the in to capture the pre-set speed.	. The approach controller says "Descend to seven ets". the clearance speed is at level-off. D ft. Spin the speed knob back to 210. Maintain 250 V/S wheel. As you level, the throttles smoothly come
Calculating your own top-of-descent point forces y airplane	you to keep your mind active and ahead of the
Situation: Cruise altitude is 35,000. Restriction exi Partial throttle - V/S (easy) 25 x 3 = 75 At T/D, set V/S to half the ground speed + 10% * Add 1 mile per ten kts for deceleration to 250 kt; * Adjust for tail/head wind of 1 mi. per 10 kts of w * Add 1 mile for each half inch of mercury above s TEC If you are descending with the MCP using V/S, and select SPEED. (The light goes out.) Leave the aut to control descent with the V/S wheel. As aircraft re	sts at 10,000' at 250 kts. 35 - 10 = 25 <i>Idle throttle</i> - LVL CHG (much harder) 280 kt descent, multiply 25 times 2.5 320 kt descent, multiply 25 times 2 + 10% for the 737, this is conservative. ind. tandard. <i>HNIQUE</i> I you want to stop the autothrottles from hunting, de- othrottle switch ON. Throttles are in ARM. Continue eaches MCP ALT SEL, throttles come in to assume
present indicated speed not the hug speed	and the second states and second states of the second states of the second states of the second states of the s
present mulcaled speed, not the bug speed.	and the one divised as an all
Astronauts & engineers: WINDS - DESCENT The FMC uses <u>cruise</u> winds (either actual or estimated) at cruis	e altitude and a linear interpolation of this value down to zero wind

at destination. Interestingly, the path is re-computed using <u>current</u> wind values if any modification of the route is performed during the descent. A simple speed change, re-entry of an altitude constraint, or a route modification are examples of a modification that would cause a re-computation of the path. This could result in putting the aircraft above or below the re-computed path but may yield a more accurate descent path for the conditions. More research is needed.

If the wind variation in descent is significantly different than the linear model in the FMC, the result might be a path that is more difficult to stay on, i.e. under/overspeed, deviations over or under the path.

You get to this page by:

- DES page FORECAST prompt (LSK 6L)
- CRZ DES page FORECAST prompt (LSK 6L)

NO REQUIRED ENTRIES

DES FORECASTS page is made ACTive when the vertical flight plan becomes active. It is used to increase the accuracy of the descent path when descending through the jetstream or when forecast winds are significantly different than the computer generated linear model.

TECHNIQUE When passing through the Transition Layer, • Start descent early. For each 1,000' that 45% N, your vertical position should be expressed in is expected to be used, start down 1 nm earlier terms of Flight Level (QNE) when climbing and than the FMC computed T/D. (May be up to 35 in terms of Altitude (ONH) when descending. nm earlier than usual) Use of this rule may still require the use of speed brakes, especially when initiation altitude is low. The TRANS ALT or TRANS LVL is extracted Press LVL CHG. Turn autothrottles OFF. from the nav database for SIDs, STARs, Manually position throttles to 45% N₁. Rate of and approaches (not runways). descent is controlled with speed knob. • If one of these has not been selected, the value defaults to FL180. • Carrier can change the default value by • TAI ON/OFF - Expected altitudes for antiice usage. Presently disabled. If Boeing purchasing a Perf Defaults Data Base diskette from Smiths. goes back to low idle, it will be enabled. • Manual entry has priority. • U5.0 The altitude band over which antiicing will be used to help the FMC account for the additional thrust delivered Predicted ACT DES FORECASTS 1/1 by 28-40% N, required for bleed air. cabin rate of TAI ON/OFF TRANS LVL FL180 --/---descent req'd ISA DEV / QNH CABIN RATE from CRZ Destination ISA DEViation and QNH altimeter -° / 30. 20 480FPM altitude to - - DIR / SPD WIND ALT setting (millibars or inches) to provide FL240 080° / 50кт DEST compensation for that portion of descent elevation. 14000 100° / 25кт below TRANS LVL. Decimal required. • Helpful if Above TRANS LVL, FMC uses baro - - - º/- - - KT using the uncorrected altitude. stby press. Defaults to 29.92. If you do not enter the Enter average ISA true setting, you are telling the FMC to use deviation for desent U3 and up the default value, which, when desired, does in °C (±XX) or °F Forecast descent WIND save operating time. $(\pm XXF)$, though has · FMC will interpolate from negligible effect. the T/D wind to wind(s) entered on this page to - TECHNIQUE predict a complete descent If you think the software consistently wind profile. puts you above the path in a tailwind... TECHNIQUE • Enter ALTitude (line 3L) use the QNH entry to bump the altimeter Descending from QNE and DIRection / SPeeD up an inch. This produces a buffer of to a high QNH puts the (line 3R) for up to 3 about 800' crossing the TRANS LVL. aircraft above (high) the forecast true wind values. The airplane with pitch up to recomputed idle path so Any altitude sequence capture the idle path and you'll bleed always make the QNH entry is allowed. off about 10 kts of excess speed. entry when in a high • FMC initially places each below the path in a headwind... pressure area. entry at line 3. Subsequent make a QNH entry an inch lower than T/D will be a few miles entries displace entry at reported. The airplane with dive to resooner. Don't bother with line 3 to a lower line. capture the path and you'll gain about an entry when altimeter 10 kts crossing the TRANS LVL. is lower than standard.

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TEMPERATURE COMPENSATION TO BARO ALTIMETER

Special thanks to Jim Gregory and George Dewar for help in preparing this lesson.

Pressure altimeters are calibrated to indicate true altitude under ISA conditions. However, a correct setting of the altimeter does not correct for nonstandard temperature.

If the temperature at a given altitude is equal to the standard value at that altitude, and the lapse rate and sea-level conditions are also standard, the altimeter will read the correct altitude. The altimeter can be corrected for sea level conditions, but no way has yet been devised to account for variations in the lapse rate. Any deviation from ISA will therefore result in an erroneous altimeter. And the vertical path, if flown in baro VNAV, may not be the same as that printed on the chart.

To ensure appropriate obstacle clearance when an aircraft is operated at any charted minimum IFR altitude, it is necessary to apply a correction to the charted altitude.

RNAV plates specify a minimum temperature at which the procedure can be flown to ensure obstacle clearance in the final approach segment, but conventional approach plates do not - they are designed for +15°C.

If the temperature is other than standard, errors become proportionally greater with altitude above the altimeter site (usually the airport). In the case when the temperature (at the reporting site) is higher than ISA, the true altitude will be higher than the figure indicated by the altimeter. Higher than ISA temperature results in VNAV (Gradient Path) flying a higher approach angle.

Likewise, unless a temperature correction is applied, the true altitude will be lower when the temperature is lower than ISA. Lower than ISA temperature results in VNAV flying a lower approach angle. This will result in less than the required obstacle clearance (ROC) if the aircraft is operated at the charted minimum IFR altitude without a correction. Altimeter errors are significant under conditions of extreme temperatures, therefore it is particularly important to apply a correction to minimum IFR altitudes under these conditions.

Remember the old saying,

"WHEN IT'S COLD, LOOK OUT BELOW".

Example: Assume we're shooting the conventional LOC (BACK CRS) DME Rwy 10 at Calgary. The chart displays the minimum descent altitude at GADIS as 5400 ft MSL (1853 HAT). This minimum IFR altitude provides the required obstacle clearance only under ISA conditions (15°C).

If the temperature at the airport was -30 °C, the true altitude would be about 5100 ft (5400 -300), Conservative when aplied at higher aerodrome.

or just 670 ft above and a mile north of a tower (4430'). Canadian controllers are aware of the effects of cold temperature on aircraft altimeter systems. All ATC minimum vectoring altitudes in Canada account for cold temperature and require no corrective action by the pilot.

It is particularly important to make cold temperature altitude adjustments on initial, intermediate, final approach and missed approach segments if the aircraft is going to be at any minimum IFR altitude during each off these segments, especially in a non radar environment. Doing so will ensure the appropriate obstacle clearance. When cold temperature corrections are made to an initial or missed approach minimum IFR altitude, pilots should advise ATC how much of a correction will be applied.

Any temperature correction made by the pilot to the minimum IFR altitudes on an approach, especially the final segment, will not affect the controller's separation. You will have already obtained your clearance for the approach; therefore altitudes at the point of the receipt of the approach clearance all the way through to the missed approach clearance limit are the pilots.

If an adjustment is necessary for missed approach or minimum enroute altitude simply request a higher altitude from the controller.

It is important to restate that cold temperature corrections are only applied to the minimum IFR altitudes and are not applied while on radar vectors where the ATC assigned altitudes have a temperature correction factor applied. General Rules:

- At -30C and at 3000 ft above the field, the intermediate ROC is completely lost.
- At -30C and 1500 ft above the field, half the intermediate ROC is lost.

Required Obstacle Clearance (ROC) Proc. turn / Arc / Initial App. Segment = 1000 ft Intermediate App. segment = 500 ft (IAF to FAF) FAF to MA point = 250 ftCircling (Cat A, B, C) = 500 ft above the airport Circling (Cat D) = 600 ft above the airport

(Circling MDA's are based on a 300 ft ROC)

VAL (4 ft	UES TO per 1,0	D BE AI	DDED TO above th	D PUBL e sourc	ISHED / e per °	ALTITU C off st	DES (ft) andard)	
Source Temp	S el	ea Lev evatio	vel Aero n of the	drome altime	- Heigh ter setti	t in ft a ing sou	bove th rce (AG	e L)
°C/°F	200	500	1,000	1,500	2,000	3,000	4,000	5,000
0/+32	20	30	60	90	120	170	230	200
-10/+14	20	50	100	150	200	290	390	400
-20/-04	30	70	140	210	280	430	570	620
-30/-22	40	100	190	280	380	570	760	860
-40/-40	50	120	240	360	480	720	970	1,100
-50/-58	60	150	300	450	600	890	1,190	1,380

Table calculated for sea level aerodrome - linear variation.

HOLD

U10.2 and up

- You get to this page by:
 - Select the HOLD key. If a hold does not already exist in the flight plan, this action displays the HOLD AT page which allows the pilot to specify a desired fix for the hold.
 - If one or more holds already exist in the flight plan when the HOLD key is pressed, the ACT RTE
 - HOLD page is displayed which shows the characteristics of the nearest hold in the flight plan.
 - The NEXT HOLD prompt can be used to access other holds in the flight plan.



You get to this page	by:
----------------------	-----

(HOLD) key.

The RTE HOLD page provides a means of selecting a holding pattern fix point from either the aircraft present position (PPOS) or a preplanned geographical point. Performance predictions assume level flight. The FMC will complete and perform tear drop, parallel, or direct entry holding patterns according to the hold geometry and the initial course to the hold fix.

Fixes will utilize charted holding pattern data automatically if available from the nav data base.

ATC : "Avro Tudor, hold northwest of Cugar on the 280 radial, right turns, 1 minute legs".













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All exit paths treat the exit hold point as a flyover waypoint, crossing it on the original track.

If the EXIT HOLD command is issued while flying either a parallel or a teardrop initial entry, the aircraft will fly the remainder of the initial entry and exit the hold pattern at the next crossing of the hold fix. Manual intervention may be desired.

If the exit command is made while flying a direct initial entry, an immediate direct-to path to the hold fix may or may not be generated, depending on where the aircraft is in the entry path.

If the hold pattern exit is armed and executed just

after passing Navis, a temporary exit hold point is built at G - 2 sec. past the fix. The exit path - almost a 360° turn - is generated from present position to Navis followed by a 2 sec. straight path to G, which is treated as the exit hold point.

When a hold pattern exit is accomplished at B. and winds are as indicated, the aircraft will continue towards **D** until the constant radius path (bank angle will vary) will cross Navis on the inbound course. Manual intervention may be desired.

If the exit command is issued between points C and E, the direct-to exit path is generated from current position.



HOLD

PLACE-BEARING / DISTANCE HOLD FIX - U10.2 and up

When you are holding at a DME fix, and your inbound course points away from the VOR but into the DME fix, the radial and the inbound course are the same, rather than reciprocals. There is a special rule in the 737 which is: If the holding fix is a place-bearing / distance waypoint, where the "place" is a VHF navaid, the radial field on the hold page gets set equal to the "bearing" of place-bearing / distance. The RADIAL is always displayed relative to the reference navaid for the hold fix. The INBD CRS now defaults to the course from the reference navaid to the hold fix!

The INBD CRS is "uncoupled" from the RADIAL field and can be changed separately.

This special rule is only invoked when the hold fix is a PBD from a VOR.



PROCEDURE TURNS (U6, 8, 7.2 & up)

The system's guidance routines for entry are

determined by the FMC. A pilot-entered speed may of altitude, as programmed in the FMC. also be used in flying the holding pattern. Sometimes the pilot feels as though the entry is not correct due to the timing of the turn or the bank angle but both of these items have been calculated to maintain the desired holding track.

The turn radius of the pattern is determined prior to each successive crossing of the hold fix. It bases its calculation on predicted ground speed at the fix, taking actual wind into account. A max turn radius is programmed as a function of predicted altitude at the fix. Up to 25° bank angle is used to construct the path.

If the pilot commands a higher speed than predicted, the airplane will fly a 30° bank in an attempt to stay on the track; if speed is excessive, the airplane will fly a larger pattern than displayed. The pilot must be ready to intervene, especially in mountainous terrain.

The entry method used (parallel, teardrop or direct entry) is a function of actual airplane track as the holding fix is crossed, not as a function of airplane heading or the direction from which the active route approaches the holding pattern.

The AIM states that the pilot is expected to start reducing speed three minutes prior to reaching the fix and to use 25 degree angle of bank if using the FD. If the FMC appears to be flying something other than the clearance, as always, the pilot should be ready to intervene.

Some databased procedures contain procedure turns. They cannot be manually entered. These accomplished. maneuvers provide a means of performing a course reversal within defined geographical boundaries.

The nav data base includes procedure turns encoded for the terminal area procedures that require their execution. The FMC will construct predicted paths based on the geometric limitations of the maneuver, predicted winds, and a 170 knot airspeed. In cases where strong winds prohibit accomplishment of the maneuver within the geographic limits, leg length of the maneuver will be shortened in an attempt to fit the maneuver within the prescribed area.



The radii of the turns of the hold patterns are based upon the FAA's 70° sector decision criteria. limited as a function of aircraft altitude. This table Constant radius turns and a Best holding speed is lists the maximum hold pattern radii as a function



A discontinuity will be inserted if this cannot be

ACT	RTE LEG	iS 1/X
50°	29 NM	
ATL	The start of	/
THEN		
00000		
BC	UTE DISCON	JTINUITY
BUBNY	OIL DIGGOI	170 / 4000A
		1101 4000/
(INTC)		170 / 4000
(11110)		170740004
93°	3.0 NM	1 1000
IZZY		/4000
93°	0.1 NM	
GS-08R		160/4000
93°	4.2 NM	GP 3.0
BURNY		/2620
93°	4.7 NM	GP 3.0
RW08R		/1082
		7 1002
1 70 / 0 OF		BTE DATA >
1.70 / 0.05		HIE DAIA >

APPROACH REF

You get to this page by:

- INIT/REF INDEX page APPROACH prompt (LSK5L).
- INIT REF

NO REQUIRED ENTRIES

Prior to U7.0, within 50 nm of the Origin, Airport Information relating to a return approach to the Origin is displayed. Beyond 50 nm or before the halfway point (whichever is less) from the Origin, data for the Destination is shown. If the aircraft is not yet airborne, pressing the APPROACH prompt on the INIT/REF INDEX page displays information relating to the Origin airport.

With U7.0 and on, airport information for the Destination, if selected, is displayed after CRZ is active.


You get to this page by:

- INIT REF INDEX page MSG RECALL prompt (LSK 2R).

NO ENTRIES ARE ALLOWED

- Lists all alerting and advising messages whose display criteria are still true.
- Messages which have been acknowledged with the CLR key may be checked on this page to see if they are still active.
- Messages which are no longer active because the causing conditions are no longer true, are removed from the list.
- The list has no limit to its size.
- Use $\left(\begin{array}{c} NEXT \\ PAGE \end{array} \right)$ or $\left(\begin{array}{c} PREV \\ PAGE \end{array} \right)$ to review additional pages of messages when more than one page exists.

INIT / REF INDEX 1/1 <IDENT NAV DATA> a.c. <POS MSG RECALL> 18 <PERF ALTN DEST> 1 fest <TAKEOFF ACARS> IRS NAV> 120 <APPROACH <OFFSET MAINT> **MESSAGE RECALL 1/1** NAV DATA OUT OF DATE UNABLE CRZ ALTITUDE SCANNING DME FAIL http://www.contential <INDEX Leading Edge Libraries © 180

ALTERNATE DESTINATION - U6, U8 & up

You get to this page by:

Feb 92

- INIT/ REF INDEX page ALTN DEST prompt (LSK 3R).
- APPROACH REF page ALTN DEST prompt (LSK 6R).
- RTE page ALTN DEST prompt (LSK 6R) when in air only.
- NEAREST ARPTS page PREVIOUS prompt (LSK 6R)
 - NO REQUIRED ENTRIES
- This function provides the crew with a simple and quick means of determining the distance, time, and fuel burn to up to five alternate destinations.
- Six pages are available. The first is the summary page; up to five may follow, one page for each *entered* alternate for review or alteration______



You get to this page by:

- ALTERNATE DEST page NEAREST ARPTS prompt (LSK 6R).



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Dec 02

DIVERTING

We'll consider the topic of Diverting (without the Alternates Airports option) using 2 circumstances.

First example: Diverting Direct To the Alternate. FIG. A Second example: Planning a divertion long before it's needed. FIG. B

Jan 03



FIG. B -



Dec 95

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May 98

SELECT DESIRED WPT

You get to this page by:

- Automatically accessed when an entered identifier has more than one location in the nav data base.
- Presently limited to one page, but addition of another is planned.

NO REQUIRED ENTRIES

- If an identifier is entered that identifies two or more navaids or waypoints in the FMC database, the SELECT DESIRED WPT page automatically appears.
- It provides a means to further define to the system which of the waypoints having the same identifier is the intended one.
- U1 through U8: The database is searched in the order the data was loaded. It is not searched starting with waypoints closest to the airplane.
- U10: Intelligent sorting is available. The database is searched starting with waypoints closest to the reference position.
 - The reference position is defined as follows:
 - If a MOD is being made to a RTE or LEGS page which does not affect the go-to (active wpt), then the reference position is the lat / long of the wpt preceeding the entered wpt.
 - All other operations including a DIR-TO and INTC use the airplane position as the reference position.
- Anytime this page is displayed, ratchet up your concentration a notch. Don't get in the habit of selecting the top choice. This page increases your workload and opens a window for error.

A navaid or waypoint is not always stored in the database under the one-, two-, or three letter coded identifier shown on aeronautical charts and approach plates. Instead, it may be stored under a waypoint name comprising several letters. This inconsistency is particularly common with respect to waypoints in South America.

• U1 through U8: May list

up to 6 wpts on one page.

entry attempt was made.

If the desired waypoint is stored in the FMC under its name rather than its coded identifier, it will not appear on the SELECT DESIRED WPT page at all. A more distant, probably undesired waypoint will appear at the top of the CDU. Before executing the selection at the top of the screen, extreme care should be taken to compare the lat/lon taken from the database against the lat/ lon shown by the chart, if available, and to check that the proposed routing shown on the Map display looks reasonable.

U10: Up to 12 wpts with the same identifier may be contained in the database, requiring 2 pages.
Select desired waypoint from given information using the line select key of your choice (left or right side).
The display automatically returns to originating page with the selected waypoint entered where the previous

SELECT DESIRED WPT 1/2 R NDB N04°40.7W074°06.3 R NDB S02°07.8W079°52.1 R NDB S16°30.5W068°13.1 R NDB S17°23.8W066°15.8 R NDB S33°06.6W064°17.3 R NDB N43°44.3W079°42.2

SELECT DESIRED WPT



The ILS's are in the nav database to support LOC updating.

If you enter the ID of an ILS, such as IBFI, it will only display on the LEGS, RTE, or FIX pages if there is a DME associated with that localizer. If here is no DME, like ISEA, you will get the message NOT IN DATA BASE. It is in the database for LOC updating but cannot be used as a wpt.

The coordinates are for the LOC antenna position, which is near the departure end of the runway (Near the landing threshold of the opposite runway).

The DME may be colocated with either the LOC antenna or the GS antenna which is typically abeam the TDZ. If it is colocated with the LOC antenna, there is only one entry in the database. If it is not colocated with the LOC antenna, there will be two entries in the database: one for the LOC and one for the DME.

The location of the ILS DME facility is not on the chart, so there is no way to know in advance when you will get the SELECT DESIRED WPT page. A DME associated with an ILS is usually at the far end, though not always.

If an ILS approach does not have a DME, the identifier's coordinates will be that of the localizer antenna. (You can tell this by looking at the chart.) Ref: IAH (14L-32R) SJC (12R-30L)

If an ILS approach has a DME, the identifier's coordinates will be that of the DME antenna. (unless the dreaded SELECT DESIRED WPT page comes up, in which case you've got two coordinates)

The following is the only time you'll get the SELECT DESIRED WPT page from an ILS ident entry.

If a runway has an ILS DME approach to EACH end, then ONE of the ILS identifiers will bring up the SELECT DESIRED WPT page, asking you to select the ILS coordinate (localizer antenna) or the DME coordinate.



May 98

역학 신경위원 값의 1.0월.13

Fur-RA's no in die say daterer o regord AC spiedre

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The location of the E.H.H. Emility is are outhe clear , so there is no very to loave is advance what you will get the SHEET USER WAY WAY page.

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W qu H.S. approach does bet fifter a PAR, the highliter two and nutes will be fidded the foodlary injugate, V as superallified by bothing with others 5 Ref. 1348 (1-4), -3283 (3107) (201-333), p.

M nu 40.8 approach loss a ObBH, the stamples's "resultant will be due of the DMB amount, (unitant the divided BOUECT OESINEE WPT page estimates) in which man, and we get five anoth mass).

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May 01

REF NAV DATA

You get to this page by:

- INIT/REF index NAV DATA prompt (LSK 1R).

Provides a means to review Permanent or Temporary data stored in the data base. If the desired data is not stored in the data base, allows the crew to enter new data into the Temporary data base.



- EXISTING DATA BASE ITEMS:

Dash prompts:

Enter waypoint, Runway, Airport, or Navaid identifier. Data for entered identifier is displayed. OR Note: To display runway data, enter runway identi

Note: To display runway data, enter runway identifier in WPT IDENT (RWXX). Box prompts will appear for airport identifier. Enter ICAO airport identifier. Ref: Runway Entry next page.

- TEMPORARY DATA BASE ITEMS: (Examples on next page)

• Enter identifier in REF NAV DATA (box prompts will appear if entry is not already defined).

- Enter required data in the box prompts and EXECute.
 - Note: Runway data cannot be stored in the Temporary database.
 - VOR-only navaids must be accessed as wpts.
 - REF NAV DATA items may be deleted by using DEL key and EXECute, but only if the waypoint is removed from the ACTive flight plan and FIX page.
- All data stored in the temporary data base is cleared at flight completion (squat switch and ground speed less than 20 kts) or loss of power for more than 10 seconds.
- The U1.x FMC can hold up to 20 wpts, 20 navaids, and 3 airports in its Temporary
- database. U3 and up doubles these numbers; 40 wpts, 40 navaids, and 6 airports.



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May 01

SUPPLEMENTAL NAV DATA

U3.0 & up

You get to this page by:

- INIT / REF INDEX page (LSK 1R while on the ground after entering SUPP in the s/p).

SUPP NAV DATA and REF NAV DATA consist of separate sets of pages which have similar but distinct functions. The counterpart pages of each set have identical displays for Waypoint Data, Navaid Data, Airport Data, and Runway Data. The initial display of each set is unique.

 Either of the SUPP NAV DATA and REF NAV DATA pages can be used to review data (for Waypoints, Navaids, or Airports) which is already stored in any of the nav databases (Permanent, Supplemental, or Temporary). Runway data, which is stored only in the permanent database, can also be reviewed.

- When reviewing stored data, note that the page (SUPP or REF) which is displaying the data has no direct correlation to the specific data base in which the information is stored.

If the desired data is not already stored in data bases, the crew may use these pages to define new entries. The SUPP and TEMP databases share storage capacity for 40 navaids and 6 airports; the entries being stored in either database on a first come, first served basis. For the WPT catagory, exclusive storage is reserved in the TEMP data base for 20 entries (including those created on the RTE or LEGS pages). An additional 20 wpts (up to a max of 40) can be stored in either the SUPP or TEMP database on a first come, first served basis. When any storage capacity is full, entries which are no longer required should be deleted to make space for new entries. Created wpts cannot be stored in the database RUNWAY catagory.

(10.3 & up) SUPP NAV db increased to 40 wpts. The SUPP NAV DATA pages are accessible on the ground only by entering SUPP into the s/p prior to selecting the NAV DATA prompt on the INIT/REF INDEX page.

Nav database updating does not DELete the Supplemental entries.

Changing the OP PROGRAM will DELete it.

U6.0 & up — Select SUMMARY to view all currently defined Supp. and Temp. nav database items.	U3.0 & up EFFECTIVE FROM DATE LINE • Used for entry and/or display of the effectivity date (MONth, DaY, and YeaR) for data stored in the SUPP database. With a new entry, the EXECute key illuminates. • The entry must be EXECuted before any entries are permitted on the Identifier lines. • Entry propagates to the IDENT page. • If no entry is displayed, lines 1L, 2L, and 1R will not accept entries (no dash prompts).
SUPP NAV DATA WPT IDENT NAVAID IDENT AIRPORT IDENT SUMMARY > EFF FRM MON DY/YR UDU DU/UN SUPP NAV < REPORT REQUEST > < INDEX	 U6, U8, & up Fields 4L and 4R provide the capability of reporting or requesting SUPP nav data to or from the airline's ground station, respectively. Selecting the REPORT prompt causes the FMC to download the entire contents of the SUPP nav database. This prompt is only displayed when the database contains SUPP data. Selecting the REQUEST prompt requests SUPP nav data to be uploaded. Once selected, this field remains highlighted until the SUPP nav data loading is complete. After the data is loaded, NAV DATA UPLINK is displayed in the s/p to indicate that the loading is complete.

U3.0 & up

If the entered identifier is already stored in either the Permanent, Supplemental or Temporary data base, then relevant data propagates to the subsequent SUPP NAV DATA display.

If the entered identifier is not stored in any data base, the subsequent SUPP NAV DATA display contains box prompts. Following entry of the required information, the new data may be stored in the Supplemental data base by EXECuting (except runway data). Data is stored indefinitely, but may be subsequently cleared from the Supplemental data base : By DELeting an individual identifier after entry on line 1L, 2L, or 1R; or by using 6R to delete all Supplemental data if an ORIGIN has not yet been entered.

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To DELETE, the identifier(s) cannot presently be displayed on any other page, e.g. LEGS, or FIX.



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<INDEX

SUMMARY PAGES

U6, U8, & up

You get to this page by:

- REF NAV DATA page, SUMMARY prompt (LSK 2R) on.
- SUPP NAV DATA page, SUMMARY prompt (LSK 2R).

NO ENTRIES ALLOWED

- SUMMARY pages are provided to display the contents of the Temporary and Supplemental nav data bases.
- These pages provide a convenient means of reviewing waypoints, navaids, and airports that have been previously defined through crew entries.
- The SUMMARY pages include the position for each entry as a latitude and longitude, or as bearing/ distance from a reference, corresponding to how the entry was defined.
- They are organized such that the Temporary and Supplemental entries appear on separate sets of pages, and each set of pages lists waypoints, navaids, and airports separately.







MAINTENANCE



IRS MONITOR

- Computed 30 sec. after flight completion.
- It is the IRU Position Error Rate(PER) during the last flight for each IRU (nm/hr).
- The PER (drift) for the flight is computed by dividing the distance from the FMC position to the IRS position occuring during the flight by the total flight time.
- If the error rate for any IRU is greater than 2.0 nm/hr for 2 consecutive flights, consider a discussion with maintenance.
- The error rates are retained (unless a long-term power interruption occurs) until the next flight completion at which time the rates will be updated, or if no 2 dimentional updates have occurred in the last hour.
- If blank, monitor data for that leg was invalid.

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IRS L		in an
IRS C IRS R 0.8 NM / HR		1 T T
< INDEX		



MAINTENANCE



MAINTENANCE

MODEL / ENGINE CONFIGURATION



Abeam Waypoints (U10.0 and above) Alternate Destination (U10.0 and above) Altitude/Speed Intervention (U10.0 and above)

AOC Datalink (U10.0 and above)

- ATC Light & Chime on FIXED OUTPUTS page displayed (U10.4 and above)
- ATC Message on Map displayed (U10.4 and above)

CDU Color (U10.2 and above)

Engine-out SIDs (U10.3 and above)

- FANS-1 ATS DataLink (U10.4 and above)
- FMS RNAV ILS Look Alike Approach (U10.5 and above)

Geometric Descents (U10.3 and above)

- GPS Landing System Approach (U10.5 and above)
- GPS Operational Mode Bits 1 & 2 (U7.0/8.0 and above)

GPS Select (U7.0/8.0 and above)

Gross Weight Entry inhibit (U10.4 and above) VNAV ALT Enable (U8.0 and above)

High Idle Descent (U7.0/8.0 and above) Manual RNP (U7.0/8.0 and above) Manual Takeoff Speeds (U7.0/8.0 and above) Message Recall (U10.0 and above) Missed Approach on Map displayed in Cyan

(U10.4 and above)

Optional Quieting Gradient (U10.3 and above) Pilot-Defined Company Routes (U10.3 and above)

Plan Fuel (U10.0 and above)

QFE Altitude Reference (U10.0 and above)

Quiet Climb System (U10.3 and above)

Runway Offset/Remaining (in feet)(U7.0/8.0 and above)

Runway Remaining (U7.0/8.0 and above) Takeoff Derates disabled (U10.4 and above)

Takeoff Speeds certified (U10.0 and above) Vertical RNP Values loadable by default (U10.5 and above)

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ABNORMALS

ALTERNATE NAV

The Alternate Nav System is a GPS based system which provides nav capability independent of the FMS. The Alternate Nav System consists of the Alternate Nav CDU (ANCDU) and on-side GPS. In the event of FMC failure, the ANS provides a backup mode of operation which is immediately available for use.

Each Alternate Nav system operates independently, the left, the right. Each ANCDU performs its own computations based on inputs from its own GPS.

Keep in mind that the ANCDU has special features. AN stands for alternate nav. It has a memory chip and is able to store the FMC route, up to 60 wpts. The FMC automatically sends the current active route to the ANCDU. The ANCDU has no performance or nav database. Thus there is no stored information from which the desired wpts can be extracted by use of their identifiers.

Alternate Nav cannot drive the Maps and cannot provide LNAV to the FCCs.

The ANCDU does not perform VNAV computations, nor provide autothrottle commands. MCP can be used for this function.

The ANCDU cannot tune the VHF nav radios and does not use radio information for position updating.

Both ANCDUs are powered by transfer bus 1.

The ANCDU requires a moment to load the route from the FMC; therefore, it is recommended that the entire route be entered into the FMC either prior to departure or as soon after takeoff as time and duties permit, the ANCDU will probably contain most of the waypoints necessary to navigate to your destination following a dual FMC failure.

Wpts beyond the destination (missed approach procedure) and conditional wpts, are dropped from the flight plan.

The ANCDU flight plan can be in various states of activity. These possible states are inactive, active (ACT), and modified (MOD).

Only certain keys will operate in the Alternate mode; they are the EXEC key, the PREV PAGE and NEXT PAGE keys, the line select keys and the alphanumeric keys, including CLR, "/", ".", and "±".

Four ANCDU pages will be available after failure of an FMC; MENU, ACT IRS/GPS LEGS, ACT IRS/GPS WPT DATA, and IRS/GPS PROGRESS.

Route modifications are made on the ACT IRS/ GPS LEGS or ACT IRS/GPS DATA pages. A MOD page will display an ERASE prompt to readily facilitate changing back to the original ACT page.

The database of nav stations and waypoints is contained in the FMC, and since it has failed, you do not have access to it and cannot load waypoints by name not already in the flight plan. Note that the modifications must be made to each ANCDU independently; there is no remote loading or re-syncing of a route. The crew must exercise great care in modifying the route. The pilots must independently cross-check each other's entries.

Complete departure and arrival or approach procedures cannot be manually entered or crossloaded from the FMC. This is because the ANCDU does not accept undefined wpts or legs, that is, no fixed heading or course legs, and no conditional wpts.

For those of you who have experience in Inertial Navigation System (INS) equipped airplanes such as the DC-10 or B-747, the major differences may be summarized as follows:

- 1) Waypoints cannot be remotely loaded. Each pilot must make identical changes to the route.
- 2) The GPS position is much more accurate than the INS position.

If in MNPS airspace, notification of navigation system failure to ATC through the appropriate radio is required, but the airplane can still be navigated with sufficient precision in this configuration to remain in the Minimum Navigation Performance Specification (MNPS) airspace. Consult Company regulations for the specific procedures applicable to you.

ALTN NAV course deviation is only displayed on the ISFD (Integrated Standby Display). BBJ only.



ABNORMALS

ALIGN	ON DC	ALIGN	ON DC
FAULT	DC FAIL	FAULT	DC FAIL
ALICH			L
ALIGN	MAY ATT		*
		OFF	
	ATT	OFF	ATT

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When the aircraft is moved during alignment, the FAULT light illuminates steadily and the ALIGN light flashes.

To demonstrate while in flight, turn one IRU from NAV to ATT. Saves time by not going to OFF first.

The IRS FAULT light illuminated indicates the respective IRS system has detected a fault. The NAV mode (s) is no longer available, and in most cases the IRU can not be used in ATTitude

If an IRS looses both AC and DC power, the alignment is lost. Alignment can also be lost if the mode selector is moved out of the NAV position.

If alignment is lost in flight, the navigation mode (including present position and ground speed outputs) is inop for the remainder of the flight.

. . SELECT OFF THEN ATT This clears the fault and extinguishes the FAULT light. There may be a chance that ATT mode will work, depending on what the nature of the fault is. Allows the attitude mode to be used to re-level the system. Requires approximately 20 seconds of straight and level unaccelerated flight to complete the ADI leveling; a little longer for HSI leveling. Some attitude errors may occur during acceleration but will slowly be removed after acceleration. If the FAULT light reappears, the ATTitude mode is inop.

To provide heading information . . . ENTER MAGNETIC HEADING USING ISDU OR CDU

- To enter the magnetic heading with ISDU:
- 1. Place mode selector (s) in ATT.
- 2. Switch SYS DSPL to affected IRU.
- 3. Press $\begin{bmatrix} H\\ 5 \end{bmatrix}$ (for heading).
- 4. Enter compass heading using numeric keys. 4. Enter heading in SET IRS HDG
- 5. Press ENT

- To enter the mag heading with CDU:
 - 1. Place mode selector (s) in ATT.
- 2. Turn to POS INIT 1/3
- 3. Enter compass heading in s/p.

Crosscheck and verify heading with opposite AHRS or magnetic compass. Heading flags should retract from view on round-dialed aircraft. Heading indicator is re-

displayed for EFIS.

The IRS heading will precess up to 15°per hr. and must be updated periodically.

If the FAULT light reappears, the ATTitude mode is inop. Proceed:

Aircraft is equipped with an IRS TRANSFER switch:

MALFUNCTIONING IRS MODE SELECTOR . . . IRS TRANSFER SWITCH BOTH ON OPERATING SYSTEM Switches all associated systems to the functioning IRS. If the switch is moved with an autopilot engaged, it may disconnect.

Aircraft is not equipped with an IRS TRANSFER switch:

MALFUNCTIONING IRS MODE SELECTOR .	OFF
COMPASS SWITCH	BOTH ON OPERATING SYS.
ATTITUDE SWITCH	BOTH ON OPERATING SYS.
	ATTITUDE

OR

BOTH IRSs FAIL IN FLIGHT - B 737

Loosing **both** IRSs is a remote possibility, but a quick look at how it affects the pilot is in order.

The IRS's feed data to many important systems in the cockpit such as: ADI, HSI, Autopilot/ Flight Director, FMC, VSI (EFIS aircraft), and the Autothrottle. The most obvious equipment losses are both primary attitude indicators, flight directors, autopilot, and some of the features of the FMC. The sole source of attitude information is now the standby horizon. Heading must be obtained from the magnetic compass. What this means to the pilot is that his instrument crosscheck just became a real problem. The distance between the magnetic compass and the standby horizon is significant, especially if "IMC". Crew coordination on a higher than normal level is required due to the technique for making instrument turns on the standby compass. Remember all the basic rules for turns on the standby compass? Also, if an approach is required, crew coordination really becomes critical when trying to coordinate the turns and headings with the VOR/ ILS performance readouts on the HSI without heading inputs.

Some performance indicators are lost such as the VSI on EFIS aircraft. However, pressure altitude is available on both the electric and pneumatic indicators. Radio altitude is displayed as normal. The Mach and IAS are operative on the electromechanical indicator (if installed), fast/slow indicator (if installed) and the speed tape (if installed). Airspeed is also available on the pneumatic standby indicator. Groundspeed is inoperative but TAS is displayed on the last PROGRESS page.

The MCP is inop except for the IAS/MACH window, course selector and altitude display. The IAS/MACH window sets the target airspeed bug. The course selector sets ILS and VOR courses which are displayed as normal on the MCP and HSI. The altitude selector triggers the altitude alert system.

Timing or "Dead Reckoning" after the IRS shutdown can assist in determining the airplane's present position since the FMC is no longer receiving position data and the EHSI MAP display is gone. Magnetic bearing to the VOR and DME may or may not be available on the RDMI's depending on avionics installation, but the card is fixed which eliminates the relative bearing function. The ADF bearings are still functional and indicate only the relative bearing from the nose of the airplane. The GSI and CDI on the HSI (in VOR/ILS mode on EFIS aircraft) are operative in both VOR and ILS operation but only provide sensed magnetic bearing information, not relative bearing. The glide slope and localizer indicators on the standby ADI also operate (if installed).

The FMC still provides many perfomance computations such as approach speeds and N1 targets but can not compute any navigation information due to the loss of position data input from the IRS. Therefore, both LNAV and VNAV are disabled. The following is a brief rundown of what the FMC still provides on its pages following the loss of both IRS's.

CLB, CRZ, and DES pages.

No ETAs, fuel predictions or waypoint altitude predictions, but, displays N1 values, airspeed restrictions and target speeds. Pages may sequence to the next phase of flight automatically provided waypoints are manually sequenced by the crew and other conditions are met.

- DEP/ARR page operates normally.
- HOLD page operates normally except no ETA or HOLD TIME displayed.
- IDENT page operates normally.
- N1 LIMIT page operates normally.
- PERF INIT page 1 operates normally. On U4.0, page 2 of PERF LIMITS operates normally, but th RTA is inop.
- POS INIT page displays the last FMC position prior to IRS failure. Page(s) 2 and 3 (U4.0 only) are blank.
- PROGRESS pages retains fuel remaining and time over last waypoint, but no ETAs, DTG or fuel estimates. Also, the FMC will not autotune navaids. On U4.0 only, the RTA page is inop. The last PROGRESS page still displays true airspeed, SAT and ISA deviation.

REF NAV DATA operates normally.

- RTE pages retains normal information but does not sequence waypoints automatically.
- RTE LEGS page retains flight plan waypoints entered prior to failure and new waypoints may be entered. The courses between waypoints are displayed for all but the active waypoint. It retains altitude and airspeed predictions entered prior to IRS failure and allows new entries. On EFIS aircraft, the PLAN mode operates as norma' with the CTR STEP prompt.



DC FAIL light on indicates the respective IRS DC power is not normal.

IRS DC power is inop. If all other IRS lights are extinguished, operate normally.

IRS DRIFT (Dual FMC Installation) (Failed or no GPS)

FAULT LIGHT ON - ON GROUND



The Built-In-Test (BIT) function of the FMC provides continuous monitoring of the "state of health" of the FMC and CDU. Should any system failures be detected, FMCS functions then decide if downmoding to lower levels of capacity are necessary. The FAULT light will illuminate when a critical failure is sensed.

FMC

NORMAL

BOTH

ON R

BOTH

ONL

When the aircraft is moved during alignment, the FAULT light illuminates steadily and the ALIGN light flashes.

ON GROUND:

- NOTE: Placing the MASTER DIM & TEST switch to TEST for 10 seconds may preclude this fault when associated with the first alignment of the day.
- 1. Turn MSU mode select switch to OFF. Wait until align light is out (± 30 sec).
- 2. Verify that aircraft is not moving. Set parking brake.
- 3. Turn mode select switch to NAV.
- 4. After align light is on, enter correct present position twice. Wait normal 10 minutes for the IRS to enter NAV.

NOTE: If FAULT light illuminates while on landing rollout, the laser beam may be getting weak. Consider advising maintenance.

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ENTER IRS POSITION message appears.

PROMPT / MAINTENANCE Codes will appear concurrently with a flashing align light. (HDG/STS position)

CODE 03	Excess motion detected. IRS MOTION message. Steps 2 thru 5.
CODE 04	Significant difference between previous and entered positions or an
	unreasonable present position entry.
CODE 08	Present position not entered. Enter present position.

A flashing align light requires some pilot action. This procedure will always allow recovery from flashing align lights not caused by equipment failure.

Select the NAV mode and enter the correct identical present position twice.
 Ref: Reasonableness Test, System Description.



2. Turn MSU mode select switch to OFF. Wait until align light is out (about 30 sec).

3. Verify that aircraft is not moving. Set parking brake.

4. Turn mode select switch to NAV.

 After align light is on, enter correct present position twice. Wait normal 10 minutes for the IRS to enter NAV.

> Any time the crew sees a single or dual FMC failure, trouble shooting data is recorded by the FMC. This data can be written to a disk by a maintenance procedure and sent to the vendor to discover the cause of the failure so that it can be corrected in subsequent versions. For this reason it is very important that you inform maintenance as soon as possible of such a failure.

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FMC FAILURE ON THE GROUND

E-8 on P-18-3 (CMPTR) PULL FOR AT LEAST 15 sec. and RESET NOTE: Maintenance can accomplish the same thing by pressing a RESET switch on the FMC in the avionic bay.

RECORD ANY STATUS CODES

If FMC failure occurs after a complete power down, the failure may be due to a dead internal FMC battery. Maintenance will have to reload the data base. A dead battery in flight will have no affect as ship's power will be the current source.

FMC/CDU FAILURE (Single FMC installation)

The FMC alert light and CDU FAIL light(s) illuminated indicates either an FMC failure (both CDUs display FMC) or a CDU failure (associated CDU display blanks). Check FMCS C/Bs on P18-2 panel (behind Captain): E - 8.

If an FMC Failure (or CDU failure with a single CDU installed):

The FMC/CDU is inop; L NAV and V NAV are inop.

Resume conventional navigation.

An attempt may be made to recover the FMC by pulling the CBs for at least 15 seconds. Pulling computer CBs should be regarded as a last resort method only.

On FMA FMC P/RST =

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DUAL FMC FAILURE

Indications:

- The $\begin{bmatrix} v \\ T \end{bmatrix}$ flag will appear on both EHSIs.
- The FMC Alert light will illuminate.
- Both CDU FAIL lights illuminate and both CDUs will fail.
- LNAV and VNAV will disengage
- 25-30 seconds later, the MAP flag (yellow) appears. All FMC data disappears from both EHSIs.

Check FMCS CMPTR C/Bs:

No. 1 on P18-3 panel (behind Captain): E-8

No. 2 on P6-1 panel (behind FO): B-9

An attempt may be made to recover an FMC by pulling the CBs for at least 15 seconds. Pulling computer CBs should be regarded as a last resort effort only.

205

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FAIL

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E

BRT

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Accomplish the following steps when you suspect an IRS "drift" to be excessive. POS SHIFT page, differences in wind readout of left and right IRSs in flight, large discrepancies in lat/lons on POS page 2/2, and/or high groundspeeds at the gate, all can indicate excessive IRS drift. Note: Your company may require 2 consecutive flights with the error on each before write up.

- RESIDUAL GROUND SPEED TOLERANCE

Groundspeed readout must be taken before the airplane has been stationary for three minutes because the system may zero the display.

a. Set the suspect IRS's DSPL switch to its own position (L or R).

b. Set DSPL SEL switch to TK/GS.

- c. When stationary, the display shows the residual groundspeed error.
- d. If the residual g/s error is greater than 20 kts, consult maintenance.

- RADIAL POSITION ERROR TOLERANCE

To accomplish the following steps, each IRS Mode Select switch must remain in the NAV position after flight. This is to preserve the IRS position coordinates. These coordinates are displayed on the POS REF 2/2 page.

In the following steps, the airplane's present position and IRS position are entered into the LEGS 1/1 page. When entered, these positions are displayed as waypoints and the distances are compared.

- a. Enter any route on the RTE page. Use your present position as the Origin airport. EXECution is not required.
- b. Press LEGS key.

AND

- c. Enter airplane present position coordinates (use gate position or figure present position from airport diagram) into the first waypoint position. (Decimal points and trailing zeros optional) Displays as WPT01.
- d. Press the INIT REF key, then NEXT PAGE. POS REF 2/2 page is displayed.
- e. Transfer position of the suspect IRS from POS REF 2/2 page into the scratch pad and then select LEGS page. Place the IRS position coordinates into the second position on this page (LSK 2L).
- f. Note the distance and bearing from WPT01 to WPT02. This represents the Radial Position Error (displayed in nautical miles) for the IRS chosen.
- g. To check the other IRS, transfer that IRS position coordinate from POS REF 2/2 page into the scratch pad and then select LEGS page. Place these IRS position coordinates into the second waypoint position (behind WPT01).
- h. Note the distance and bearing from WPT01 to WPT03 (actual coordinates on ground to where IRS thinks it is). This represents the Radial Position Error for that IRS.



i. A position error exceeding the value of the chart is considered excessive. If it is excessive, consult maintenance.

The equation $\frac{3+3T}{T}$ may also be used. T is the hours in the NAV mode (since full alignment). EXAMPLE: 2 hr. time in NAV.

3 + (3x2) = 9/2 = 4.5

If the Radial Position Error exceeded 4.5 nm in this case, that particular IRS has excessive Radial Position Error.

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DISAGREEMENT BETWEEN FMCs (Dual FMC installation)

When a disagreement occurs between the left and right FMC, the right FMC "condition fails" and is unavailable. A solution to this software problem is being sought.

dications:

- FMC Alert light and FMC Message light illuminate.
- ETA and Distance To Go data only blanks on right MAP, CTR MAP, and PLAN.
- 30 seconds later, the MAP flag (yellow) appears. All FMC data disappears from the right والمتحديث الخرية والشراب والمترا
- MAP, CTR MAP, and PLAN modes.
- Message, SINGLE FMC OPERATION appears in scratchpad.

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flag does not appear with a disagreement between the two FMCs. If the flag appears, refer to SINGLE FMC FAILURE (Dual FMC installation) - p.132

	FMC		
BOTH	ଭ	BOTH	
ONL	Ŷ	ONR	
	NORMAL		

The right FMC is commanded to re-sync with the left. Allow several minutes for resync. Note: Any switch movement initiates a re-sync.

Message DUAL OPS RESTORED appears in scratchpad.

Re-sync is successful. Do not record in the maintenance manual.

Message DUAL OPS RESTORED does not appear in scratchpad.

Re-sync is unsuccessful. Continue with single FMC operation. After landing, attempt recovery by complete power down.

STEPS Go to the INIT/REF INDEX Press MAINT prompt (6R) 1 MAINT BITE INDEX Press FMCS prompt (1L) 2 3 Displayed BITE Press INFLT FAULT prompt (1L) 4 INFLT FAULTS Record abnormalities from any of the 3 pages 5 6 Displayed FLIGHT SELECT Press FLIGHT X* and record 7 8 Displayed FLIGHT SELECT Press the next FLIGHT and record 9 Continue in this fashion until all faults are recorded. 10 Go back to the BITE page by pressing INDEX . . . Press the FMC R prompt (2L) 11 Follow steps 4 thru 10 to record faults for the right FMC. 12 13 Take this data to maintenance. 14

Space exists in memory for the last 10 flights. If an anomaly has occured it will be labeled FLIGHT X (Example: FLIGHT 4 would mean an irregularity occured on the fourth flight ago.)



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ON DC LIGHT ON

The IRS is operating from the BATT BUS (limited to 5 minutes for the right IRS).

NO or OUT-OF-DATE DATABASE

Check the MEL.

If you are allowed to dispatch without a database, choose one of the steps below.

OR

Short on time.

- 1. Align the IRUs. Use the POS INIT page to manually enter the lat / Ion position. Have your crew double-check your entry.
- 2. Navigate using groundbased navaids.
- Inform your dispatcher and ATC of your status. ("slash alpha")
- 4. Select EXP VOR or FULL VOR. TCAS and radar can only be viewed on EXP.
- 5. Do not use Map, center Map, LNAV, or VNAV.
- FMC probably has the performance database, so if the PERF INIT and TAKE-OFF REF pages are completed, the autothrottle can be used.

Lots of time.

- 1. Using the REF NAV DATA / AIRPORT, build the ORIGIN AND DESTination airports. Lat / Ion is required and can probably be found on your Jepp 10-9. Have your crew double-check your entry of the ORIGIN airport.
- 2. Align the IRUs. Use the POS INIT page to enter the REF AIRPORT position.
- 3. The FMC probably has the performance database, so if the PERF INIT and TAKEOFF REF pages are completed, the autothrottle can be used.
- 4. Define your nav fixes using the REF NAV DATA page. You will use the WPT and NAVAID fields.
- 5. It may be difficult to find the lat / Ion of waypoints (WPT) and VORs. Your flight plan may have this information.
- The CLASS entry for VOR requires specific entry. Refer to the page that describes REF NAV DATA / VOR entries in this book. VDH should always work. You may have to estimate the elevation.
- Define VORs alongside your route using the same method. Choose VORs that are within 200 miles of your centerline. The FMC will use these to update its position. If the flight is long and time is short, define just the ones you need at the beginning of the flight and do the others enroute.
- 8. After all the fixes are defined, you can build the route leg-by-leg on the RTE or LEGS pages, but first enter the ORIGIN and DEST airports.
- 9. Updating will take place, but will not be as accurate as normal.
- 10. Use Map for position awareness.
- 11. Enroute, the applicable ground based navaid must be displayed and is controlling; however, LNAV can be used if you've built the necessary fixes. Using LNAV is much smoother than following a VOR that *scallops*.

POWER LOSS and SENSOR FAILURE RECOVERY

The FMC and both CDUs are powered indirectly by transfer bus No. 1. The FMC is designed to survive power transients and interruptions without suffering permanent loss of its navigation and guidance capabilities. Three modes of power loss recovery are possible:

- 1 If electrical power has been interrupted for less than 10 seconds, VNAV and LNAV disengage, all entered data is retained by the FMC, and the system will continue to operate normally as if no interruption had occured.
- 2 If the power has been interrupted for 10 seconds or more while on the ground, the system goes through a complete power-up procedure. All preflight data and flight plan entries must be re-entered when power is restored, including those in the Temporary nav data base.
- 3 If the power has been interrupted for 10 seconds or more in flight, the system retains all loaded data, LNAV and VNAV disengage, and when power is restored, the CDU reverts to display of a MOD LEGS (page 1/1) with a SELECT ACTIVE WPT / LEG message in the scratch pad. The system will not illuminate the EXEC key until or unless TO waypoint has been defined and a valid radio updated nav mode is available.
- NOTE: A software "restart" which results from the FMC entering an impossible computational state, such as division by zero, will appear to the pilots to be a temporary loss of electrical power. The CDU will momentarily blank and then display "FMC".

This is followed quickly by the display of the **MOD** RTE LEGS page with box prompts in the active waypoint line.

The message SELECT ACTIVE WPT / LEG will be displayed.

In some cases, multiple software restarts inflight will result in FMC failure. The FMC may be re-initialized by removing AC power for more than 10 seconds after landing.

Mag. ggrager Mau,

RIGHT FMC FAIL DURING PREFLIGHT (Dual FMC installation) (under development)

During *boot-up* of a dual FMC configuration, many comparisons must take place. If any comparisons do not match, the slave, or right FMC, will declare itself invalid. There is much cross-talk going on and usually the FMCs will solve this problem if left alone. It may take 15 minutes. The keyboard will not accept entry while this cross-talk is taking place. The right FMC may come on-line, and drop off-line a few times.



. If the right FMC does not stay on line or you run out of time:

- Place the FMC swith to BOTH ON L This copies the flight plan, perf data, etc, into the problem computer. Note: Do Not place the FMC switch to the side with the bad computer.
- 2. Both Maps will now function and keyboard action will resume.
- 3. You may get a DUAL OPS RESTORED message later on at which time you can place the FMC switch to NORMAL.
- Tell maintenance as the FMC stores these faults. Smiths Industries would like to get this stored information to help solve the problem.

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When the display select switch is turned to HDG/STS, the highest priority malfunction code is displayed. If another code bit is set, the cue light on the CLR key lights. The next highest priority code will be displayed after the CLR key is pressed. Continued pressing of the CLR key will cause the display to "roll over" from the lowest priority code back to the highest priority. If the code being displayed "goes away", the next highest priority code will automatically be displayed.

PROMPT/MAINTENANCE CODES

01	ISDU FAULT Maint reg'd	Replace ISDU
02	IRU FAULT: Possible maint req'd	Complete the FAULT LIGHT ON procedure. If necessary, check IRS and FMCS BITE (Current and In-Flight Faults Interface Check). Fault is Critical or Non-Critcal (no flag on instruments).
03	EXCESS MOTION IN ALIGN	MSU switches OFF, wait 30 seconds for ALIGN lights to go OFF. Perform 10 minute align.
04	ALIGN PROBLEM	Perform procedure from Abnormals section.
05	DAA FAULT (LEFT) Maint req'd	Check IRS and FMC BITE (Current and In Flight Faults, Fixed Outputs, Interface Check).
06	DAA FAULT (RIGHT) Maint req'd	Check IRS and FMC BITE (Current and In Flight Faults, Fixed Outputs, Interface Check).
07	ADC FAULT: Maint req'd	Check FMC BITE (Sensor Status should show same ADC-FAIL) Code 07-IRU receiving Fail Warning from ADC.
08	ENTER PRESENT POSITION	Enter Lat/Long Code 08 if 10 min. elapsed without entry.
09	ENTER MAG HEADING (ATT)	Enter magnetic heading on CDU or ISDU. Code 09 after 30 seconds in ATT mode. HDG flags in view until magnetic heading entered.
10	ISDU POWER LOSS	Check power to IRS's. ISDU power not received from one IRU.

SYSTEM TEST



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Temporary

There are two catagories of CDU messages. The generation of any message causes the white CDU MSG light to illuminate.

Alerting (A) messages have the highest priority and identify a condition which must be acknowledged and corrected by the crew before further FMCS-guided flight is advisable or possible. These messages appear in the scratch pad as they occur and displace any lower priority messages. Alerting messages also illuminate the amber \boxed{PAST} alert light on each pilot's FMA.

Entry error advisory (*EE*) messages have lower priority and inform the crew of CDU entry errors or system status regarding readiness for operation or prediction of profile parameters. These messages do not replace data which is already in the scratch pad.

System advisory (SA) messages inform the crew that changes made cause unattainable conditons, or ase ued to verify the changes.

ACARS/ATC messages provide status of the ACARS sstem and data transmissions. This option requires at least one of the FMCS displays to be a MCDU type. ACARS messages are not included in this manual.

When multiple messages are generated, they will be stacked for display in priority sequence, or in the order of their occurance if of the same priority. For this reason, it is important to clear your messages. As each message is cleared, the next message in the stack is displayed. Most messages are cleared with the CLR key, or by correcting the condition. Other messages are cleared by changing the displayed page; this will delete the entry which caused the message.

The queue is layered in the following sequence: ATC Uplink Pending messages

Entry Error Advisory messages

Only displayed on the LCD the error was generated on.

Manually entered data

ACARS Uplink Alerting messages

Alerting messages (active flight plan)

Alerting messages (mod flight plan)

Advisory messages

If these messages pertain to specific data on a specific display page, the message is only displayed when that page is viewed.

ACAS system level messages

The CDU MSG light remains on until all awaiting messages have been displayed.

Non Entry error messages will re-appear after alpha-numeric data entry is complete.

Alternate Nav (AN) messages applies to MCDU or FANS MCDU with 10.2 when displaying the alternate nav pages. These messages cause the MSG annunciator to illuinate.

your messages.				in or a fille to a to a f	ACT	RTE LEGS	6 1/3
					^{99°} NEPTA	2.8 NM	.745 / FL3700
	/				98° WPT01	40 NM	.745 / FL3700
	A/P P/PST	A/T	FMC @		COVIA	120 NM	.746 / FL3700
Land (all to part of	P/hST	FINST	TES		90° BLOND	84 NM	300/10000
	•	adden a			90° PIE	25 NM	180 / 3500
					RNP / ACTUAL	NLY	RTE DATA >
			and a strong of		X	<u>, 11</u>	
		Exa	ample of an				
	BRT	ALI	ERTING mes	ssage.	ACT	RTE LEGS	G 1/3
					94° FST	48 NM	.745 / FL3700
		/			JCT	165 NM	.745 / FL3700
	Ğ	Ex	ample of a	1	82° CLL	176 NM	300/21400
		A	VISORY me	essage.	CUGAR	23 NM	300 / 13255
				D	127° HOAGI	11 NM	250 / 10000
					BUFFET AL	ERT	RTE DATA >
					1		

MESSAGES

MESSAGE	CAUSING CONDITION	CORRECT ACTION		
ABOVE MAX CERT ALT <i>(SA)</i>	Aircraft has exceeded its maximum certified altitude.	n Descend to an altitude below maximum certified altitude.		
ACARS ALERT	Crew action required for ACARS.	Select ACARS MU on an MCDU and perform necessary action. Clear message.		
ALT CONSTRAINT AT XXXXX (Altitude value)	Added or modified constraint conflicts with existing downtrack constraints.	Clear message and revise entry.		
APPRCH VREF NOT SELECTED (SA)	VNAV req'd. FMC is in approach en- vironment and VREF has not been se- lected.	Select VREF on APPROACH REF page.		
ARR N/A FOR RUNWAY <i>(SA)</i>	Runway or approach does not match up with the selected arrival procedure.	Modify selection (ARR page) or manu- ally clear message.		
BUFFET ALERT <i>(SA)</i>	Current conditions result in maneuver margin less than specified. Speed greater than hi speed buffet, lower than low speed buffet, or altitude greater than buffet limited altitude.	Check current airspeed and altitude as compared to buffet limits. Bring aircraft back within operating envelope. U1.3/3.0 has a pad of 5 kts and 300' built into the logic that issues the messages in		
		order to reduce nuisance messages.		
CHECK FLIGHT PLAN	The FMC has found, thru its periodic Cyclic Redundency Check, an internal code error (checks parity bits on each word in NDB). The FMC can correct a single bit error, but no more. If it finds an error larger than one bit it gives up and wipes out the nav database and the flight plan.	Check the flight plan and other dis- played data on the CDU. If the FMC finds an error larger than one bit, it gives up and wipes out the NDB and any flight plan data. NAV DATA BASE INVALID appears in the s/p.		
CHECK FMC FUEL QUANTITY <i>(SA)</i>	A 1500 lb decrease in fuel quantity inputs to the FMC for a period over 120 sec. Also appears if there is a power interruption to the left bus. Must be manually cleared.	Check fuel quantity indicators. Verify FMC fuel from flight plan or fuel used data. Possible quantity sender failure or a failure within the Fuel Summation Unit.		
CRZ ALT CHANGED TO XXXXX <i>(SA)</i>	CRZ ALT changed automatically to match the highest wpt altitude con- straint in the procedure that you have just selected.	No action should be necessary other than to verify the new CRZ altitude.		
CHECK ALT TARGET	Aircraft altitude incompatible with VNAV engagement. Aircraft is be- tween MCP ALT and VNAV target altitude, and VNAV won't engage or just disconnected.	Reset MCP altitude.		
CUTBACK UNAVAIL- ABLE <i>(A)</i>	FMC is unable to compute a Cutback N1 value.	Clear the message.		

May 01	MESSAGES	LINKD: LARBER
MESSAGE	CAUSING CONDITI	ON CORRECT ACTION
CYCLE IRS OFF - NAV (A)	IRS logic requires manually restarting alignment.	Move IRS control to OFF, then to NAV.
DATA BASE FULL <i>(EE)</i>	Entry attempted has exceeded capacity of the Temporary nav data base.	Go to REF NAV DATA or SUPP NAV DATA pages and delete unneeded tem- porary wpts, navaids, or airports.
DATA BASE INVALID <i>(A)</i>	The automatic validity test of the nav database done at power-up has failed. Likely a multiple bit failure the FMC could not correct.	Advise maintenance personnel to reload data base or repair equipment. Consider use of Temporary nav data base.
DES PATH UNACHIEVABLE	After the descent is active, the FMC predictions show the profile constraints at the next wpt cannot be made and the path maintained. Displayed if the required flight path angle to meet the next altitude constraint exceeds 7° for aircraft operation when more than 1,000' above the airport speed restriction altitude; otherwise 6°. VNAV will disengage (CWS)	Modify the active LEGS or DES page plans re-engage LNAV and VNAV.
DISCO INSRTD AFTER XXXXX (WPT identifier) '4)	Geometry of the next wpts will not allow the FMC to fly the plane without bypassing more than one wpt.	Amend the active flight plan.
DISCONTINUITY (A)	Passing last wpt in the plan prior to a Route Discontinuity (LNAV disen- gages), or pressing LNAV while in a discontinuity.	Select RTE or LEGS to specify the wpt (s) for a continuous plan.
DRAG REQUIRED <i>(SA)</i>	Due to unforecast conditions, the air- craft is 10 kts or more above FMC target speed, or within 5 kts or .01M of V_{MO}/M_{MO} . (PATH DES only).	Use speedbrakes or change drag as re- quired to bring aircraft to within 5 kts of FMC target speed.
DUAL FMC OP RESTORED (A)	Movement of the Source Select switch position has caused a resynchroniza- tion and dual operation is restored, or the Source Select switch position has not changed, and is in either BOTH- ON-LEFT or BOTH-ON-RIGHT and	None required.
	the FMC has automatically restored DUAL after 5 minutes.	
MESSAGES

MESSAGE	CAUSING CONDITION	CORRECT ACTION
DUPLICATE FLIGHT PLAN ID <i>(EE)</i>	The entry attempted is a duplicate of an existing supplemental flight plan name.	Clear the message and select a unique flight plan name.
END OF OFFSET (A)	2 minutes prior to passing the offset leg termination.	Go to RTE or LEGS and enter the de- sired waypoints.
END OF ROUTE (A)	Passing the last wpt in the route (LNAV disengages).	If desired, go to RTE or LEGS and EXECute a route modification.
ENG OUT SID MOD (A)	An ENG OUT SID has been automati- cally inserted into the flight plan as a modification.	Clear the message.
ENTER IRS POSITION (same as Re-enter Position) (A)	IRS is in the alignment mode; it needs PPOS, entry did not go through, or there was a mis-compare of 1° or more with the stored PPOS.	CAUTION: Re-enter IRS position. If present position was previously entered, overwrite displayed data. If necessary, enter present position directly into the IRS CDU.
FMC APP MODE UNAVAILABLE <i>(A)</i>	The approved FMS approach cannot be performed. The final approach angle check may have failed.	Verify QFE is not selected on AP- PROACH REF page. Verify correct FMS approach is selected.
FMC APP/TUNE DISAGREE <i>(A)</i>	An FMS approved approach is in the active FP and an approach navaid (ILS/GLS) is being tuned with G/S on.	Turn G/S off. Clear message.
GPS FAIL <i>(AN)</i>	GPS data is not being received	Clear message. ALT NAV processing halts.
GPS INTEGRITY LOST (AN)	GPS data received is invalid or the GPS HIL value is greater tan two times RNP for the current nav environment.	None.
HOLD AT XXXXX	Holding fix was entered on the RTE LEGS HOLD AT page that is not on the active route.	Place offroute wpt in proper sequence and complete HOLD entries.
INSUFFICIENT FUEL (A)	Estimated fuel at destination is less than 2000 lbs (900 kg).	Modify flight plan or cruising altitude, or divert for fuel.
INVALID DELETE (EE)	DEL key operation attempted for a data line not allowed.	Clear message and repeat entry with correct data.
INVALID ENTRY <i>(EE)</i>	Attempted data entry has incorrect for- mat or range for the selected data line.	Clear the message and select proper field after DEL key is pressed.
INVALID OFFSET <i>(SA)</i>	The leg is not offsettable, too short or starts at a wpt followed by a DISCO. This entry may be from an ACARS uplink. An ACARS uplink may also cause the message if a start wpt was uplinked, followed by a disco or end of flight plan dashes.	Close DISCO or enter a valid wpt in end- of-flight-plan dashes.

TEMPORARY

MESSAGES

MESSAGE INVALID QUAD (EE)

IRS MOTION (A)

in need for re-alignment.

IRS NAV ONLY

Messages inhibited in approach environment when VOR/LOC mode is active from DFCS, both VOR receivers are manually tuned to the Procedure navaid, a valid VOR data is being received, or aVOR/ ILS mode is displayed on at 'ast one EHSI.

CAUSING CONDITION

The QUAD/RANGE entry is incorrectly formatted or is out of range for a PBD wpt from a VHF navaid.

IRS has detected motion during alignment resulting

Discontinued in U10.3

U7.1 and up: Actual Nav Performance (ANP) exceeds Required Nav Performance (RNP). Current default values are:

ENVIRONMENT		TIME TO ALARM
OCEANIC	12.0 nm	80 sec
ENROUTE	2.0 nm	80 sec
TERMINAL	1.0 nm	60 sec
APPROACH	0.5 nm	10 sec

U6 and below: FMC has down-moded to IRS only mode of navigation. Transition from one of the radio updated nav modes to IRS dead reconing occurs 15 seconds after radio measurements lost.

Radio updating has not been available for 12 min above or 10 min. below 15000'.

U5.0. Updating does not resume within 2 minutes of a reference IRS switch or an FMC nav program reset.

After an FMC POS SHIFT to an IRS position, the message will display if updating has not occured for 2 minutes in U5 or 1 minute in U4.0.

U5.0. After an inflight power up of the FMC, the message displays if updating has not occured for 2 minutes.

CORRECT ACTION

Ckar message and repeat entry with correct data for desired field.

If automatic realignment has not started, then move the IRS mode control knob to OFF, then to NAV.

Clear message and check nav radios are set for AUTO tuning. Allow radios to be tuned by the FMC.

Check aircraft position. U6 and down: If on an ILS, consider allowing one radio to autotune until on final approach.

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MESSAGECAUSLNAV BANK ANGLELNAV roll comLIMITED (A)tude maneuveriror buffet based	ING CONDITION mand during high alti- ng is limited to the thrust bank angle limit. ontal figure of merit is IP for the current nav	CORRECT ACTION None	
LNAV BANK ANGLE LNAV roll com LIMITED (A) tude maneuverir or buffet based	mand during high alti- ng is limited to the thrust bank angle limit. ontal figure of merit is VP for the current nav	None	
	ontal figure of merit is VP for the current nav	None	
LO POS ACCURACY The GPS horizor (AN) greater than RN environment.			
LOC CAP ACTIVE <i>(SA)</i> Aircraft is appr the localizer co an intercept hea	coaching its turn onto urse and will maintain ding.	Clear message manually or wait for AFDS to signal reset to the FMCS.	
LOC CAP CANCELLED Flight plan mo (SA) craft condition of izer capture.	difications or the air- did not facilitate local-	Clear message manually.	
MAX ALT FLXXX (A) Altitude entry (Flight Level value) (current capabil	is above max altitude ity-1.3g U.S.A.)	Clear message and amend data entry in scratch pad.	
MAX MACH .XXX (SA)In manually sMAX CAS XXXmode, cruise alMIN MACH .XXXentered will resMIN CAS XXXspeed.	elected cruise speed ltitude or target speed ult in limit on selected	Clear message; accept limited speed for new altitude, or modify selected altitude or speed.	
MCP APP DISARM A change in the proach was uplication of the proach was upl	ne expected FCC ap- nked when the mode is or engaged.	Review and accept or reject modifica- tion. Change approach type on ARRIV- ALS page.	
MISSED CAPTURE (A) Proper localizer formed, but AF	capture maneuver per- DS did not capture.	Clear message manually.	
MODEL / ENG DATA A valid perform INVALID (A) available.	nance database is not	Contact maintenance.	
NAV DATA LOADING Supplemental n is loading into t	av data from ACARS he FMC.		
NAV DATA OUT OF Nav data base et match Captain's	ffectivity date does not s clock date.	Check the clock date and correct if nec- essary. Otherwise, select effective nav data base or have maintenance reload new nav data base.	
NAV INVALID-TUNE FMC is unable XXXXX (A) (Navaid ID) approach proce	to autotune or receive dure navaid.	Cross-check radios and manually tune specified navaid.	
NO ACTIVE ROUTE LNAV is select been activated.	ted when no route has	Clear message and activate route or de- select LNAV.	
NO DES PATH AFTERThe profile coXXXXX (SA)achieved and tl(Waypoint identifier)planned after th	onstraints cannot be ne path maintained as e named waypoint.	Modify speed or altitude restrictions on the LEGS page.	
NO OFFSET AT LEGEntry of lateralXXXXX (EE)for a leg that is	offset start or end wpt non-offsettable.	Review offset plan. Enter a valid start or end wpt.	

MECCACEC

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MESSAGE	CAUSING CONDITION	CORRECT ACTION
NOT IN DATA BASE <i>(EE)</i>	FMC does not contain the required data for the entered indentifier.	Clear message and check data entry, or enter required information into Temp or Supp nav data base via REF NAV DATA page.
NOT IN FLIGHT PLAN (EE)	RTA wpt or lateral offset start/end wpt entry is not in active FP.	Clear message and amend entry.
NOT ON INTERCEPT HEADING <i>(SA)</i>	Present heading (HDG) or course (TRK) does not cross the leg to be captured, or its backward extension, or it is not within 3 nm of the desired leg and LNAV is engaged.	Manually steer aircraft onto a heading which will intercept the active leg of the planned route and engage LNAV.
OFP MISCOMPARE	Primary FMC has detected a discrep- ancy between its software and that of the secondary FMC.	Contact maintenance.
OFFSET DELETED <i>(SA)</i>	The entered start wpt has been deleted from the FP.	Clear the message and amend the route.
OFST ENDS ABEAM XXXXX <i>(SA)</i>	An invalid offset leg exists between the end wpt and the start of the offset or no end wpt exists.	Clear the message and amend the route.
OFST ENDS AFTER XXXX <i>(SA)</i>	Planned lateral offset path cannot be back by the selected end wpt.	Review offset plan. Enter a valid end wpt.
OFST ENDS BEFORE XXXX	A non-offsettable leg exists prior to the end of the offset plan.	Review and change offset plan to avoid non-offsettable legs.
op program Invalid	A fault is detected in the program memory.	Pull the FMC CMPT circuit breaker for 20 seconds and reset. This will re-boot the computer.
OVERSPEED DISCONNECT (A)	Aircraft exceeds airport speed restriction by more than 15 knots or more while below speed restriction altitude.	Slow aircraft to within 10 knots of speed target and re-engage VNAV or clear message manually.
PARTIAL ROUTE LOADED <i>(A)</i>	A route is loaded which references data not contained in the database.	Clear the message.*
PATH DES NOT AVAILABLE	Within 5 nm or T/D, a path descent is planned, and a computed path is not available.	Execute a speed descent if desired, or construct an acceptable path, or use MCP for descent.

MESSAGE	CAUSING CONDITION	CORRECT ACTION
PERF DEFAULTS INVALID /DELETED <i>(A)</i>	Loaded Perf Defaults table failed CRC check and was deleted.	Maintenance must reload table.
POSITION UNCER- TAINTY U7.0 only	FMC position accuracy is not sufficient for the current phase of flight.	System unusable: advise maintenance personnel. CLR key will not clear message.
PROGRAM PIN ERROR <i>(SA)</i>	FMCS connector wiring incorrect.	Contact maintenance personnel.
PROGRAM PIN MISCOMPARE	Primary FMC has detected a discrep- ancy between its program pin configu- ration adn that of the secondary FMC.	Clear message. Reload QRH T/O Speeds data.
PROGRAM PIN NOT IN DATABASE <i>(SA)</i>	FMC connector wiring does not corre- spond to valid interconects defined in the MODEL/ENGINE database.	FMC not operational. Call maintenance.
QRH DATA INCOM- PATIBLE	Configuration of loaded QRH T/O Speeds data not compatible with con- figuration of FMC QRH calculations.	Reload database. Clear message.
QRH T/O SPEEDS INVALID <i>(A)</i>	Loaded ORH T/O speeds database is unusable.	Clear message and repeat entry of SET IRS POS on POS INIT page.
RE-ENTER IRS POSTION	At least one IRS did not receive position data correctly from FMC or disagreement between SET IRS POS and IRS feedback position.	Clear message. Verify ACARS MU is powered and operational. Re-initiate the downlink.
RESEND MESSAGE <i>(A)</i>	A CDU downlink message is initiated and the FMC is unable to deliver the message to the ACARS MU.	Dial MCP altitude to a lower altitude for descent.
RESET MCP ALT (A)	5 nm prior to top of descent point without dialing down MCP altitude.	Clear message and review existing and desired route segments for possible deletion.
Route full <i>(EE)</i>	Entry of more than 99 wpts attempted or a 6th hold attempted.	Enter an achievable RTA or another performance mode selection.
RTA UNACHIEVABLE <i>(A)</i>	RTA does not fall within the computed RTA window.	Clear message and check selections on DEPartures page. Modify as required.
RUNWAY N/A FOR SID <i>(SA)</i>	The selected runway is not applicable to the selected departure procedure. 757 - SID is removed.	Tune the proper frequency.
RW/APP CRS ERROR (A)	An MCP selected course does not match the FMC flight plan data.	
RW/APP TUNE DISAGREE <i>(A)</i>	A tuned frequency does not match the FMC flight plan data.	Select the proper course.

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TEMPORARY	MESSAGES	arthe Marine Marine 193
MESSAGE	CAUSING CONDITION	CORRECT ACTION
SCANNING DME FAIL <i>(A)</i>	Both DME inputs are failing (displayed only on aircraft with scanning DME and VOR inhbit options selected).	Clear message and report failure to main- tenance.
SELECT ACTIVE WPT / LEG <i>(SA)</i>	After first restart or insertion of a differ- ent flight plan while airborne.	EXECute a direct-to or leg-intercept to tell FMC which leg of route is active.
SELECT MODE AFTER RTA <i>(A)</i>	Exiting RTA into manual speed mode.	Select a normal performance mode such as ECON.
SINGLE FMC OPERATION <i>(A)</i>	In a dual FMC installation, one FMC is inoperative.	Refer to company MEL.
SINGLE IRS NAV	Nav environment is OCEANIC and one IRS is invalid.	None.
STEEP DES AFTER XXXXX <i>(SA)</i>	FMC altitude constraint at waypoint XXXXX results in a steep descent path - >200' discontinuity - to the next waypoint.	Monitor descent. Remove altitude con- straint at XXXXX if allowed. Will prob- ably exceed planned speed to make the path.
SUPP RTE DATABASE FULL <i>(EE)</i>	Attempted save of the 11th supplemen- tal flight plan.	Clear the message, delete unneeded supplemental waypoints and re-attempt entry.
SW OPITIONS INVALID	The validity check of the software op- tions database has failed.	Contact maintenance personnel.
TAI ON ABOVE 10° C <i>(SA)</i>	Aircraft is operating with anti-icing with TAT above 10° C.	Clear message and check use of anti-icing for engine cowl or wing surfaces.
TAKEOFF SPEEDS DELETED <i>(A)</i>	Manually selected takeoff speeds de- leted due to change of departure run- way.	Reselect desired takeoff speeds. Clear message.
THRUST REQUIRED <i>(A)</i>	Airplane is 17 kts below the target speed in cruise.	Increase speed to target speed and clear message.
UNABLE CRZ ALTITUDE <i>(SA)</i>	FMC predicts aircraft cannot reach the new CRZ ALT due to performance limitations or no cruise time possible at entered CRZ ALT.	Clear message and review CRZ ALT se- lection. Enter aircraft altitude or lower. FMC will not recognize descent phase until cruise phase is attained.
UNABLE HOLD AIRSPACE <i>(A)</i>	Displayed when lateral's predicted hold path, (during high altitude maneuver- ing) using the bank angle limit, causes protected airspace to be exceeded.	Reduce speed to return to hold racetrack.

	MESSAGES	Dec 02
MESSAGE	CAUSING CONDITION	CORRECT ACTION
UNABLE MACH .XXX <i>(SA)</i>	In manually selected speed cruise mode, entered Mach not attainable at any alti- tude.	Clear message and select new speed command.
UNABLE NEXT ALTITUDE <i>(A)</i>	Due to an undershoot on climb or an overshoot on descent, the next descent constraint cannot be achieved. U5.0. In VNAV SPD DES, next descent constraint cannot be achieved due to overshoot.	Clear message. If in a climb, review FMCERROR AT prediction (CLB page) and consider selection of a steeper climb. If in a descent, review vertical informa- tion on DES page and consider a steeper descent.
UNABLE REQD NAV PERF-RNP <i>(A)</i>	ANP is greater than the RNP. Message also displayed on the EHSI when in the approach environment. Inhibited if VOR LOC is engaged. Inhibited from dis- playing on the CDU on ground if GPS installed option is not enabled on the	In flight, check status of updating and check the position differences on POS SHIFT page; if FMC position is clearly corrupted, shift FMC to best sensor po- sition source. If displayed inside FAF and IMC, go
	FMC. 10.3 anomaly: If ANP exceeds RNP during approach, landing, or rollout and FCC switches are turned off above 20 kts, message will not clear until a/c is in the air and ANP less	around. 10.3 anomaly: On the ground, can clear messaage from MAP by depowering FMC for 15 sec.
	than RNP. Fixed in 10.4	
UNABLE TO OFFSET <i>(SA)</i>	A valid offset cannot be constructed due to geometric limitations.	Clear the message and amend the route.
USING RESERVE FUEL <i>(SA)</i> (USING RSV FUEL)	U5.0. A change in route causes fuel burn to exceed total fuel minus reserves.	Clear message and amend the active flight plan.
VERIFY GW AND FUEL <i>(A)</i>	Fuel flow data becomes invalid after engine start and fuel value is replaced with dashes. FMC uses last valid fuel	Enter fuel weight on PERF INIT page 1/ 2. Periodic update of fuel weight is re- quired to keep gross weight value cur-
	quantity for performance predictions until manual entry is made. Message appears 30 minutes afer last manual fuel entry	rent. Use ETA and fuel predictions im- mediately after a manual entry has been made since this is the only time they are
	luei entry.	accurate.
VERIFY OFFSET	A change in flight plan is executed that results in a conflict between the new flight plan and a pilot or ACARS en- tered lateral offset start or and wayspoint	Clear message and amend the active flight plan if required.
	tered fateral offset start of end waypoint.	

MESSAGE

VERIFY POSITION (A)

VERIFY POSITION message triggers POS DIFF display on EHSI. POS DIFF display is also triggered if referenced IRS (Single FMC installation) exceeds FMC Sys Pos by 12 nm.

FD, AP may not engage. Cause? Excessive IRS drift, an anomoly in the nav signal, or nav data base dumped and FMC unable to update. In the case of the latter, you can place needed navaids in the Temporary data base (estimate elevation and class). Consider LOP.

VERIFY RNP (A)

VERIFY RNP VALUE (SA)

VERIFY TAKEOFF SPEEDS (A)

VERIFY VERT RNP (A)

VERIFY VERT RNP VALUE (SA)

VNAV DISCONNECT (A)

MESSAGES

CAUSING CONDITION

Position Differences: On the Ground: Airport vs: IRS > 4 nm FMS vs: Rwy Upd > 10 nm In the Air: L IRS vs: R IRS, for 40 sec. > 10 nm IRS vs: FMC Radio for 150 sec. > 4 nm; FMC Sys vs: IRS for 40 sec. > 10 nm FMC Sys vs. FMC Radio for 150 sec > 2 nm U7.1 FMC Sys vs. FMC Radio for 150 sec > 2.8nm-Enroute for 60 sec > 1.7nm-Terminal for 10 sec > 0,5nm-Approach U7.1 FMC Svs vs: GPS, same as FMC Sys vs. FMC Rad. U7.1 FMC Sys vs: FMC Sys, same as FMC Sys vs. FMC Rad.

Default (underlying) RNP be- Clear message. comes less than entered RNP, or a Check pilot-entered RNP and GPS approach has been selected, enter appropriate RNP. the FMC is in the approach envi- GPS Approach requires entry of ronment, and the default RNP is RNP .3. For an NDB Approach active.

enter RNP .6; VOR approach enter RNP .5.

CORRECT ACTION

for accuracy.

In flight:

On the ground: check entered data

U1.3 or less: Check radio data

accuracy using FIX page. Retune

to different station if necessary.

U1.4 up and EFIS: Check the

position differences on POS

SHIFT page; if FMC position is

clearly corrupted, update FMC

to best sensor position source.

Manually entered RNP is larger Clear message. than default RNP, or manually Check entered value of RNP. entered RNP is less than ANP.

GROSS WT or PLAN or ZFW has Check selected small font takeoff changed since the V-speeds were speeds. Pressing REJECT will drop entered. The manually entered V- the V-speeds from the page. speeds will default to small font. Pressing ACCEPT will cause the <REJECT or ACCEPT> prompts V-speeds to return to large font. appear.

While in descdnt, the manually Clear message and check entered entered vertical RNP is larger than value of RNP. default vertical RNP.

Manually entered vertical RNP is Delete manually entered RNP or larger than the default vertical RNP re-enter a different value. or the manually entered vertical RNP isless than the vertical ANP.

The criteria for VNAV engage- Manually control the vertical path. ment are no longer satisfied (FMC disengages VNAV).

MESSAGES

MESSAGE	CAUSING CONDITION	CORRECT ACTION
V SPEED UNAVAIL-	Displayed if any of the independent	Re-enter correct V SPEEDS
ADLE (JA)	VSPEEDs fall outside of the tabular	
	data set boundaries.	
XXXXX ** (SA)	Resetting MCP ALTITUDE to a	Select MCP ALTITUDE value into
(MCP altitude value)	value not equal to the CRZ ALT causes	the appropriate target altitude data line
	the value to appear in scratch pad	or clear message.
	(CRZ page only).	
XXXX * * * <i>(SA)</i>	A REF AIRPORT is entered on POS	Select the airport identifier into the
(Airport identifier)	INIT page and no entry of ORIGIN	ORIGIN data line.
	appears on RTE page 1	
WAYPOINT NOT	An attempt was made to enter a	Clear the message. Correct the entry
DEFINED (AN)	waypoint that does not have a known	error.
	LAT/LON.	
WAYPOINT	An attempt to enter an existing	Clear the message. Then correct the
PREVIOUSLY	identifier using a LAT/LON that is	possible error in desired LAT/LON
DEFINED (AN)	different from the currently stored	data or the delete stored waypoint and
	LAT/LON.	re-enter the desired data, or select
		another name for the desired waynoint.
INOP <i>(SA)</i>	The key just pressed is not enabled.	Clear the message.
NOTE: XXXXX = Altit	ude value or waypoint identifier.	
XXXX = Airpo FLXXX = Flight	rt identifier entered on POS INIT page. ht Level value.	
** MCP altitude	setting appears in s/p for possible line selection	on into a data field when MCP ALT is changed.
* * * Airport identif	tier appears on RTE page for possible line selec	ction into the Origin field. Leading Edge Libraries ©
<i>LL</i> T		

MESSAGES

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In general, most items that can be entered or selected can also be deleted. Listed below by function are the enterable data items which **cannot** be deleted.

ACT WPT

Instead of being deleted, these items must be changed by an overwriting entry from the scratch pad.

LEGS

IDENT

Nav data base effectivity date

POS INIT REF AIRPORT GATE SET IRS HDG SET IRS POS GMT

REF NAV DATA

LAT LONG CLASS FREQ MAG VAR

ELEVATION

SUPP NAV DATA EFF DATE

PERF INIT

GROSS WT ZFW RESERVES COST INDEX CRZ ALT TRANS ALT

TAKEOFF REF OAT

V-SPEEDS

RTE

ORIGIN DEST

CO ROUTE TO WAYPOINTS First ACT VIA RTE HOLD INBD COURSE LEG DIST LEG TIME TURN DIR RTE HOLD when ACTive

CLB CRZ ALT TGT SPEED

CRZ

CRZ ALT TGT SPEED STEP TO

DES TGT SPD

DES FORECASTS TRANS LEVEL CABIN RATE QNH

IRS LEGS ALL ENTRIES

IRS WPT DATA ALL ENTRIES

System default values cannot be deleted. The DEL key is only used to remove crew entries from the system.

The purpose of the Advanced Technique Section is to introduce you to specific features of the FMC as used *on the line* and to discuss procedures not covered in the preceding sections.

Technique

Definitions:

A *technique* is a method of accomplishing a desired aim. No claim is made that these techniques are the best possible. They are simply presented for educational purposes.

A *workaround* is pilot input required due to inadequacies of software/hardware design.

Not every possible combination of displays or key strokes can be shown in a document of this type. Consequently, you must use your own time to build upon the information presented here in learning to apply the flexibility of the FMC to meet your own requirements. Other shortcuts will be recognized through your own experience and ingenuity.

Developing FMC skills takes time and practice. Using the *technique* best suited for a particular approach is challenging.

If any *technique* presented here conflicts with your Standard Operating Procedure, of course your procedure takes precedent.

Fly As Much As You Can

When flying with a pilot that has a high skill-level, feed off of them. You'll learn by watching as well as discussing and your own limits will naturally grow.

Man-Machine Interface Problems

New generation a/c design has created some new problems. The *glass* cockpit has relieved pilot workload in some areas and created workload in others. LNAV is an easy tool to use and well displayed on the Map. VNAV is more complicated, possibly because of fewer pilot interfaces. Mode awareness, where pilots are confused about what the automation is doing, is another concern. Common statements you hear on the flight deck are: "What's it doing now?" "Why did it do that?" "It does that sometimes!" and, "What's it going to do next?" Followed by, 'click' "I've got it."

Credibility of the Glass Cockpit

Automation appears to lose credibility when it unexpectedly fails to do what we expect. There are deficiencies in the design. When you are not satisfied with what the automation is doing, disconnect it.

Backup the Computer

After receiving a clearance, mentally calculate the solution. If the clearance demands an immediate

change in the controls, waiting for the FMC calculation may make the restriction more difficult to achieve, though it's tough to beat the latest processor. One technique is to ask your teammate to operate the computer while you arrive at your own solution.

Don't Sacrifice Heads-Up Vigilance

The crew must not sacrifice heads-up vigilance to operate the computer, especially at lower altitudes. Priorities must be set straight. Accomplish the bulk of approach setups where traffic is light, radio communications are minimal, and restrictions are few. To further emphasize this point, 95% of all programming required for descent and approach should be accomplished at cruise altitude. Do not make the blanket statement that programing should not be attempted below 10,000 ft; an experienced user can certainly accomplish FMC tasks below "ten" if circumstances permit and the steps required are minimul.

Glass Cockpit Complicates Some Procedures

In many instances using the MCP or simply hand flying is more desirable. For example, a runway change in visual conditions can become a more difficult maneuver because the pilot is tempted to draw his attention inside the cockpit. Generally, you will see less experienced glass pilot use the FMC more than an experienced pilot, but it takes years!

Be Efficient

Keep your workload as low as possible. Strive for operating efficiency. Allow the computer to use its default information when conditions permit and enter only information you plan to use. This technique helps to keep all skills sharpened.

Monitoring Pilot Responsibilities

As the MP, be careful when making changes in the FMC without direction or consent from the PF. Much can be learned by watching how your teammate tackles a particular maneuver. And backup your teammate with an occasional check of raw data when navigating with LNAV during an intercept or in the holding pattern. I use the term Monitoring Pilot rather than Non Flying Pilot because it is pro-active!

Keep Your Basic Skills Sharp

Finally, don't forget how you used to fly an airplane. You will still have an occasional use for those "rules of thumb" that have gotten you this far in your career, and you need to practice your scan and concentration that hand-flyng demands. Hand fly the a/c without the FD once in a while to keep basic skills sharp. Learn what to change - the *control instruments* (pitch, bank and power) and how much to change - the *performance instruments* (altimeter, compass, VSI, airspeed)

ILS Approach - EFIS

Prior to descent: Select the approach from the ARRIVALS page, tune the radios, select the inbound course, and brief the approach. When building the terminal routing, try to accept as much default information as possible to cut down computer input. EFIS 3-4-5 - prior to the Approch Check, press MANUAL on the nav head to display raw data on the ADI and to

U5 and up Technique

If no localizer DME, create a wpt .1 nm from RW09 using the Along Track feature. Place this wpt in a FIX page and use for position and altitude awareness. U1.x pilot may create a threshold wpt with the LAT/LON entry on the REF NAV DATA page.



Map and EXECute.)

have now transitioned to the MCP.



If you want to use the VERT DEV indicator, LNAV must be engaged.



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ILS Approach - EFIS (continued)





Consider this technique **only** if your carrier **does not** have procedures in place.

Don't be distracted by what display to select for the HSI. Remember, raw data is **always** on the ADI, your primary instrument; it's got everyting you need except the DME counter.

If the weather is below CAT I with strong crosswind, consider selecting raw data on the HSI to avoid disorientation caused by track up displays (Track up may lead you to believe rwy is straight out the windscreen).

Within 5/8 dot of localizer capture, the ADI localizer scale expands to 1 dot each side. If you exceed the one dot display, you will have to go-around unless you have ILS displayed on the HSI. The example shows EXP ILS. Either EXP or FULL ILS mode will display two dots each side of centerline.

Dec 94

ILS Approach - Non EFIS

Prior to descent, brief the approach, tune the radios, and select the inbound course. Explain to your partner your planned use of the FMC in the terminal area. Set up the RDMI to monitor the OM. Create a wpt at the threshold and place in the FIX page for distance - altitude awareness:U1, use the REF NAV DATA and a rwy lat/lon entry; U5, create a wpt at the threshold using the Along Track wpt feature. The localizer ident or the DESTination ICAO ID in a FIX page may also work but may not be at the threshold. Assume you are flying inbound on the Humble 305° radial(CUGAR ARR). A few miles northwest of MACED, ATC says: *"Nakajima AT-2, fly heading 090°, descend to 3000 ft."*

Dial 090° and press HDG SEL. Transition to MCP SPD, with LVL CHG or V/S, depending on the position of the glideslope pointer. Look for a 3:1 ratio ± wind correction and slowing to flap speed. You've now transitioned to the MCP. Press MANUAL (nav head). Now the ADI has raw data glideslope and DME information, your main instrument for the approach.

With both of you in MANUAL - unless your flying a U5 box - updating is no longer taking place.

U1.x software requires a wpt behind the marker on the runway centerline for the intercept. The example uses GRAFF. Perform an INTC LEG TO MARBE and EXECute. Verify the intercept leg is the same as the localizer course (146° in header of LSK 1L). Continue using MCP HDG SEL until you are established on an intercept heading; then press LNAV. This will update the VERT DEV indication. If LNAV will not engage, you are not on an intercept heading (track). With 1.x software, you can go back to HDG SEL and the VERT DEV will remain useful.

One CDU should display the LEGS page (routing) and the other should be used to display PROGRESS 2/2 for the approximate distance to the localizer course (XTK ERROR) and winds.

This is your ADI and HSI as you await localizer intercept. Pay close attention to the FMA and avoid the practice of looking at the CDUs because that increases "heads down" time. The HSI displays the airplane symbol on a course to intercept the localizer, depicted by the course deviation bar still not off the case. The Waypoint Bearing Pointer indicates the relative direction of the next wpt (MARBE) 30° to your right, verifying that you are on an intercept heading. Use this as a lead-in if there is no beacon at the FAF. The HSI displays the ground speed and string-line distance to MARBE, and your vertical position relative to your restriction at MARBE (1997'). VERT DEV is most accurate when LNAV is engaged.

For localizer and glideslope capture to occur, the pilot flying must have his HSI switch in VOR/ ILS. The VHF nav unit on the same side as the autopilot in use must be tuned to the primary approach facility.

ATC: "Nakajima AT-2, maintain 3000 ft. until intercepting the localizer, cleared for the 14L ILS, contact the tower at MARBE".

Consider this procedure:

When the course deviation bar is alive, you're four miles from intercept. Place your HSI switch to VOR/ILS and press LOC. The course bar will now indicate the proximity of the localizer in degrees instead of miles. APP is not appropriate until the localizer is captured. If altitude constraints have been met, and cleared for the approach, then press APP.

Monitor PROGRESS 2/2 for closure with the localizer.

Note: One pilot should place his HSI switch in VOR/ILS prior to localizer intercept.

Software below U5 will not update from the localizer beam. With U1.x to U4 software, LNAV intercepts usually do not exactly match the localizer centerline. Therefore, intercept the "LNAV localizer" only during a visual approach to a single runway operation.

PROS: Very realistic depiction of approach on HSI.

CONS: Complex and takes practice. Some steps must be accomplished in the right order.

5

2

3

ILS Approach - Non EFIS



NDB Approach - EFIS (GPS overlay)

The EFIS control selector will remain in MAP for the complete approach.

Plan to use V/S for speed control. You should step down each level-off when using the MCP ALT SEL. If your FMC skills are well developed, VNAV can be used for speed control and altitude level-offs. Unless the approach has a VASI or PAPI the nonprecision approach may have, all the way to the threshold, obstacles that reach up to the MDA less the Required Obstacle Clearance. ROCs can vary. In the US, an NDB approach with a FAF is 300 ft; an NDB approach without a FAF is 350 ft.

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4 NM

RW05R

232

150/830

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NDB Approach to 5R at Cleveland - Non EFIS (GPS overlay)

ATC: "Wibault 283, cross Wakem at 10,000 ft." The HSI switch will remain in NAV for the complete approach.

Plan to use V/S for speed control. You should step down each level-off when using the MCP ALT SEL. your FMC skills are well developed, VNAV can be used for speed control and altitude level-offs. Unless the approach has a VASI or PAPI the nonprecision approach may have, all the way to the threshold, obstacles that reach up to the MDA less the Required Obstacle Clearance. ROCs can vary. In the US, an NDB approach with a FAF is 300 ft; an NDB approach without a FAF is 350 ft.



VOR Approach (FMS overlay)



We'll use LNAV for lateral path. Since this is not an RNAV approach, the MP will back-up the FMC in a VOR mode. The MP's raw data is used to verify lateral path, step-downs, and the missed approach point. Select a raw data display prior to intercepting the final course.

Vertical restrictions can be met using the V/S thumbwheel or VNAV.

- The Missed Approach Point (MAP) can be prior to, at, or beyond the rwy threshold.
- The RW + 50 ft will be displayed if the MAP is at the threshold. In the example -VOR 25L/R at LAX, the MAP is *prior* to the rwy; the RW may not be displayed.
- This MAP is labeled MA25B (Both) and *prior* to the rwy. It is on the vertical path the FMC has constructed from the threshold to the FAF. The computed path from the threshold to the FAF will put you at 230 ft. at the MAP.
- This has nothing to do with minimums! In this case you reach the MDA before the MAP. If you level off at the MDA, you'll be high at the MAP so get ready for a miss.

Ensure LEGS page crossing restrictions match the charts. Brief the approach thoroughly.

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Some non-precision approaches may not be contained in the operator's database. Unless specifically prohibited by your SOP, the approach may be constructed using wpts and the rwy contained in your database.

Unless the approach has a VASI or PAPI, the nonprecision approach may have obstacles that reach up to the MDA less the Required Obstacle Clearance. The ROC is generally 250 ft inside the FAF, however ROCs can vary. In the US, a VOR without a FAF is 300 ft.

- If the step-down fix is added by the pilot, the new VNAV path to the threshold may or may not clear this fix. In the example, the predicted altitude at NOELE is 575 ft MSL.
- If the step-down fix is part of the database contained approach, the VNAV path is calculated to clear the fix.
- If weather is such that the lower minimum is needed, ensure that the altitude at this fix is honored.

ACT RTE LEGS

2/3



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DESCENT PLANNING WITH NO PUBLISHED ALTITUDE CONSTRAINT

- Select the approach ILS 03R to Panama City in this example. The approach must be selected first otherwise all created wpts will be dropped when the approach is selected later.
- I discarded the glide slope intercept point optional. (GS-03R) .
- Build a wpt one tenth of a mile this side of the threshold by typing RW03R/-.1 and placing on top of 0 the runway. This is needed for entry to the FIX and DEScent pages because the FMC will not recognize RW03R as a waypoint.
- Place this waypoint (RW001) into a FIX page. Build a waypoint 35 nm from this by typing /35. The FMC will create a waypoint 35 miles from the threshold at a point where it crosses the active flight plan. (reference the dashed circle)
- Downselect this waypoint to the scratchpad and then place it into the LEGS page between MORLI and TBG. Enter 250/10000.

Now decide whether you wish to do a VNAV PATH (idle throttle) descent or a CONSTANT ANGL (partial throttle) descent.

1/3

.760 / FL330

VNAV PATH DESCENT (idle throttle)

MORLI

CONSTANT ANGLE DESCENT (part. throttle)

- · Enter the destination altimeter setting in the DES FORECAST page if it is above standard.
- A few miles prior to the T/D, select DES NOW for a smooth capture of the descent leg.

ACT RTE LEGS

91 NM

Build a deceleration segment; you'll need 1 mile per 10 kts to decelerate. Lets build a waypoint 5 nm to decelerate from 300 to 250. This is done by typing RW002/-5 and placing on top of RW002. Enter 10000 ft at this point.

- When the V/B indicates 2.9, thumbwheel the V/S wheel over to follow the angle of 3° to this waypoint (RW003) (5)
- Upon reaching RW003, wind the speed bug back to 250 kts to meet your speed restriction





Changing a Cruise Waypoint to a Descent Waypoint - U6 and below

Situation:

You are northbound on J55-191 at FL370, 24 nm south of Patuxent for the WARRD 3 ARRIVAL to Newark (no longer current). A restriction at KENTON has been entered on the LEGS page. ATC: "Short Solent, cross 20 southwest of Kenton at FL240".



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PACHUC

112.7 PC

Expect to cross at

MATEO ARRIVAL TO MEXICO CITY

Two things of concern regarding Mexico City ops: (1) FMC position accuracy in the terminal area, (unless you've got GPS) and (2) whether or not to use VNAV. VNAV is not recommended unless you have speed intervention, as the approach controller will probably assign a speed after SMO you cannot hold, such as 160 kts.

During Preflight, align the IRSs to gate coordinates. If you don't have GPS, you may have an inaccurate FMC in the Mexico City terminal area.

At cruise, monitor the POS SHIFT page to determine which IRS is the closest to the Radio position, and therefore, the most accurate. Make sure the FMC POSition is accurate before making this comparison. This may take an extended period of time and re-

DESCENT and DIRECT-TO LUCIA (SLM):

- Accomplish an FMC POSition Along Track check; manual tune to 116.6 and compare the SLM RDMI DME to the RNAV DME. The raw data DME (slant range) should be about a .2 mile greater than the RNAV DME at 50 miles.
- If the FMC POSition is off, a shift to your favorite IRS should be accomplished. Remain in LNAV during a shift in a high workload environment.



- At 9.2 DME, set the heading bug for a localizer intercept and press HDG SEL (25 or 30° bank). Note the winds and position of the ADF needle PLAZA (MW).
- · Select 1200 fpm rate of descent to catch the glideslope.
- Engage the FP's A/P and arm LOC.
- After you catch the glideslope with V/S, arm APP.

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Navigate in the Terminal Area with a Created Waypoint

the heading clearance. This example uses Houston Intercontinental.

It's helpful to use the FMC to start a turn as a Situation: You're arriving from the northwest for reminder in case workload is such that one forgets runway 14L. After passing HOAGI and descending from ten thousand for six, ATC says, "Tupolev 20, depart MACED heading one one zero, descend to 2.000 feet."

Two methonds: PB/D and PB/PB



U3.0. 3.1, and U4.0 users only:

There have been FMC position updating problems during runway changes when the updating is from the manually tuned localizer. Airplanes flying the ILS have been maneuvered to the opposite runway via radar vectors - while the airport ILS direction was switched. This resulted in a reversal of the localizer deviation polarity while the FMC thought the airplane as still on the original ILS. The FMC position was driven off at the rate of 8 nm/min while localizer (LOC) updating was continued. This has resulted in large errors in FMC position at a time when the pilots thought everything was normal. If runways are changed after the FMC has started localizer (LOC) updating, the pilots should ensure that the ILS stations are detuned during the initial vectoring. U5.0 corrects this problem.

CUGAR

Intercepting a VOR Radial on Descent

You're on the CUGAR ARRival to Houston Intercontinental. The restriction at HOAGI is 250/10000 Two possibilities: ATC may turn you direct to the restricted wpt (shortening the flight path) or take you all the way to the radial,(lengthening the flight path).

- ATC: "Latecoere 521, fly heading zero six zero. Intercept the Humble three zero five radial. Cross HOAGI at 10,000 feet and 250 kts."

Dial 060 on the MCP and select HDG. Enter 10000 into the MCP altitude window.
 Immediately check the DME to HOAGI to see if you have time to use the FMC to calculate top-of-descent. (Alt/1000 x 3 plus a deceleration segment = req'd distance)

Set up an INTC LEG TO HOAGI on 305 R. (U1.x software, build HOAGI305/100. Close up the DISCO, then accomplish an INTC LEG TO HOAGI and EXECute.)

Check the initialized inbound course to HOAGI $(125^{\circ}\pm2^{\circ})$. After rolling out on the clearance heading, press LNAV. Use VNAV PATH for idle path (Fig. A) or V/S and 3:1 technique for partial throttle. Your teammate should back you up with his VHF nav for the intercept. When you press LNAV with the later software, the XTK ERR goes to zero.

ATC: "Sikorsky 42, fly heading 060°, vectors for descent, pilot's discretion to to FL 240."

Let's assume clearance for direct to HOAGI could come at any time.

2

3

(A

OR

Dial 060 on the MCP and select HDG. Dial 15000 into the MCP altitude.

The DES page should have HOAGI / 10000 in LSK 3R. Check the V/B in line 4. If it's more than 3.0°, press LVL CHG and determine if you have excess energy (depends on speed and winds). If not, set a V/S of half the groundspeed plus a zero plus 10%. Keeping the V/B around 2.2-2.4° allows a deceleration segment prior to the restriction. See Fig. B

The situation is very dynamic and challenging. Use the MCP V/S, recalculating your
 3:1 position constantly. Altitude to loose divided by 1000 x 3 = required distance without a deceleration segment. (This is a 3.1° descent angle).

The DES page tools at LSK 3R will verify your manual calculations (FIG B). The FPA must be equal to or greater than the V/B to meet the restriction in 3R when flying direct to the fix. If you are not going directly to the restricted wpt, you may keep the actual V/S slightly less than the displayed V/S at 3R.

The FPA, V/B, and V/S are good tools, but remember, they do not calculate a deceleration segment, which may or may not be needed in your situation.

If you really want to make the FMC useful in this situation, while the workload is low, build a wpt on your side of HOAGI equal to the distance you desire for deceleration. (Example: HOAGI / -5). This will display as HOA01. Next, place this wpt in line 3R of the DES page, along with the altitude restriction. HOA01 / 10000. Don't leave this new wpt (HOA01) in the LEGS page. Now, fly the V/B (angle), selecting a V/S that keeps the V/B at 3-3.2° (light winds). Yes, you can simply use the V/S in line 4! Reaching 11,000 ft, roll the speed knob back to 250 and you've got the restriction met. This take practice but you'll love this tool.

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VISUAL APPROACH

Angle-to-Runway technique

This example uses a visual to RW26 at Houston Intercontinental. Elev 100 ft.

STEP 1

Building the threshold wpt.

U1.x LEGS page construction: Fig. A

 Create a wpt near the threshold using the runway coordinates in the database.
 Ref: Building a Runway Waypoint.

U3 and up LEGS page construction: Fig. B

- 1. From the ARRIVALS page, select the approach, if available, or runway and EXEC.
- 2. Two choices now.
 - (a) If you do not need the altitudes at the stepdown fixes, such as with a ground based nav aid approach where raw data is used, delete all altitudes except the runway altitude. Do an intercept-to or direct-to any wpt on the approach. The V/B on the DES page will display the angle to the runway.

(b) If you need the step-down altitudes, build a wpt a tenth of a mile in front of the threshold. This is done using the Along Track feature. (Example: RW26/-.1) It will display as RW201. Downselect it (RW201) to the s/p and place in a FIX page for storeage. When needed, select the DES page and enter your created wpt and desired altitude to LSK 3R. The altitude at this wpt is always 30 ft higher than the altitude displayed at the runway wpt. The entry may be something like RW201/0170. The V/B on the DES page will display the angle to the runway.

STEP 2 Using the V/B (angle) display

- 1. Monitor your angle to the threshold by watching the V/B indication. Your window should be between 2.8 and 3.5°. If you get below your limit, such as 2.8°, press ALT HOLD until you're back in your window.
- 2. Use the V/S thumbwheel to set your desired FPA or V/S.

Downwind Altitude-to-find-Base Turn technique -

BASICS

These are the basic steps in maneuvering for a visual approach from a downwind position.

- 1 Transition *outside the cockpit* as soon as possible. This is much easier said than done. You may have to study the landscape to allow your eyes time to adjust to the light level.
- 2 Monitor the distance to the threshold. This may require creation of a wpt at the runway threshold. (Ref: Building a Runway Waypoint) Enter this threshold wpt in a FIX page. Initiating your descent and turn to base is predicated on a ratio of the altitude vs: distance to the threshold. There are other ways to monitor this distance; if a LOC-DME exists, it can be used. Note that most LOC DMEs are at the *far* end of the runway; this will add a step to your math calculations.
- 3 Enter downwind with Flaps 1 or 2 and 190-210 kts. Flaps 2 pushes the nose over a bit more than Flaps 1 and may aid in visibility.
- 4 When cleared for the visual, set 1000 AFE in the MCP ALT SEL and start idle descent.
- 5 A turn to base can be started at a position where the AFE vs. distance to threshold is 1.5:1, but call for the gear and flaps 10. Example: From a 4000 ft AFE downwind, start your turn to base 6 nm from threshold. Pattern work involves making corrections for

wind. If you've got a wind down the runway, you can start the turn at a 1:1 ratio. If ATC extends you beyond a 1.5:1 ratio, you do not have to be as aggressive (call for the gear on base leg).

- 6 If ATC turns your base at a 2:1 ratio, (4000 ft and 8 nm) configure to F5 and 180 kts as soon as you start your base turn.
- 7 As the airplane stabilizes at Flaps 5 call for the gear, flaps 15, speed to 150, and dial in 750 fpm of vertical speed.
- 8 Turning final, select landing flaps and target airspeed. Hold the same approximate pitch and rate of descent throughout the approach.
- 9 At 1000 AFE, check 3.1 miles from the threshold (3°). Keep the touchdown zone point in the same place in the windscreen. If the point on the runway moves up, you are getting low, and if it moves down, you are getting high. Find a mark on the windscreen to better notice relative movement of the touchdown point.
- 10 Planning is important for a visual approach. Early preparation will make the approach safer, especially at night to an airport with no navaids or approach lights. Check runway information such as lighting and Instrument Approach Procedures (IAP). If an IAP exists, always use it as a backup.



VNAV LEVEL OFF at 10,000'

- NOTE: Prior to accelerating above 0 Minimum Maneuvering or Best Angle, ensure you are heading towards your destination. Vectors in the wrong direction wastes time and fuel.
- Problem: The FMC retards the thrust levers to maintain the 250 kt limit as it approaches 10,000', and then when the altimeter hits 10,000', it changes the target speed to the higher speed for climb and accelerates. FAA certification required that the FMC would not command an acceleration to a speed greater than the speed restriction when the airplane was below the speed restriction altitude.

FIRST WAY - FMC

During preflight:

- 1. Enter 245/9500 into line 3L of CLB page. (Entries will vary with weight)
- 2. During climb-out, select CLB-2 (N1 page). Slows rate of climb.

Passing 9500', the speed bug will reset to 284 kts. (This example). The nose will lower in order to capture this speed. Throttles will not come back until this speed is captured.

CAUTION

Watch speed. Do not exceed 250 kts below 10,000'. There is no overspeed protection using this technique.

PROS: Transition to climb speed is very smooth.

CONS: May have to disconnect throttles and pull them back. No guarantee of meeting speed restriction.

SECOND WAY - MCP

- 1. During climbout, select CLB-2 (N1 page). Slows rate of climb.
- 2. Select LVL CHG climb speed of 245 kts.
- 3. Passing 9500', set the speed bug to recommended speed on CLB page. (284 kts in this case).
- 4. The nose will lower in order to capture this speed. Throttles will not move until this speed is captured.

Watch speed. Do not exceed 250 kts below 10,000'. There is no overspeed protection using this technique.

PROS: Same smooth transition to climb speed with no programing.CONS: No guarantee of meeting speed restriction. May have to disconnect and retard the throttles.

THIRD WAY - HAND FLYING

1. Leave aircraft in VNAV

- 2. As 10,000' is approached, allow the throttles to move rearward a small amount, then simply disconnect them. Turn speed knob to the planned climb speed.
- 3. Level the aircraft following the FD command bars.
- 4. As you approach the climb speed, re-engage the throttles and reset the speed bug.

Level-Off at 10,000'

ATC: "Zeppelin Staaken, climb to and maintain 10,000 ft. Expect further climb clearance in 20 miles".

System will sense altitude ACT ECON CLB 1/1 CRZ ALT FL330 capture sooner at a higher rate of climb (lighter TO FL330 TGT SPD 280/.740 1840.3 z/82 NM weights). Weight entries SPD REST will vary with takeoff 245/9500 CLB-2 N1 weight and some 85.5/ 85.5% experimentation may be necessary. 10,000-Starts to increase to 284 kt -9,500 ²⁴⁵ kt-120 -300 TO 245 140 KNOTS 200180

CIRCLE TO LAND

This procedure requires some CDU input in the approach environment.

Four Arrival for Newark, ATIS is advertising seven advertised, lining up with a tailwind to a runway 6500 thousand scattered, five miles and haze. Temps are 85/65, winds from the east at seven, vectors for a part, such as loosing sight of the runway or poor speed VOR DME Rwy 22L/R, with a circle to runway 29. (This technique will work for any circle-to-land approach).

Now take this ATIS and turn it into real terms.

You're going to be faced with a saturated traffic Example: South of New York City, on the Waard area, a circle in poor visibility - possibly less than feet long from the threshold! A mistake on anyone's control by a pilot, or poor spacing by the controller could lead to a missed approach.

> Don't forget, you cannot continue the approach if you loose sight of the runway or at some point you think it unsafe to continue.

THE APPROACH BRIEFING

Brief runway lighting; RW29 has CL, REIL, and a PAPI on the right side. Shoot the approach in raw data (VOR LOC) or LNAV, but display RW29 on the Map, not RW22. When we're cleared for the approach, switch to the VOR EXPanded mode to confirm you're navigating the 218 degree radial. EXPanded display allows TCAS traffic and wx radar to be monitored. Plan to use the Map mode (NAV for non EFIS) after reaching the MDA for situational awareness.

THE SETUP

TEB

219

219°

CF-22B

OKANO THEN

RX29

2879

RW29

246

From the ARRIVALS page, select RW-29 and a short extension (2-3 nm). Close up the DISCO between RX-29 and RW-29.

With software U3 and up, build an Along Track waypoint one tenth of a mile inside the threshold. (RW-29/-.1) It will display as RW201. Enter RW201/ 0100 in 3R of the DES page (30 ft higher than RW29 TCH). You will use this during your turn to base and final to set up a 3° descent angle.

Enter this wpt (RW201) in a FIX page and draw a circle around it 1.7 nm in radius. This defines the size of the area that offers 300 ft obstacle clearance for Approach Category C aircraft.

1/X

170/3000

170/2500

170 / 1800

---/----

130/70

ACT RTE LEGS

20 NM

3 NM

3 NM

NM

ROUTE DISCONTINUITY

3 NM

If you want to use LNAV for the approach to RW22-L/R, manually enter the wpts that make up the approach since selection from the ARRIVALS page would throw out the RW29 display.

FLYING THE APPROACH

Start the circle between the MDA and OKANO. Tell your teammate to do an intercept to the runway and to set the MA altitude in the MCP.

Transition outside the cockpit, occasionally checking the Map for distance to the runway centerline. Use the angle indicator (V/B) for vertical planning.

Configured and on base leg, look for 4.5° and descending. If the angle indicator shows you below 3°, stay in ALT HOLD until it shows 3°, then select a V/S to maintain 3° descent.

The important lesson is to use the tools at hand in a safe and efficient manner at your own level of expertise. Outside circumstances often dictate how these can be used.

To get the most out of your team-



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ADVANCED TECHNIQUES

FMS Approach - Bridge Visual

The FMS Bridge Visual to 28R at San Francisco is an officially charted visual procedure in the nav database. Some advantages to having FMS approaches loaded in the database are: reduced pilot workload, greater accuracy, reduced controller workload and potential for lower wx minimums than currently req'd for visual approaches. As for accuracy, manual entries are limited to 0.1 min. lat/ lon. Nav database waypoints, provided by the airline to Jeppesen, are accurate to the nearest 0.01 sec. This is a reduction in error tolerance from 600' to 1'. Don't, however, accept clearance for an FMS procedure unless it is defined in your database. Nor should you modify the routing of an FMS procedure unless cleared to do so.

There is no need to display raw data but the FMC must be operating in a radio updating mode. Position radio controls so that updating will take place. The FMC may **P**rocedure tune.

This approach has recently been changed; legs have been lengthened, improving the vertical path.

- This is the display after selecting RNV28R.
- Note that altitude restrictions are included.
- Enter the speeds as displayed below.
- When cleared for the approach, dial the OM elevation (1800') in the MCP ALT SEL.
- If Approach Control needs 180 to the bridge, disconnect the A/T and operate manually.
- Disadvantage: VERT DEV looks at the next wpt rest. only. As you approach ARCHI, VERT DEV does not tell you you're actually **above** the desired path to TRDOW, which makes it more difficult to plan speed reductions; and speed is sacrificed for path.



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• Prior to descent, build wpts along the arc matching the

ATC: "Savoia Marchetti 75, cleared for the ILS to Runway One One via the 14 DME arc."

• Tune a nav aid so you can navigate on the



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- When workload is low, such as prior to descending through 10,000 ft, build a wpt a tenth of a mile from the runway threshold. This is done by downselecting the runway to the s/p and typing /-.1 behind it. (RW26/-.1) Place it on top of the runway. This creates a new Along Track Wpt in the Temporary database (RW201). Downselect it to the s/p, then press the <ERASE prompt - do not leave this new wpt in the LEGS page as it is not needed and can cause confusion. Place the new wpt in a FIX page for storeage until needed. Ref: *Building a Runway Waypoint* in the index.
- 2. While being vectored for the approach, insert the runway wpt that you built and the crossing altitude (30 ft higher than the altitude at the runway) into the DES page at 3R (RW201/0170). The altitude entry requires 4 characters. You've now got the angle calculator set up to display your angle to the runway from any position in the approach. This tool requires practice, but it can be used in many different ways. This is just one.

Another excellent application is on the River Visual to 19 at Washington National. I've been inside Cabin at 4.3°, but configured.



TEMPORARY

V/B On High Overhead Approach

The V/B (Vertical Bearing) indicator on the Descent page is a great tool. But do you know how to use it to its fullest potential?

First, the basics. The V/B indicator is an angle calculator; it shows the elevation angle the airplane is from whatever waypoint is in 3R of the DES page. It can be used in many different situations, but I think you can break it down to 4 basic situations, 3 of which are in the terminal area. The 4 basic situations are:

- (1) descent from cruise altitude,
- (2) approaching the runway from straight-in (includes from dog-leg),
- (3) approaching the runway from base (includes an arc approach), and
- (4) approaching the runway from downwind (includes teardrop/reversal).

This technique is an example of the fourth (4) situation - from downwind.

As many of you know, some Mexican resorts on the Pacific side have significant terrain right up to the coast line.

An approach in this environment can become unstable. What is needed is a tool to help in the vertical dimension.

Consider this approach to RW26 at Zihuatanejo, Mexico.

The set-up: FO's NAV radio is manually tuned to ZIH during descent. At station passage the course selector is turned to 125° for the initial turn outbound.



	ACT RTE LEGS 1/2	1
\square	ALIPO .742/FL325	
	ZIH 210/15000	
\square		
	RX-26/	
\Box	RW26 / 69	
	2.00 / 0.26NM RTE DATA>	
	and a first of a second s	

The Captain's NAV radio is in AUTO for updating and remains there for the complete approach. The LEGS page has ZIH at 210/15000. 210 kts allows selection of flaps 10 and the gear; 15,000 ft is the MEA. A discontinuity exists after the runway with an extension. (RX-26, 263° to RW26/ 69).

Smoke and haze has reduced forward visibility to just a few miles at higher altitude but improves during descent. We cross over the airport at 15,000 ft and 210 kts. We catch sight of the Pacific beach directly below us and request a visual approach. The controller clears us for the VOR-A and the visual.

Gear down, flaps 10, and the descent is begun at 200 kts in LVL CHG.

An *intercept-crs-to* RW26 is accomplished. Press 6R to make 263 BIG. This does 3 things: it displays the final approach course on the MAP/ HSI, and, on the DES page, displays the distance to

RW26 and puts the runway and TCH into line 3R.

Using heading select, we fly outbound on a track of 125°. If you're in an EFIS airplane, this is displayed on the MAP by the FO's NAV radio that is manually tuned. If you're in a non-EFIS airplane, use the orange track indicator. Flying the track will correct for wind.

One CDU is on DES and the other is on the PROGRESS wind/ cross-track error page. As we fly outbound on the 125° track, our cross-track error grows. When it reaches 4 nm, we turn the airplane (HDG SEL) to downwind.

Parallel the inbound course at 4.5 nm. Again, use your track indicator to correct for wind.

250

TEMPORARY

V/B On High Overhead Approach

Of course the elevation angle from the runway to the airplane is initially very steep.

As we continue downwind it decreases until at some point, we can turn base. That angle is 8°. As soon as the V/B shows 8°, we turn directly toward the magenta final approach course (CDI bar in non-EFIS).



You'll be approximately 10 nm from the runway and under 8,000 ft. Continuing to monitor the angle calculator, I find I can actually round out the turn toward the runway in an effort to keep the vertical bearing around 4.5°, after all, we've got lots of drag and we're descending at a FPA of around 5°.

On the EFIS airplane, the MAP displays the runway. On the non-EFIS airplane, the runway is the yellow waypoint bearing pointer on the HSI. The radar is on to display the Sierra Madre del Sur,



right in front of the airplane!

As we join the final course, flaps go to 15, 25, and 30. Target is set and we join a vertical bearing angle of about 3.5° . It is at this point the V/S display (DES page) becomes useful as we're flying



directly to the WPT in 3R.

The throttles come up before 500 ft AGL and we put the airplane down gently in the landing zone.

We release the parking brake at the gate and note the fuel used from FL350 to parking was 200 lbs. What a fuel savings, and a very safe, efficient approach - all by use of the angle calculator.

You can take a great deal of satisfaction in knowing your exact lateral and vertical position throughout the complete approach.

The V/B indicator can also keep you from getting too low! (below 3°) My wish list includes a runway angle display on the EFIS map.

With practice, you'll find yourself flying curved, near-idle descents for visual approaches. But it does take practice - lots of practice.

With no wind, the soonest a turn from downwind to base can be started is 8° (from 210 kts, flaps 1), but it takes aggressive maneuvering (flaps 10, gear down, 200 kt descent). On your first few attempts, try the technique from 7° as you get a feel for the tool. Treat 8° as a limit. Gear down and flaps 5 might work from 6-7° and be more comfortable. Watch the wind. A tailwind on final will require an angle less than 8°.

A normal turn from downwind to base can be accomplished from 5.5° which is very nice to know when doing a night visual with few approach aids, and feeling a little fatigued. A base turn past 5.5° will place you low on the final approach course.

Practice using the V/B indicator on every approach as a way of monitoring your vertical position and you'll soon become an "angle pilot".
CONSTANT ANGLE NON PRECISION APPROACH

to the threshold when the electronic glideslope or charts for obstructions. Just because the FMC calcu-VNAV is unavailable.

This is not only useful for a localizer, VOR, or NDB approach, but also for a visual approach at night to a runway with no VASI (the black hole approach).

The DEScent page can be used to fly a constant angle Caution: You must check your area and approach lates an angle to the threshold does not mean that the path is obstruction free.

NOTES:

- 1. Use V/S, not LVL CHG. At 1,000 ft AFE max V/S is 1,000 fpm.
- 2. At each ALT HOLD, set the next altitude and stay ahead of the airplane. This is one of the most difficult tasks of the NPA.
- 3. At the VDP with approach lights in sight, start down to 100' above TDZE. You may not descend below 100' above the TDZE unless visual reference to the runway is established.
- 4. Disconnect AP at MDA minus 50'.
- 5. For LOC/BC and NDB approaches, use LNAV or HDG SEL to maintain final approach course tracking. The localizer is extremely sensitive due to the close proximity of the transmitter.
- 6. For LOC or VOR approaches, use VOR/LOC, (EXP or FULL). Ground based navaid is preferred and keeps things simple; two differing DME displays such as the slant range DME vs the RNAV DME on the VOR DME approach to 15L to IAH can be confusing, disrupting concentration on step downs.
- Monitoring Pilot can be in Map mode for situational awareness.
- 7. RA technique: Set to 300' AGL. This is the altitude the TERPS guarantees terrain clearance on final approach segment.
- 8. If your LEGS page has RNP / ANP, check the ANP is less than the RNP.
 - A low ANP, such as .3 or less indicates a pretty accurate FMC position.

Calculating a VDP



May 01

CONSTANT ANGLE FROM A LOCALIZER OR VOR APPROACH

7.

PROCEDURE A STEP-DOWN APPROACH

- 1. Arrive at the FAF fully configured and at target speed.
- 2. The MDA should be set in the MCP ALT SEL window. V/S is armed.
- 3. At the FAF, dial 1000 to 1500 fpm descent in the V/S window.
- 4. At 1000 AGL, reduce V/S to 1000 fpm.
- 5. At MDA, (ALT HOLD annunciated) set missed approach altitude.
- 6. If the field is in sight start descent at the VDP, not before or after.
- 7. If the field does not appear before the VDP fly to the missed approach point and accomplish the missed approach procedure.

PROCEDURE B WEATHER ABOVE MINIMUMS CONSTANT ANGLE

 At cruise and before briefing the approach, build a wpt a tenth of a mile from the runway threshold. This is done by downselecting the runway to the s/ p and typing /-.1 behind it. (RW26/-.1) Place it on top of the runway. This creates a new Along Track 8. Wpt in the Temporary database (RW201). Place it in a FIX page for storeage until needed.

Then hit the <ERASE prompt - do not leave this new wpt in the LEGS page as it is not needed there. Ref: *Building a Runway Waypoint*.



- Plan to shoot the VOR or LOC approach with raw data. Use LNAV for an NDB or LOC/BC approach, but monitor raw data - that is controlling.
- While being vectored for the approach, insert the runway wpt that you built and the crossing altitude (30 ft higher than the altitude at the runway) into the DES page at 3R (RW201/0150). This is the only computer work required for an angle display.
- 4. Arrive at the FAF fully configured and at target speed.
- 5. The MDA should be set in the MCP ALT SEL window. V/S is now armed.
- 6. At the FAF, note the V/B indication (it will probably be around 3.0°) and thumbwheel the V/S that is indicated at line 4R. (750 in example) If the V/B is less than 3°, remain in level flight until you reach your desired angle, i.e., 3°



As you descend, your ground speed will change due to wind and a/c configuration; the V/S will also change - it is very dynamic. The required V/S is usually higher at the FAF than at lower altitudes. Use the V/S wheel in conjunction with the FPA and V/S indicators to keep yourself on the 3° angle (V/ B).

The V/B, right next to the V/S display, shows the angle you are to the threshold. Do not let it get less than your own limit - such as 2.8°. If you get low, thumbwheel V/S to zero until the desired angle is achieved.

- At the MDA transition to the view outside the windscreen. You'll be impressed with the smoothness of this technique.
- 9. If the field does not come in sight prior to the MDA, level at the MDA, set the missed approach altitude and continue to the missed approach point. Don't dive for the runway after passing the VDP (steep V/B). And don't rotate through the MDA unless your governing body has approved such a maneuver; the MDA cannot be treated like a DH.

PROCEDURE C WEATHER AT MINIMUMS V/B FOR VDP

Steps 1 through 5 are the same as Procedure B.

- 6. At the FAF, dial 1,000 to 1,500 fpm descent in the V/S window.
- 7. At 1000 AGL, reduce V/S to 1000 fpm.
- 8. At MDA, (ALT HOLD annunciated) set missed approach altitude. V/S is armed.
- When the field comes in sight: Start descent when the V/B indicates 2.8°, not before.

Dial the V/S that is displayed at line 4R.

If field does not appear before the V/B indicates 3.0°:

Fly to the missed approach point and accomplish the missed approach procedure.

LEARNING PROCEDURE

To learn how to shoot these approaches, practice these procedures in visual conditions with a glideslope as backup. You'll learn how to quickly set the FMC up and how the V/B and V/S indications on the DES page operate. This will build confidence in the procedure. Don't wait until you are wading in the alligator pond at night wishing you had these tools.

May 98

Bradford Arrival to O'Hare



Dec 94

Loupe Departure from San Jose, California

This technique demonstrates the planning required to interface the FMC with the MCP in a complex departure. At first examination, this technique will seem too complicated to be practical. But that's not the case. Proper computer set-up reduces le in-flight workload and meets all restrictions. Your clearance is the LOUPE departure from RW30L at San Jose. A combination of clearances will require you to: maintain 5000' until crossing the 047° radial of the SJC VOR; then, at your discretion, you're cleared direct to the VOR, but you must cross it **at** 12,000'; then you're cleared to FL230. Do not exceed 250 kts until past the SJC VOR.





VNAV PATH will honor LEGS page restrictions since it is slaved to the vertical path, but it may exceed the flap speed when high and diving for the path. You may have to use the speed brakes or even the gear to get the airplane down to the desired speed.

VNAV SPD (except for U1.x) will also honor LEGS page restrictions, but only from the low side, i.e. it will level at each wpt restriction. VNAV SPD will not guarantee crossing from the high side since it simply looks at the speed, like LVL CHG.

If you are able to stay in VNAV, you can set the MCP ALT to an altitude such as 3200 ft which lower the workload. VNAV SPD works great on this arrival if you can use it.







Apr 03

NPS, IAN, and the ILS

IAN

Integrated Approach Nav (IAN) is the Boeing term for using ILS look-alike functions for a non-ILS approach. It will also allow LOC for roll and Gradient Path for pitch.

To use the Integrated Approach Nav, the approach must be selected from the database. The nav radios must not be tuned to a localizer frequency. The only exception is that if you tune a localizer frequency and select G/S OFF (ARRIV-ALS or APPROACH REF page) the pitch mode can be G/P using the FMC information from the nav database, i.e., the vertical angle or GP on the LEGS page.

NPS (Nav Performance Scales) look similar to the loc and glideslope scales we're used to and provide an intuitive representation of the LNAV and VNAV path and nav system performance for RNP operations. This option will support operations to RNP 0.1 capability and will provide increased capacity for operations such as for closely spaced parallel approaches.

RNP and ANP bars provide an indication of the airplane system's nav performance relative to the RNP. The ANP bars are the long ones. They will shrink or grow (breath) as the airplane position is being updated. For situations where the Integraged Appraoch Nav display

Apr 03



deviation pointer exceeds the flight technical limit, the pointer will visually overlap the deviation limit bar, the deviation limit bars will turn amber, and the pointer will blink for 10 seconds.

To get the anticipation cues (ghost pointers) you must have both the NPS and IAN options enabled. They reflect LOC-G/S if an ILS is tuned, FAC-GP if no ILS is tuned, or LOC-G/P if a localizer frequency is tuned and G/S is selected OFF.



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demonstration Food Characteries





May 01

Critiqued by Captains EAST SIDE ARRIVAL TO ORANGE COUNTY

Craig Johnston and



May 98

TEMPORARY

ADVANCED TECHNIQUES

ANALYSIS OF A CANADIAN ARRIVAL USING A DTW

ACT RTE LEGS 2/5 219° 49NM BOOTH	 This is the CANUCK FIVE Arrival with the BOOTH transition to Vancouver (CYVR), B.C. Interesting points: The vertical path is predicted on two hard altitudes, VITEV and GS-08L. All the rest are at-or-aboves. There is a speed reduction at BASRA, and a speed at BAJOL that is meant to be at-or-below. The Downwind Termination Waypoint (DTW) is BAJOL.
MOD RTE LEGS 2/5 219° 49NM 300/FL232 218° 5.9NM VITEV 300/FL210B 210° 8.0NM STAVE 300/FL210B 210° 8.0NM STAVE 300/FL189 218° 14NM LANNE 300/13296 236° 10NM MILLS 264/10402 - - ERASE PTE DATA - - MOD RTE LEGS 3/5 - 260° 4.2NM - - - BASRA 230/ 9945 - - - 260° 5.0NM - - - - SEBOG 230/ 8436 - - - - 260° 7.3NM -	 Delete the altitudes at LANNE, BASRA, SEBOG, VARSY, BAJOL, and FAGUE. Delete the 200 kt speed at BAJOL and connect FAGUE to BAJOL. Don't execute. Notice the FMC predicted altitudes. It looks like the airplane will fly the vertical path very nicely, crossing all the waypoints just right, except for BASRA, which will be just a bit high. So with this arrival, I wouldn't change any of the database altitudes. Press the ERASE prompt. There are many ways to shoot this arrival, and this will just give you some ideas. Delete the 200 kt speed at BAJOL and connect FAGUE to BAJOL. With the deployment of flaps you're going to be less than 200 kts. If you are not cleared for the approach by BAJOL, use HDG SEL to fly 260°. Add a 210 kt speed restriction at VARSY, for this is where you will be abeam the runway. When I'm abeam the runway, I want to be at a speed where I can start adding flaps to help the airplane slow-down and come- down at the same time. As you fly past VARSY, control your speed with flaps. BAJOL is 11 nm from the runway, which leaves plenty of room for the turn to base and final, even from 6,000 ft.

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HISTORY OF AN UPDATE

Step 1:

Aircraft manufacturer decides if an update is needed. Computer manufacturer can propose one if problems have developed. Order is then sent to the computer manufacturer.

tep 2:

The software is designed by the computer manufacturer (Smiths Industries or Honeywell).

Step 3:

Software package goes to the aircraft manufacturer where it is added to and subtracted from. Customer (carrier) input takes place here.

Step 4:

Software modification takes place with testing at computer lab.

Step 5:

Aircraft manufacturer certifies the update. Step 6:

Production box is sent to the aircraft manufacturer. Whole process takes at least 6 months. The material presented on the next four pages lists selected improvements in FMC software.

UPDATE CERT. DATE	CHARACTERISTICS
CERT	Model originally used for certification.
U1 Nov '84	Engine data, 20 k (CFM56-3B1) - more accurate. Engine data, 22k (CFM56-3B-2) and related software. Hold - enroute holding capability added. Lateral / vertical design improvements. Messages - modified alert and advisory logic to eliminate nuisance displays. Nav data base - expanded capability. Reasonableness tests between Radio position and IRS position. Reasonableness tests for vertical velocity. Software timing improvements. Waypoint bypass logic modifications.
U1.1	Added more nav data base terminal area procedural capability.
U1.2 Oct '86	Displays the derate climb 1 N1 limits above 4000 ft. U1.1 miscomputes the distance at destination when the destination does not have a runway defined or selected. The problem is more noticeable when the destination is south of the origin. The wrong computed distance for the destination causes the FMC to display a jump (100 ft) in vertical deviation when in path or speed descent. The problem only occures in the air. Fixed in U1.2. Not a problem on U 3.0.
U1.3 Mar '88	 APPROACH REF page has blank display if the selected destination approach does not contain ILS information (replaces the erroneous BCSC display). Autothrottle will re-enter the FMC SPD mode to capture the speed when actual speed falls to more than 15 kts below target speed. It returns to the ARM position when within 5 kts. Auto re-tune search to the best DME-DME pair each 2 minutes instead of keeping the last pair tuned as long as they remain valid. BUFFET ALERT has a pad of 5 kts and 300' is built into the logic that issues the message in order to reduce the instance of nuisance messages. CYCLE IRS OFF message - displayed whenever IRS logic requires manually restarting of alignment. DES page - If DEST does not have a speed restriction, the SPD REST field will be blank. ENTER IRS POSITION message changes, including (a) a position not equal to the value entered in the SET IRS POS field is returned to the FMC from any IRS, and (b) after entry of a SET IRS POS value, FMC detects an IRS in align mode that requires a position entry and condition has lasted for 45 seconds.

SOFTWARE UPDATES - Non EFIS

UPDATE	CHARACTERISTICS
U1.3 (Continued)	 FIX page displays bearing as a Great Circle path so as to be consistent with course information on LEGS page instead of a flat earth bearing. Flight plan predictions improved whenever there are no waypoints in cruise. FMC will not fail for flight plan leg between the North Pole and the South Pole. IBS MOTION message is displayed whenever the IBS has detected motion and has
	restarted alignment (if the IRS has that capability), or needs to be manually realigned (if the IRS does not have the automatic realignment capability).
	PROGRESS page - No more stray M during step trades. Reduced thrust annunciation displayed only if the actual N1 value is reduced. Restart First and second restarts display SELECT ACTIVE WPT / LEG; third displays
	FMC fail. Counter resets to zero at landing and/or after one minute of most recent restart. SELECT DESIRED WPT page - proper display of multi-defined wpts.
	SET IRS POSITION has some changes and additions to the message. SIDs that begin with an "FD" leg type can be processed and flown. STEP CLB function checks max altitude when a step altitude is entered.
	Step-point computed for the step descent and displays it together with the resulting penalty on the CRZ page. Updating is suppressed whenever ground speed is less than 100 kts.
	VERIFY POSITION has some changes and additions to the message. Waypoint - Ability to define a place/bearing/distance Temporary wpt by referencing a multi-defined waypoint name.
	 Wind - FMC can now tolerate very small values of estimated cruise wind. This fixes the previous problem which caused an occasional fail in the FMC when winds were entered into the PERF INIT page during flight. Wind calculation and display is suppressed whenever TAS is less than 100 kts.
U1.4 Feb '91	Agility tuning ability improved through revision of nav receiver selection . Auto tune increased to range of 200 nm, independent of altitude. Increases number of 10 best list.
	Fixed Offset (velocity washout) - If the FMC is misled by an erroneous radio update, its position may drift away from the IRS position. In U1.3 this offset error increases with time during IRS NAV ONLY. In U1.4, the offset grows only until the IRS NAV ONLY message is displayed. After this, the offset is held constant until further radio updating
	FMC transmits engine rating to the autothrottle instead of engine type on IDENT page. High Idle - Engines assumed to operate in high idle on descent.
	IRS NAV ONLY messsage displayed after 2 min. of operation without radio updating after an IRS position shift has occurred. POS SHIFT display and inflight update capability on third page of POS INIT.
	RADIO position now displayed on POS REF 2/3. REF NAV DATA page adds capability to inhibit selected VORs and DMEs. TAKEOFF REF page allows for further selection of derated takeoff thrust on page 2.
	Updating - Single DME updates eliminated. Reduces ability of radio update contamina- tion from misplaced or badly biased DMEs. Updating from a VOR is reduced to a maximum of 25 nm.
	Velocity divergence test is added to determine if automatic re-initialization of FMC nav is required. Prevents nav reference to a badly drifting IRS.
	in the VOR/DME position. Results in less divergence in FMC position. Wind anomaly in using forecast winds during cruise. To be fixed in next update.

SOFTWARE UPDATES - Non EFIS

Dec 95

All U1.x software is found on non-EFIS aircraft.

UPDATE	CHARACTERISTICS	
U1.5 May '92	Wind anomaly in U1.4 fixed. Problem:	09 w
itte nävelä spanäv - Otar 6 täla dora di Bran di ²⁰ 7, and	 Occasional FMC re-starts have been experienced. The lock-up can occur or in flight. The problem is more likely to occur when: 1) both nav radios are in the MANUAL tune mode. The computer's sear through its nav data base increases. In a densely populated nav are may take too much time, for it searches up to 390 nm. 2) the operator is using the <i>universal data base format</i>. A change was nav data base packing program. The changes, made in the January for certain operators, have also resulted in additional time required for search. 	at the gate irch time a the search made to this data base for the navaid
	3) the operator is using a large nav data base which also extends the s	search time.
ente 2	Until a permanent solution is implemented, have at least one nav radio mode (on the ground and airborne) whenever normal operating proced	in an auto ures allow.
	None EFIS aircraft place the HSI switch to NAV. EFIS aircraft, use the MAP or PLAN position.	, °
U1.6 Mar '95 FMC must be sent back to the factory for re- programming or the carrier can obtain a re- program from	 APPROACH REF page will display FREQuency to 2 decimal points. Fix: In previous software, when one radio is tuned manually, the FMC would latitude bands of its memory in its attempt to build the best 10 navaid list t angles" with that manually tuned navaid. In an area of high density navaid the northeastern United States, this search would "time out" and the FMC "restart". (The search is also heading sensitive.) The OFP's internal navailogic will now search 3 latitude bands to shorten the search time, and charpriority of the search; that is, it does not have to be done in one calculation finished at a later time. REF NAV DATA - NAVAID IDENT page will display FREQuency to 2 decimal 	search 5 o "match s such as would d search nge the n but can be I points.
Smiths.	NUPPER PC., process to ensurement to apply while or new memory of the CPT STORE and products on the process of the CPT STORE and playment products.	
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UPDATE	CHARACTERISTICS
U2.0	Added EFIS output and backup nav with ANCDU.
U3.0 Jul '80	 ALERT and ADVISORY messages have been modified to eliminate nuisance displays. Along Track Offset - capability of creating a waypoint either side of a fix that is in the flight plan by entering the fix, a slash, then a plus or a minus sign and the desired distance into the scratch pad. APPROACH REF page - rwy length in feet or meters. ANCDU compatibility.
sentatabler 1. mm. Witten	Aspirated TAT probe (option). Autothrottle will re-enter the FMC SPD mode to capture the speed when the actual speed falls to more than 15 kts. below target speed. Returns to ARM when within 5 kts.
אתה יישוארים, לייה נערך ייגוב, נאגנס ענו לנג 11 יי אנוקוול-	Clock input with date. DES FORECAST page - Descent forecast winds and ISA DEV may be entered. Distance-to-go in one-tenth nm.
and that its edit	EFIS - Ability to interact with the optional Electronic Flight Instrument System (EFIS), and Alternate Navigation Control / Display Unit (ANCDU). GATE position.
uius ee te did welliksei dala	HOLD page - capability has been increased to allow for 5 holds in the flight plan. Inhibit VOR capability. Intercept course crew enterable. LEGS page - ACTIVATE prompt added.
t foress in	Localizer updating capability. POS INIT - GATE position may be entered for position initialization. REF NAV DATA - rwy coordinates retrieved by entering RW prefix or airport ident first. RTE page - flight number entry. Propagates to the PROGRESS title.
Although an ann an Although an	RTE page - optional hight humber entry. RTE page - runway entry does not require RW prefix. Runway assigned threshold crossing height instead of threshold elevation. Runway or intersection position update on runway.
ten _e n en bio lei tri, ¹⁻ d noit shirof (tari	Scanning DME compatibility. Software restart - Upon occurance of second restart (within 1 min of first software restart), performance data, including ZFW, reserves, flaps, des forecast data, approach speeds, and perf. limit is reset to zero. * SUPP nav database is provided to allow entry of nav information for longer than one flight. TAKEOFF REF page - TAKEOFF SPDS calculation (option) USING RESERVE FUEL message. VERT DEV - HI/LO
U3.1 Dec '87	Auto tuning of best DME-DME pair limited to 2 minutes. Direct to Hold fix allowed. Inhibit DME capability. INTC CRS displays previously entered course to selected wpt. Software restart - same as U3.0
U4.0 Oct '88	Data for CFM56-3C1 (23.5k) engine and aero data for B737-400. POS SHIFT displays sensor position differences and performs inflight position update. RTA PROGRESS - Required Time of Arrival (RTA) fuction and PERF LIMITS page added. Software restart - same as U3.0, but in addition results in 210 kt commanded target spd. STEP CLIMB function checks max altitude when a step altitude is entered. TAKEOFF REF 2/2 - fixed takeoff derates added. VOR - Reduced gain on VOR input, resulting in less divergence in FMC position. WIND - If the cruise wind is entered on the PERF INIT page, the climb wind is erroneously assumed to be the same as the cruise wind, from takeoff through level off.

UPDATE	CHARACTERISTICS
U5.0	ACARS - Provision for receipt and display of status messages from ACARS.
May '90	Automatic reset - If an erroneous radio update causes the FMC Position to move away
	from the IRS position at a rate of more than 8 nm/hr, the FMC position will be
- Internet and sold	automatically reset to the IRS position. The FMC will then follow the IRS position until
) ménin meresi	radio updating is again available.
2 400 transfer 1948	Auto-tune increased to 200 nm (more stations available). Independent of alt. and class.
	CDU lockup while entering route data during short alignment is fixed.
Incon- the line	C.G Max altitude computation is based on C.G. entry on PERF INIT page.
i a same m	Data (aerodynamic) for -500 airtrame and CFM-56-3B1 engine, rerated to 18500 lbs.
	Disc loader - Ability to load nav database via high speed 3.5" disk loader.
1	DME - Elimination of single DME updates. Reduces the possibility of radio update
	ENG OUT computation of max alt based on blood status by choosing it or it engine out
	Eived Offect (velocity weshout) - When the IBS NAV ONLY message is displayed EMC
	flys a constant offset from the reference IBS
- Interior - Interiora - Interior - Interior - Interior - Interior - Interior	Flan speeds - VNAV target flan extension speeds revised. Previous updates did not
age APAInen	account for increased gross weights. Bef p. 68.
	Global Position System (GPS) provision added including POS SHIFT capability.
	Heading Reference - If the Heading Ref switch is in the True position, the suffix "T" will be
B JOHUL \$6 MILL 1	added to the bearing displayed in the bearing/distance field on the REF NAV DATA
	page.
	High idle - path predictions based on engines running at high idle during descent.
BURK Jam OLAN	TAI entry on DES FORECAST page still disabled.
1	ILS - ILS approaches with glide path intercept points prior to the FAF wpt can now be
2 th binduates e	accomodated in the data base.
jon west gen	Intercept function - upon entry of a new active waypoint at 1L on LEGS page, prompt
The second second	appears in 6H for intercept course entry.
2 Large and star	IRS NAV ONLY message logic revised. (If radio updating does not resume within 2
1 100000	Influtes of a reference in 5 switch of an Five hav program reset
ga in	lumps - ETA and flight plan distance jumps during SPD DES problem fixed
	LOC DME checked for reasonable activity and rate of change before used for up-dating
 Alas e photester a pro- 	MAX altitude - Displayed on line 1 of CBZ page after OPT. When the cruise mode is
1	ECON or LRC, the max altitude is the highest possible altitude within the maneuver
	margin. This value is independent of the displayed ECON or LRC target speed.
 UT14 mat 	However, in U5.0, when the pilot enters a manual cruise speed, the maximum altitude
	displayed is the highest altitude where that entered speed can be flown within the
0	maneuver margin.
	MAX / MIN - In manually selected CRZ speed mode, a cruise altitude or speed entry will
	result in a limit on selected speed.
	Navaid pair selection to include range to visual horizon in addition to crossing angle.
	POS SHIFT - reduced roll rate when using the position shift.
	PROGRESS page displays fuel at last waypoint.
	Runway Extension replaces FA-XX waypoint.
5	Runway Opuale has option of runway remaining entry.
))	Slash Rule - In previous FMCs, the slash was always entered with the first number. In
Ť.	U5.0, the slash is entered with the number that is closest to the center of the CDU
	Change will affect left entries only. (Note FIX page use)
	Software restart - fixed second restart problem.
1	SPD DES initiated same as PATH DES; i.e. automatically or CAPTURE.

UPDATE	CHARACTERISTICS
U5.0	Step-climb - Wind values are filtered. Primarily based on values found on the PERF INIT
(Continued)	the step altitude.
ARI ILIA	T/D ADVISORY discontinued.
entra transference	mode changes automatically to VNAV SPD. The aircraft automatically descends if the MCP altitude is set to a lower altitude. Also, if no E/D is entered, a/c starts down if the
7.0	MCP is set to a lower altitude, reverting to VNAV SPD. TAKEOFF REF page includes optional entry of rny remaining for use in position update.
.ch .280	Time and Date provision from GMT clock.
o/ steps) of	is displayed if entered Mach is unattainable at any altitude.
luo sharts to i	Velocity divergence - prevents navigation reference to a badly drifting IRS.
Aukyrse, FMC	VERIFY POS message (causes) changes. Ref Messages.
Los Marcall	VNAV disengages at sequencing of a GS waypoint. VNAV PATH defaults to VNAV SPD if a roll mode other than LNAV was selected.
	VNAV SPD - guidance honors intermediate altitude and speed restrictions on LEGS page from the low side
yanış tatist " "afita -	Waypoints - altitude constraints (more) on cruise waypoints are improved.
ATMO ANNE	Winds - Problem in U4.0 of erroneous use of winds fixed. Now starts with zero at surface.
.transited	Problem:
ol ash nus	flight. The problem is more likely to occur when:
របានចំណុះខ្មែរ	 both nav radios are in the MANUAL tune mode. The computer's search time through its nav data base increases. In a densely populated nav area the search may take too much time, for it searches up to 390 nm.
formt in edi	 the operator is using the <i>universal data base format</i>. A change was made to this nav data base packing program. The changes, made in the January data base for certain operators, have also resulted in additional time required for the navaid search.
ni A fer unschieru	3) the operator is using a large data base which also extends the search time.
isu muşlariş Az — oregunar	Until a permanent solution is implemented, have at least one nav radio in an auto mode (on the ground and airborne) whenever normal operating procedures allow.
ari y pand pairmir a linais pairmir das	None EFIS aircraft place the HSI switch to NAV. Nav controller switches to AUTO. EFIS aircraft, must press nav head to AUTO.
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nor Lana misili	ingen stand in a rightweistering sons aparent in and, and mar so
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	strandska marka sa

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U6.0 Dec '90 ACARS interface. Parallel to U5.	ABEAM WPTS - Entered wpt cruise winds may be transferred to the new lateral flight path using the ABEAM prompt. Upon execution of the DIR TO modification, this
Dec '90 ACARS interface. Parallel to U5.	path using the ABEAM prompt. Upon execution of the DIR TO modification, this
ACARS interface. Parallel to U5.	
interface. Parallel to U5.	tunction creates wors on the new lateral fillight path abeam the wort on the old fillight
Parallel to U5.	nath. Entered winds assigned to the old write will be carried over to the new abeam
	white if the new points are within 100 pm of the old wat
	White the new points are within 100 time of white one white the new points are within 100 time of white the new points are written and the new points are w
	ACARS - an added ACARS interface allows uplink (ingrit plan data, performance data,
33.5 p	develors speeds, wind data, ATC hight plan thoundations, user defined upinities and
- 1000 - 1000	downlink (position reports, night plan data, actual winds, prediction data, user defined
and the second s	downlinks) for FING functions.
in all the second second	ALTERNATE DESTS page computes and displays distance, ETA and fuel for up to 5
file of billions	selected alternates. Based on PPOS to the alternate or continuing to current
	destination and then direct to the alternate.
1200-01 12-00 PM	Altitude Intervention feature incorporated with MCP. Provides for manual setting of cruise
	altitude target on MCP with VNAV engaged and for selective deletion of altitude
	constraints in climb or descent. (option)
10-10 M H H H	Computations based on direct route from current position to alternate, or continuing to
ALL OBSY BULLE	current destination and then direct to the alternate.
1	Data base extended to 1 million words. Can accomodate world wide coverage for a
All http://ik	particular airline.
to adult new	EFIS displays of MSA, MORA grid with altitudes.
	Flight Number - Provides for entry of 8 digit display and transmission of flight number.
(1)) (1) (1) (1) (1) (1) (1) (1) (1) (1)	IDENT page 2 displays list of loadable default data (via data base loader - i.e. drag, and
	fuel flow factors min/max speeds maneuver margin etc). In previous undates, the
	default data was entered by maintenance using BIT
	INIT / REF INDEX page adds prompts for MSG RECALL and ALTN DEST
matrik, atomen	Marsage Recall - Ability to recall scratch and messages after being manually cleared
	whose set logic is still valid
10715-0081-601-6	Miceo departo other automatic quidance provided by EMC (vertical and lateral) upon
VSDTLes	activation of microad approach
· · · · · · · · · · · · · · · · · · ·	All LIMIT page adde Thrust Deduction Altitude (T/D ALT) feature
economical Automation	NT LIVIT page alus Thusi neudolion Allice (Th ALT) reduce.
a fraction of the	have and dianautha five airporte alegast to the airport (alegast first)
	Dase and display the live airpoins closest to the aircraft (closest list).
La francisca da la composición de la	PLAN FOEL (PERF INIT) - FMC switches to actual fuel at engine start (pack on & haps
National Indiana Contractor	aepioyea).
diaran ang a	POS INIT page displays MON/DY. Works in conjunction with date sensitive nav data.
	Procedure turns - defined from nav data base with automatic guidance from FMC for
	vertical and lateral steering.
NUL WELL MADE	QRH TAKEOFF REF - V1, VR, and V2 displays on TAKEOFF REF page accounts for
	runway length, slope, condition, temperature, takeoff N1, flaps, gross weight, winds,
the beyelden value	and C.G. (option)
Endi Ryumadi, gr	Sensor positions (IRSs, GPSs, Radio) displayed on EFIS when POS SHIFT page
	displayed and EFIS is in PLAN mode.
n magnaphil (POPE	SUMMARYprompt on REF NAV DATA or SUPP NAV DATA pages will display all data in
Turns 2042 é p	Temporary and Supplemental data base and how they were constructed.
sana 44	Scanning DME installed (opt) blanks the nav radio window. (108.0 is not visible.)
	Speed Intervention feature incorporated with MCP. Provides for manual setting of speed
1, silore	target on MCP with VNAV engaged. (option)
	TAKEOFF REF page displays engine rating selected rather than RED TO N1.
U6.1	Minor changes including maneuver margins.
116.2	Fixed fuel quantity problem

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UPDATE	CHARACTERISTICS
U7.0	4 MCU chasis is smaller and lighter than the old 8 MCU chasis (17lbs vs 25lbs). Also uses
Mar '93	less power (25 watts vs 100 watts).
	Altitude constraints may be entered on any cruise wpt, not just a climb or descent wpt.
	CHECK FMC FUEL QUANTITY appears if the FMC has detected a decrease in fuel gty.
	greater than 1500 lbs, and 120 sec. has elapsed since the decrease was detected.
	EFIS MAP displays the FMC, IRS, GPS (if available) and RADIO sensor positions by
	selecting the POS SHIFT page while in the PLAN mode.
	FLIGHT NO, will take up to 8 alpha-numeric digits.
	FMC - includes option to prohibit manual entry of performance default data via CDU.
	GPS - monitoring and an advisory option provides a one-shot update to GPS position.
	IDENIT 2/2 displays identification number of the performance defaults data base.
	IBS NAV ONLY will display when POS ACCLIBACY is not sufficient for phase of flight
	Message is inhibited during the approach phase of flight under certain conditions
	IPS NAV ONLY logic revised to include when POS ACCURACY is not sufficient for curant
	phase of flight
	Manauvar margin Jawar limit has abangad from 1 15 to 1 20
	New Date Dase has option to include a 1 merceword new date hase. Normal is CEC k
	NAV OBTIONS prompt is evoluble from the DEE NAV DATA or NAV STATUS poors The
	NAV OFTIONS prompt is available iron the HEF NAV DATA of NAV STATUS page. The
	NAV OP HONS page allows inhibiting of specific navalus for updating.
	NAV STATUS prompt on POS SHIFT, INT/REF (In flight), PROGRESS 1/3, and NAV
	OPTIONS pages allows selection of NAV STATUS page, which displays status of
	navaids being tuned by the FMC and reference IRS data.
	OFFSET prompt is displayed on RTE and INDEX pages. This feature, allowing
	construction of a lateral OFFSET, is inactive until U7.1.
	Operational Flight Program (OPF) - on board load of OFP.
	OP Program 549297-001 (U7.0) displayed on IDENT page.
	OP PROGRAM INVALID message means a fault is detected i program memory. Action:
	Pull FMC C/B for 20 sec. and reset. If still invalid reload OPF.
	Performance Default data - option to prohibit manual entry of default data via the CDU.
	POS SHIFT page displays additional sensor information and position accuracy.
	PRE-FLIGHT status prompt deleted with TAKEOFF SPEEDS option.
	PROGRESS 1/3 includes wind display and NAV STATUS prompt. VHF nav displays
	moved to NAV STATUS page.
	RC-XXX - runway centerline intercept wpt added.
	REF NAV DATA - VOR and DME inhibits removed. SUMMARY prompt allows selection of
	TEMP NAV SUMMARY page and SUPP NAV SUMMARY page. NAV OPTIONS
	prompt allows selection of NAV OPTIONS page.
	Response time is faster from a high speed 32-bit processor.
	SUMMARY prompt on REF NAV DATA and SUPP NAV DATA pages displays TEMP and
	SUPP NAV SUMMARY pages.
	TAKEOFF REF 1/2 - (without VSPDS option) VERIFY TAKEOFF SPEEDS displayed with
	ACCEPT/REJECT prompts if the gross wight is changed after takeoff speeds are
	manually entered.
	TAKEOFE BEE 1/2 - with VSPDS ontion: Computed takeoff speeds (VSPDS) displayed in
	center of name and may be selected to right side of name. Select these VSPDS on/off
	by toggling 6B. Pro-flight status prompts delated Massage VERIEV TAKEOFE
	SEEDS come as above
	OFEEDO Sallie as above.
	TEMP NAV OLIMMAPY display changed to include thrust rating with the NT rating.
	LEWE NAV SUMMARY - displays contents of Temporary nav database.
	SUPP INAV SUIVINIARY - displays contents of Supplementary nav database.
	VERIFY POSITION message is inhibited during approach phase of flight.

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U7.1	CHARACTERISTICS				
1202 SAN	APPROACH REF page - VNAV target speed includes WIND CORRection.				
Jan '94	APPROACH VREF NOT SELECTED displayed when in VNAV and FMC is in approach				
our or	environment and VBEE has not been selected.				
Dual FMC	FIX page title changes to OFESET FIX INFO during route offset operation.				
canability	EMC dual installation: Permits operation with EMC as the primary means of navigation.				
Dorollolo LI5	Basic operation with dual EMC is identical to single EMC operation. An EMC Source				
Parallels 05	Salect switch is installed on the aft overhead nanel with the standard instrument				
	switches. It parmits the selection of Normal (system coordinates EMCs and nav				
Street Silver and	instrumente) right or left EMC for all new purposes				
	Credient Deth (vertical angles) from the new data base allows I NAV/A/NAV to the runway				
en U	threaded a reasing bailet. Appundiated on LEGS page				
37 P000	Intestion crossing neight. Annunciated on LEGS page.				
- Alexandra - Alex	GPS position update option.				
Sector Contraction Contraction	IRS NAV ONLY will display when ANP is greater than RNP. Message is inhibited during				
and the second	the approach phase of flight under certain conditions.				
contract managed	Missed Approach can be manually constructed and flown in LINAV and VINAV. Speed and				
	cruise altitude is assigned to CLB and CHZ pages at time of missed approach.				
APRIL 1981	OFP nav data and performance data defaults can be crossloaded onboard.				
	Route offset, accessed from RTE or INIT/REF INDEX page.				
	RNP / ACTUAL position displayed on LEGS and POS SHIFT pages.				
	STEEP DES AFTER XXXXX displayed immediately when an altitude constraint at XXXX				
	results in a steep path to the next wpt.				
	VNAV maintains PATH DES until XTK ERROR is greater than RNP, at which time it				
	reverts to SPD DES.				
	VNAV path guidance to the TCH or MAP on non-precision approach.				
	VNAV available for any flap setting.				
U8.0	U8.0 contains all of U7.0, U7.1, and the following capabilities from U6:				
Dec '93	Abeam waypoints selectable after DIR TO.				
200 00	ACABS interface.				
Dual FMC	Altitude intervention (via MCP).				
capability	Alternate Destinations / Nearest Airports in data base.				
Parallels I I6	Messare Becall				
ACARS	Missed approach procedures loaded in database.				
interface	OEP loadable via the Data Loader Linit				
intenace.	Procedure Hold and Procedure turns in data base				
	OBH Takeoff Speeds on TAKEOEE BEE page				
	Speed intervention (via MCP)				
U7.2	FANS1 MCDU compatibility (VNAV key)				
U7.2 Jan '95	FANS1 MCDU compatibility (VNAV key) GPS is certified as a sensor for FMC position updating.				
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May 98

UPDATE	CHARACTERISTICS					
U7.3 Winter 95 Dual FMC capable	 This upgrade is required for FMC operation with GPS and with manual RNP capabilities. Delection of PROC HOLD/TURN is easier. Also allows deletion of the (INTC) point. Dual restart process will include one additional attempt, after a period of 5 minutes, when the FMCS Source Select switch is in BOTH-L or BOTH-R. GPS clock serves as the internal FMCS clock source when "GPS with Integrity" software is installed. Holding: When in the descent mode, and when an approach speed has been entered on the Approach Ref page, the displayed active speed on the Hold page will be changed 					
Ver 1 i Ver 1 i V u mon u V	 to match the target speed for flaps deployed at angles greater than 15°. Holding: Ability to hold on the same wpt twice, once before the approach and again in the missed approach procedure. Message UNABLE REQD NAV PERF-RNP cannot be cleared from EFIS Map. Message VERIFY RNP has revised logic where no manual or nav database RNP has been selected. This will back up the procedure to enter the RNP prior to commencing 					
New Gared and opmost of of energy a 1000%	 Message VERIFY RNP VALUE has revised logic to provide immediate feedback for the case where the manual RNP entry is smaller than the current ANP. NDB Approaches may be included in the database and may be selected from the ARRIVAL page. RNP - new default constraints. TAI ON ABOVE 10° C message logic is revised (minor). 					
U8.3 Winter 95	Same features as U7.3. Dual FMC capablility. Parallels U7 but offers ACARS interface.					
U7.4 U8.4 1996	 Data is recorded anytime a single FMC fails in a dual configuration. Fixed dual down-mode to single FMC operation. Holding - Two holds on the same waypoint (one in the missed app, and one in the regular route. Holding pattern can be placed on the same wpt that has a procedure turn from an approach transition. If you try this in 7.2 or earlier, the FMC may fail. Procedure Turn can be deleted by deleting the INTC wpt. NDB approaches in the nav database. RNP default values changed. Support for new higher memory hardware. TAI on above 10°C message revised. Maintenance features allow download bite data. 					
U7.5 / 8.5 1997	 ARRIVALS page display problem fixed regarding runway display. Ref: 15.2. Downmode and software restart problems fixed. El Paso "problem" fixed. Ref: 12.8. ENG OUT page cannot be EXECuted. Though title displays MOD, it is advisory only. FAF defaults to 150 kt speed restriction on database contained non-precision approaches. NAV DATA OUT OF DATE nuisance message fixed. NAV DATA OUT OF DATE year 2000 message eliminated. Maintenance: Additional recording parameters added to download file. RNP: Manual entry of RNP is now the default option. Runway wpt is no longer a "force overfly" wpt. SELECT DESIRED WPT page adds "intelligent sorting", second page if required, second decimal point to NAVAID FREQ, and clears scratchpad when leaving page. VNAV operation with failed fuel input. 					

May	98
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UPDATE	CHARACTERISTICS				
U10 Cortified	U10 is a derivitive of U6 and 8 with the following added features.				
Oct. 1997	737-600/700/800 thrust rating model. ADIRU automatically adjusts IRU alignment time as a function of latitude (5 to 17 min).				
sangana dig	Minimizes ground time for alignment. ADIRU is automatically updated (aligned) prior to takeoff. Reduces accumulated drift				
	during extended ground operation (sitting at the gate in NAV). ANP improvements. BITE maintenance and interface changes for CDS APLL FEC FOIS MMB				
	CDU is a LCD. Increases reliability and less weight. Climb speed restriction down to 100 kt from 210 kt. VNAV Minimum Limit Speed = Vref +				
	increment. Common Display System interface replaces EFIS display for 737-600/700/800 (9" x 9").				
	Deceleration Point (DECEL) to the next speed restriction displayed on ND. DES page. DES NOW prompt replaces CAPTURE prompt.				
	Discontinuity auto-sequencing. DME arc. (AF leg) Center required to be a DME. Double by pass no longer inserts a discontinuity. Possible path overshoot for adverse				
	wind conditions. Downmode and software restart problems fixed.				
	EFIS POS switch displays green VOR and/or cyan ADF bearing vectors. EFIS/ND has additional map ranges of 5 nm and 640 nm.				
	ENG OUT page cannot be EXECuted. Though title displays MOD, it is advisory only. Fixed-radius (constant radius) turns between airway or procedure legs when airway or				
en option corte.	Fixed Radius Enroute Turns. (Eurocontrol routes) Turns less than 135° for non-flyover wots. Turn radius of 22 nm or 15 nm.				
	FMC (left) and CDU (left) will operate on standby power (option) GPS with integrity				
	GPS updating adds a symbol to the tip of the aircraft triangle on the ND Map. High-speed Aero loadable.				
	IDENT page two displays more configuration selections such as QRH T/O SPEEDS and MODEL/ENGINE DATA.				
	INIT / REF INDEX displays SEL CONFIG at LSK 5R while on the ground. ISDU adds a GPS annunciator				
	LNAV bank limit increased from 8° to 15° between 200 ft and 400 ft. LNAV will arm on the ground. Roll command is wings level until 50 ft. (-600/-700/-800)				
	Magnetic Variation table coverage extends from 82° N to 82° S except for keyhole areas which coincide with the Magnetic Poles and is common to FMC and ADIRU.				
	MENU page allows selection of system for which the MCDU will be active, such as FMC, ACARS, or DFDAU. MCP flyaway logic - allows pilot to dial MCP altitude to missed approach altitude (above				
	aeroplane) when established in a descent on approach. (-600/-700/-800) Model engine database in the OFP.				
	Multiple approaches of the same type to the same runway. (More than one ILS) Operational Program Configuration (OPC) options via software programming instead of				
	Program Pins. Performance database for -600/700/800 is loadable.				
	Radius to Fix. (RF leg) Any fixed geographic point can define the turn center. RNP values supplied in the nav database for each leg.				

UPDATE	CHARACTERISTICS
U10 (continued)	 RTA allows entry of "At or Before" or "At or After" as well as "At" times. SELECT DESIRED WPT page increased to two pages with "intelligent sorting" and navaid type displayed in header. Sensor positions sent to ND via POS switch on EFIS Control Panel. Software (FMC) may be loaded via floppy discs. Tabular database is loadable including calculation of takeoff speeds. Replaces predefined tables. TAKEOFF REF flap entries are defined in the database. U10 features (OPC) may be selected by the airline. Active options are listed in the MAINT section of the FMC, on the ANALOG DISC pages. VNAV ops may continue with FQIS inop. Message CHECK FMC FUEL QUANTITY will remind pilot to enter fuel quantity. Pilot must keep fuel weight in FMC current. VNAV capability added for engine out in descent phase of flight only. VNAV descent below MCP altitude (requires A/P change) WGS-84 Earth Model.
U10.1 Spring 1998	N1 LIMITS page allows selection of all takeoff ratings. N1 LIMITS page redesigned to accomodate Thrust Bump feature. Revised takeoff thrust limit. Takeoff Flaps box prompts added to TAKEOFF REF page. Thrust bump allows for selection of one engine rating higher than the FULL rating. Thrust Reduction Altitude moved from N1 LIMITS page to TAKEOFF REF page. WET GRV (gravel) runway condition added to TAKEOFF REF page.
U10.2 Aug 1998	Approaches: LDA, SDF, and IGS approaches added. Color when used in conjunction with LCD CDU and appropriate software option code. High altitude maneuver control will provide a bank angle limit, which is calculated as a function of gross weight, altitude, speed, temperature and selected thrust. HOLD page: TURN DIR moved from 2L to 3L, same field as INBD CRS QUAD / RADIAL now displayed at 2L HOLD EXIT altitude restriction.
	 INESSAGES. LNAV BANK ANGLE LIMITED issued when LNAV roll command is limited to the thrust or buffet based bank angle limit. UNABLE HOLD AIRSPACE issued when predicted lateral hold path using the bank angle limit causes protected airspace to be exceeded. VSPEED UNAVAILABLE displayed if any of the independent variables used in the calculation fall outside the tabular data boundaries. Nav database size will increase from 1 meg to 2.5 meg. Runway position TOGA update inhibited when valid GPS data is being received. VNAV disconnects 7 kts before VMO/MMO rather than at VMO/MMO.
U10.2A Dec 1998	Fixed a descent lockup

UPDATE	ATE CHARACTERISTICS				
110.3	Alternate Nav capability for LCD CDU adds GPS alternate nav capability. FMC can				
Feb 2000	transmit up to 60 whits to the LCD CDU				
1002000	Cannot drive the Mans and cannot provide I NAV to the ECCs				
	Approaches: Limitation removed to allow LDA and ILS/LOC to same runway. Previously				
	there were two localizer based approaches to the same runway, but using different				
	lacelizer facilities, potter could les undats if both were in the pay database				
	Disclose anaroting anarota for (200, 400, 500) increased				
	Block operating speeds for (300-400-500) increased.				
	CLB N1 limits display all the way to 1/C. (Prior, only derated CLB N1 was displayed).				
	DIR-10 logic is improved (10 second straight line shortened).				
	Engine Out page is for reference only and no MOD/ACT is possible.				
	Engine Out SIDS can be displayed in MOD format by pushing ENG OUT>. Requires flap				
	not up and an engine out. Engine Out SID can then be executed or erased.				
	Dual FMC ops improved with better detection of vertical miscompares.				
	Flight plan size has been increased from 100 to 150 waypoints.				
	FMC Block Operating Speeds increased for 3-4-500. (Flap positions 5 and 10)				
	FMC continues operating even if both CDUs fail. LNAV, VNAV and Map operates.				
	Gradient edit rules have changed to maintain GP through various edits, which includes				
	insertion of wpts into a gradient leg and deletion of altitude restriction on gradient leg.				
	Gradient Path now displayed to nearest hundredths.(Ex: GP 3.00 rather than GP 3.0)				
	Geometric path descent (point-to-point) after the first wpt altitude constraint, (option)				
	Allows FMC to fly along a constant gradient from one altitude restriction to the next				
	Increase EliteStar flight planning tool will lead up to 20 company routes and 1 000				
	weyneinte on a dick to be leaded into the EMC (ention)				
	Massages IDS NAV ONLY discontinued and souveral added including CLITRACK				
	INESSAGES: INS INAV ONLY DISCONTINUED AND DADTIAL DOUTE LOADED DUDUCATE				
	UNAVAILABLE, ENG OUT SID MOD, PARTIAL HOUTE LOADED, DUPLICATE				
	FLIGHT PLAN ID, SUPP RTE DATABASE FULL, KEY / FUNCTION INOP.				
	N1 LIMIT page has Takeoff Bump Thrust added.				
	PERF INIT: PLAN FUEL no longer considers pack switches in logic.				
	Polar navigation. FMC will now allow flights over the poles.				
	PROGRESS 3/3 displays GPS track at 4L to support polar navigation to mitigate the loss				
	all aircraft heading data at the poles in case of dual IRU failure.				
	REVERSE Flight Plan prompt will be available on the RTE page to reverse the existing				
	flight plan. All procedures will be deleted. (included in FliteStar option)				
	RTE page reformated. Airport data on page 1. Airways and enroute data starts on page 2				
	Runway symbol now retained on the Map during missed approaches. (Prior software it w				
	removed when the runway was sequenced)				
	Bunway waynoint can be end-of-descent anytime. PDI defaults to 3° if direct-to.				
	SAVE Flight Plan prompt included in FliteStar option: available on the RTF page to save				
	the current flight plan for recall at another time. Must give it a name. (limit of 10)				
	SLIDD Nev detabase size increased from 20 to 40 waynoints				
	TAKEDEE DEE page automatically changes to CLB page after takeoff				
	TAKEOFF HEF Page automatically changes to OLD page alter takeoil.				
	TAKEOFF HEF 2/2 "Quiet Climb" (option) COTBACK prompt along with reduction and				
	restore altitudes. Provides cutback maneuver to support noise abatement such as				
	Orange County (requires -52 autothrottle).				
	UNABLE REQD NAV PERF-RNP message displayed for all cases of ANP exceeding RN				
	This is the feature that supports elimination of IRS NAV ONLY message.				
	VNAV no longer disconnects at GS-XX unless FCC G/S armed. This supports ILS overla				
	VNAV PATH now valid to two-times the RNP, or as long as LNAV is engaged.				
	Weather maps can be displayed on CDU when specific ACARS unit is installed.				
	XTK DEV on PROGRESS 3/3 referenced to lateral steering "path" (previously to "leg")				

UPDATE	CHARACTERISTICS				
U10.4 circa Jul 2001	Alternate Nav MCDU (Update 2 LDC) adds 2 functional capabilities beyond the normal MCDU. Provides an alternate nav solution regardless of FMC(s) status. Requires on- side GPS to be operational (option) Provides capability to upload and display weather				
na Arna ach A Arguilleana Iortín	data maps. Anomoly that caused display of UNABLE REQD NAV PERF-RNP message during approach has been fixed. Prior to 10.4, this message is inhibited as long as VOR/LOC is engaged with FD or A/P on, except that if the FD was turned off above 20 kts, the				
	APPROACH REF page redesigned to include FLAP/SPD field. GA N1 field removed. CDS (Common Display System), VSD (Vertical Situation Display), and HUD (Head-Up Display), and EGPWS has several new parameters added.				
	Clock source switching improvements. FMC will use GPS clocks exclusively if available, then will use either the Captain's (first choice) or FO's clock (if Captain's has failed). Auto switching from Captain's clock to FO's clock once the source is selected at power-up is prevented. FMC will retain last valid clock value.				
	Compatible with existing 2907A4 FMC and the new model 2907C1 FMC (new single board allowing spare card slots to support growth). Single board FMC hardware will allow spare card slots to support future growth. It also incorporates 3 high speed ethernet channels. 10.4 will run on old hardware as well as on the new hardware. If				
	an old box and a new box are installed on the same airplane, they both run at the same speed as the old box. It will run 50% faster with two new boxes. ENG OUT SID (6-7-8) auto loads MODified EO SID if an engine failure is detected, (climbout and flaps down) and departure runway has an engine out SID in the nav				
	 database. (3-4-5) requires selection of ENG OUT prompt on CLB page (option). FMS BITE maintenance page added to allow selection of new H/W CONFIG display. Go Around: If during go-around you select a procedure with a waypoint altitude constraint higher than your current cruise altitude, the crz alt is raised to equal the highest constraint in the procedure and the "CRZ ALT CHANGED TO XXXXX" message is displayed. Cruise altitudes that are "made up by the FMC", such as the crz alt resulting from missed approach, or from selecting a procedure as above are 				
	GPS reasonableness checks added in addition to GPS fault indications. GR WTmanual entry or deletion at 1L of PERF INIT page is inhibited (option). HOLD EXIT prompt improvements: If you are in holding and change the leg time or inbd				
	 crs, U10.4 will retain the prompt while you finish the old pattern. Previous software removed the EXIT HOLD prompt until after you finished current pattern. Holding Pattern Resize: If your leg time is 1.5 min because the holding pattern was built above 14000', and you then descend in holding to below 14000', the pattern will resize to 1 min legs. Auto re-size only if leg time or leg length have not been manually entered. If the crew makes a manual entry into either the time or distance field, the hold will not resize. Climbing or descending through 14,200' is the trigger. Holding: Default entries for QUAD/RADIAL, INBD CRS/DIR, or LEG TIME are displayed 				
	in small font. Large font for pilot entry or data extracted from nav database. IRS reasonableness checks have been improved in dual FMC installation such that both FMCs are better able to identify and reject a badly drifting IRS. Message VNAV DISCONNECT displayed if FCC goes from VNAV to LVL CHG during				
	approach. Missed Approach path is displayed in cyan prior to being active (option). Model/Engine database size increased to 1.5 mega-words. Previous size was 1.0. Nav database size increased to 3.5 mega-words. Previous size was 2.5 mega-words.				
John of News Solds a	Nav database size increased to 3.5 mega-words. Previous size was 2.5 mega-words.				

Dec 02			

UPDATE CHARACTERISTICS			
U10.4 (continued)	 RW/APP TUNE DISAGREE and RW/APP CRS ERROR messages for conditions where a tuned frequency or MCP selected course does not match the FMC flight plan data. TAKEOFF DERATES on N1LIMIT page blanked and disabled for carriers that only use Assumed Temp (option). UNABLE REQD NAV PERF-RNP anomalyhas been resolved. Various fixes including intermittent blanking of the Map. VNAV (max) command reduced from -7° FPA to Mmo/Vmo-5 when above SPD REST. VNAV (max) command reduced from -6° FPA to 250 kts when below SPD REST. VNAV remains in PATH, even if XTK ERR exceeds RNP. Previous software reverted to SPD DES. (idle descent legs and computed gradient legs). VNAV will switch to PATH when speed intervention is exited if not already in PATH. 		
U10.4A	Corrects 3 problems in 10.4 Adaptable Datalink database part number intermittently / erroneously displayed on CDU FMC failure due to an incorrect ARINC wrap test (limited to 2907C1 hardware) Move boot software problem corrected (limited to 2907C1 hardware)		
U10.5 (Jan 2003)	 Altitude Constraints: The next active wpt altitude constraint will be displayed on the CDS Map under the wpt identifier even if the RTE DATA switch is off. Approach Ref Speeds: allows entry into 4R of FLAP/VREF values of 0, 1, 2, 5, 10, or 25. If a non-standard flap setting is entered (i.e. one not displayed in 1R-3R) then a VREF speed must be manually entered because the FMC does not compute a speed for these flap settings. ARRIVALS page has G/S ON/OFF prompt. The prompt will work identical to the prompt on the APPROACH REF page. ATC light and chime status, part of FANS-1 option, displayed on Fixed Output page. Calculated Takeoff Speeds changed: thrust rating, temperature, and airport altitude are now included in the calculation of Minimum TOGW (benefits 737-700BBJ) Climb-to-descent transition: VNAV can swtich from climb to descent when it runs into the planned descent path. Previous software required a lower entry of a CRZ altitude. This caused confusion after a missed approach and selection of another approach. Double Derate takeoff and climb thrust mode annunciations can now be displayed on the CDS. The new derated takeoff and climb thrust modes displayed (in place of the R-TO and R CLB) on the CDS will be T0 1, T0 2, D-T0, D-T0 1, D-T0 2, CLB 1, and CLB 2. Engine Performance Model (EPM) modified to table lookups as a function of altitude and corrected N1. FANS-1 via ACARS datalink: (option) ATC datalink (ATC DL) enables ATC/pilot datalink communication via the MCDU; Automatic Dependent Surveillance (ADS) provides for automatic position reporting, and ATS Facility Notification (AFN) provides for logons to ATC facilities to notify ATC of an aircraft's <i>address</i>. Fuel filter time constant decreased to 5 sec on the ground for display on PEF INIT and PROGRESS GPS Landing System Approach (GLS) (option). GLS approach types (LAAS only) if defined in the nav database. Currently, allowed to CAT I minimums. Int		

Dec 02

UPDATE	CHARACTERISTICS				
U10.5	The resulting modified FP will be executable, with a new alerting level message. CR7 ALT				
(continued)	CHANGED TO XXXXX. Previously the FP could not be executed until a new/lower CRZ				
	allitude was entered.				
18100 11110	Message ATC MESSAGE, part of FANS-T option, displays on map in amber.				
	nav radio is re-tuned to an ILS (enhancement to CIAP logic).				
a	Message VSPEEDS UNAVAILABLE display logic changed: to display if gross weight is less				
. Tir - 7 i e	than a value derived from a new Model Engine database table, as a function of thrust rating,				
	ambient temp and pressure altitude.				
	Missed Approach predicted sooner: previous software predicted MA path approximately .8 nm from MA point. MA now predicted full time so that crew can determine turn directions and				
	other data before actually beginning the MA.				
	NAV STATUS page reflects GLS channel tuning; this includes highlighting and prefix				
	nomenclature, i.e., P (procedure), M (manual), or A (autotune) for the tuned channel				
	number.				
	PROGRESS pages 2 and 3 have been reversed to match other Boeing aircraft.				
	RNP: Capability to review and enter lateral and vertical approach RNP values using a new RNP PROGRESS page (3R).				
	Runway of destination can be entered on the FIX page and on the WPT/ALT data field of the				
	DESCENT page. Down-selection of LSK 2L through 4L on FIX page is inhibited. Threshold				
	crossing height fills in automatically with destination runway entry on DES page. (Ex: RW26/				
	a socrasticitate flag adding in withend if it, one not deployed in HT-RF, The				
	TACAN approaches can be selected from the nav database. TACANs designated as military use ("M" types), channels 1-16 and 60-69 will not be included at this time but the U10.5 s/w				
	may be structured to include them at a later date. The FMC will not tune the procedure navaid associated with the TACAN approach.				
	Thrust Bating Model (TBM): adds new 737-600 configurations with 7B22/B2 bump thrust rating				
	and new 737-700 configurations with 7B26/B2 bump thrust rating.				
	Tropopause breakpoint predictions (add a new phantom vertical wpt at the trop altitude to				
	account for differences in the atmosphere models below and above the trop). Should reduce				
	the tendency to overspeed during path descents that start above FL360.				
	UNABLE CRZ ALTITUDE condition exists, FMC transitions directly from climb to descent				
	predictions when the aircraft cannot reach cruise altitude before it encounters the descent				
	path. The FMC will compute an achievable cruise altitude, referred to as the internal cruise				
	altitude. A short cruise segment will be created, but the CRZ page will be suppressed, i.e., if				
	the page is currently displaying the CLB page, the CDU display will automatically switch to the DESCENT page.				
	VNAV limits modified: Max flott path angle is approximately that which will result in a speed of				
	Mmo/Vmo - 5 kt above 10.000 ft and 250 kts below 10.000 ft.				
	VMAV Overspeed: VNAV authority modified. Currently 7° FPA above the airport speed				
	restriction altitude and 6° below the airport speed restriction altitude. Changed to an angle				
	that will result in a speed of Mmo / Vmo – 5 kt above the airport speed restriction altitude				
	and DES page speed restriction + 10 kt below the airport speed restriction altitude. This may				
	result in fewer VNAV disconnects				
	VNAV Speed Band: this feature depicts upper and lower limit speeds for VNAV PATH. The				
	descent speed will be augmented by the display of a speed band on the speed tape of the				
	PED. The top of the speed band will indicate the speed at which the descent quidance mode				
	switches from nath-on-elevator (VNAV PATH) to speed-on-elevator (I VI CHG). If the A/T is				
	on the bottom of the speed band will show where the A/T switches from ARM to FMC.				
	SPEED If the ΔT is off the bottom of the speed hand will show 15 kts below the speed				
	target and a THRUST REOD message will be displayed if the speed falls below that value				
	and a minor measure will be displayed if the speed tails below that value.				
	me not el brochtenen markage och an persente affandes sources - 7 1 Markage i vell				

TEMPORARY

SOFTWARE UPDATES UPDATE CHARACTERISTICS ANCDU Fixed Outputs problem fixed that prevented access. U10.5A FMC failure annunciation of the Multi-Mode Receiver (MMR) for GLS installations corrected. (Jul 2004) FMC logic improvement to reduce the occurrences of nuisance messages: RESET MCP ALT, UNABLE CRZ ALT, THRUST REQUIRED, USING RSV FUEL, CHECK FMC FUEL QUANTITY. MOD Hold Symbol problem corrected (incorrect display). PLAN FUEL display logic revised to ensure the field is correctly displayed on 737NG's with older auto-throttles. Restart problem corrected. U10.6 Airframe/Engine program pins (2) added to support more 737 model types (Projected Altitude Intervention - approach waypoint altitude constraints cannot be deleted to prevent aircraft from flying below minimum altitudes. Earlier software allowed this. Mar 2005) ANP is enhanced to account for sensor position and cross-track deviation differences between the 2 FMCs. ANP and position data for the last 10 RNP exceedences or VERIFY POSITION events are recorded by the FMC. ARRIVALS page added field: After selecting one of the destination runways, the FPA header is displayed. The crew can modify the descent gradient angle in the FPA field. Entry propagates to (GP x.xx) on LEGS page. ATS-Datalink: Access to ATS Uplink Delay Timer which allows FANS-1 a/c to operate in European airspace. Crew enters delay value into the LOGON/STATUS page. This change tells the crew if a datalink clearance is older than a voice message that was sent to replace it. Message UPLINK DELAY EXCEEDED displays if time is exceeded. Cruise Speed Propagation (option) - When a manual speed is entered on the CRZ page (CAS or M), it propagates to the DES page. DES - Geometric Path descent is now basic, not optional. Point-to-point instead of stair-step after the first idle descent. Path descent is now always available when at least 1 wpt is included in the descent. SPD DES prompt removed from DES page when active leg is a STAR or when the approach transition leg has a vertical angle. Dual FMC logic changed to reduce the occurrence of reverting to single FMC ops due to dual FMC software logic disagreements. The change allows the dual FMC system to continue operating while disagreements are resolved with no required crew action. Engine Out SID - the FMC will search the E/O SID database to find out if the active wpt is one of the wpts in the E/O SID. If the active wpt exists in the E/O SID, the remaining portion of the E/O SID will be loaded without a lateral discontinuity after the active wpt. Wpts prior to the active wpt are ignored. Estimated Time of Arrival and Fuel Remaining predictions are corrected. Flight Plan Intent Bus Output Option: in support of European 4-D FMS flight trials. FIX page (option) - four added for a total of six. Integrated Approach Nav option: glide path deviation now provides a smoother display under transient conditions and supports classic a/c that has compatible displays and A/P. LNAV nominal bank angle is 1/2 the track angle change with a minimun of 8° to a max of

23°. Not applicable for procedure turns, procedure holds, or holding patterns. Missed Approach LNAV go-around (CDS option) operation is changed to provide automatic re-engagement of LNAV. The missed approach must be in the active flight plan and cannot be followed by a discontinuity. Pressing TOGA while the a/c is below 400 ft AGL places LNAV in an armed state (white on FMA). During climb-out, LNAV is automatically re-engaged at 400 ft AGL.

MODEL ENGINE database size is increased from 1.5 to 2.0 mega-words to support more 737 model types.

TEMPORARY

SOFTWARE UPDATES

UPDATE	CHARACTERISTICS				
U10.6	Operational Program Software (OPS) supports APB wingles for -300 and -400 a/c.				
(Projected Mar 2005)	QRH - new logic ensures that the entered QRH V1 is less than or equal to VR and VR is less than V2 (V1 \leq VR $<$ V2). If an entry is made that violates V1 $<$ Vr $<$ V2, the remaining V speeds are deleted.				
	Quiet Climb modified to keep CUTBACK enabled during re-entry of Vspeeds except when manually disabled or past the cutback altitude. On earlier software, re-entry of Vspeeds during quiet climb disabled quiet climb.				
	SEL DES WPT page improvements: Title changed to SEL DES XXXXX where XXXXX is the ID of the duplicate. 15 characters to display names of airports, VHF navaids, and non-directional beacons.				
	Frequency (VHF or NDB) displayed in left column. New page format can be used with or without extra data in nav database.				
	A maximum of 12 duplicates on two pages may be displayed. SPD DES will switch to PATH DES on point-to-point legs.				
	Vertical Required Navigation Performance (VRNP) will be increased to 400 ft to allow the				
	 deviation pointer to come off the upper stop earlier during a normal G/P capture. VNAV Option (common): VNAV SPD is used as the speed on elevator mode for overspeed reversions instead of disconnecting VNAV. This option removes the selectable SPD descent mode and the PATH or SPEED designation from the CDU descent page titles. 				
	VNAV DISCONNECT nuisance message will not be displayed when VNAV transitions from a missed approach.				
	VNAV PATH will no longer auto-change to VNAV SPD under any circumstance.				
	Winglet configurations supported for 737-300 and -400.				

-300

DISTANCE	COST INDEX					
	0	28	60	100	200	
1	Time	Time (min) / Fuel Burn (1000 lbs)				
2400	-5/.2	0/0	3/2	7 /6	14/-2.1	
2000	-5/.2	0/0	2/1	6/5	11/-2.1	
1500	-5/.2	0/0	2/2	4/5	8/-1.4	
1000	-4 / .1	0/0	1/1	3/3	6/1.0	
500	-4/.1	0/0	1/0	2/1	3/4	

WIND TRADE TABLE				
OFF-OPTIMUM ALTITUDE	WIND DIFFERENCE REQUIRED			
+ 2000 ft	7 kts			
- 2000 ft	5 kts			
- 4000 ft	15 kts			
- 6000 ft	30 kts			
- 8000 ft	50 kts			

737-300 / 20k				
OFF-OPTIMUM CONDITION	FUEL MILEAGE PENALTY			
2000 ft ABOVE	torus skiller 1	1		
AT OPT Altitude	0	0		
2000 ft BELOW	1	2		
4000 ft BELOW	4	4		
8000 ft BELOW	10	11		
12.000 ft BELOW	15	20		

737-700 / -7B24			73	37-800 / 7E	326		
OFF-OPTIMUM CONDITION	FUEL MIL	EAGE PE	NALTY % CI30	OFF-OPTIMUM CONDITION	FUEL MIL	EAGE PE	NALTY % CI30
2000 ft ABOVE	2	2	2	2000 ft ABOVE	S S N I S S S S S S S S S S S S S S S S	1	1
AT OPT Altitude	0	0	0	AT OPT Altitude	0	0	0
2000 ft BELOW	a) 7 - 1 1 7 8 -	2	2	2000 ft BELOW	101 101 104	2	2
4000 ft BELOW	4	5	4	4000 ft BELOW	4	6	5
6000 ft BELOW	6	10	7	6000 ft BELOW	7	10	8
8000 ft BELOW	9	14	11	8000 ft BELOW	9	16	12
10,000 ft BELOW	11	19	14	10,000 ft BELOW	12	20	15
12,000 ft BELOW	14	24	16	12,000 ft BELOW	16	23	20

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PERFORMANCE CHARTS

COST INDEX FLIGHT PLANNING TABLES

Use to determine the difference from a Cost Index of 28. Example: If a -300 flight with a distance to go of 1000 nm were to change from a CI of 28 to 100, it would save approximately 3 minutes to burn 300 extra pounds of fuel.



MACH AIRSPEED DIFFERENCES TABLE

The approximated potential range of CI manipulations is shown in this table, depicting zero wind cruise Mach at CI = 0 and CI = 200 typical for the conditions indicated.

FLIGHT	GROSS WEIGHT (1000 lbs)				
LEVEL	90.0	100.0	110.0	120.0	
	CI = 0 / CI = 200				
370	.714 / .785	.726 / .776	.733 / .772	.736 / .767	
350	.696 / .788	.715 / .782	.726 / .775	.733 / .770	
330	.675 / .789	.698 / .785	.716 / .780	.725 / .775	
310	.654 / .789	.678 / .786	.699 / .783	.715 / .778	
290	.632 / .789	.657 / .786	.680 / .784	.698 / .780	
250	.590 / .786	.624 / .786	.638 / .784	.658 / .783	
200	.540 / .784	.565 / .784	.586 / .784	.609 / .783	

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FACTORY LOADED DEFAULTS

DEFAULT PARAMETERS	DEFAULT VALUES 737-3-4-5	DEFAULT VALUES 737-6-7-8-9
Hold pattern leg time below 14,000 ft	1.0 min	same
Hold pattern leg time above 14,000 ft	1.5 min	same
Transition Flight Level (descent)	18,000 ft	same
Transition Altitude (climb)	18,000 ft	same
Climb mode	ECON	same
Cruise mode	ECON	same
Descent mode	ECON PATH	same
Departure airport altitude restriction	250 kt	same
Departure airport altitude restriction	10,000 ft	same
Destination airport altitude restriction	240 kt	same
Destination airport altitude restriction	10,000 ft	same
Thrust Reduction altitude (10.2A and earlier)	1500 ft	same
Thrust Reduction altitude (10.3)	1500 ft	loadable Model/Engine db
Cutback Reduction altitude (10.3)	na	loadable Model/Engine db
Cutback Restore altitude (10.3)	na	loadable Model/Engine db
Takeoff flap setting	5	loadable Model/Engine db
BTA time error tolerance	30 sec	same
Climb min speed CAS	210 kt	same
Climb max speed CAS	340 kt	loadable Model/Engine db
Climb min speed Mach	.400	loadable Model/Engine db
Climb max speed Mach	.820	loadable Model/Engine db
Cruise min speed CAS	210kt	same
Cruise max speed CAS	340 kt	loadable Model/Engine db
Cruise min speed Mach	.400	loadable Model/Engine db
Cruise max speed Mach	.820	loadable Model/Engine db
Descent min speed CAS	210 kt	same
Descent max speed CAS	340 kt	loadable Model/Engine db
Descent min speed Mach	.400	loadable Model/Engine db
Descent max speed Mach	.820	loadable Model/Engine db
Drag Factor	0.0%	same
Fuel Flow Factor	0.0%	same
Maneuver Margin	1.3	loadable Model/Engine db
Minimum cruise time	1 min	same
Minimum B/C - Climb	300 ft/min	same
Minimum B/C - Cruise (U10.0, 10.1, 10.3)	100 ft/min	same
Minimum B/C - Cruise (U10.2 & 10.2A only)	300 ft/min	same
Minimum B/C - Engine Out	100 ft/min	same
Cost Index	Box Prompts	same
	Box Frompto	Samo

토리아슈퍼 2564457월만에게 안 야별할지수야요. 통하는 것

The representation process is reacted with the process A is a proved by the table, depicting A to which when M_{abs} at CI = 0 and $CI = 10^{-1}$ by the conditions with the d

CECURE WEIGHT (UNO Inc)				
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OFP	P/N	Processor	RAM	NDB size	NDB type
UO	539632	16 bit / 68000	84 kw	96	U1
U1	545271		1	96	U1
U1.1	547068			96	U1
U1.2	548394	1/8/r _18/	18MA	96	U1
U1.3	548720	ASE PERMOR	1 BAA	96, 192	U1, U3
U1.4	549100	Suburg-Japogav	1.634.0	96, 192	U1, U3, U5
U1.5	549397	1981	213.6	96, 192	U1, U3, U5
U1.6	549791	Res PTU	*	96, 192	U1, U3, U5
U3	547444	EL AND MY MY	108 kw	96, 192, 288	U3
U3.1	548568		ustejna Historija	96, 192, 288	U3
U4	548659	16 bit / 68000	Concession of the second se	96, 192, 288	U3, U5
U5	548925	on ASIC	V	96, 192, 288	U3, U5
U6	548926	Lister Contract in	124 kw	96, 192, 288, 512, 1M	U3, U5
U6.1	549260	BPL outs		288, 1M	U3, U5
U6.2	549349	HOADY HOALIS	V	288, 1M	U3, U5
U7	549297-12	32 bit / 68040	512 kw	256, 1M	U3, U5
U7.1	549297-34	N SUN NOON	(433)	256, 1M	U3, U5
U7.2	549297-38	. 88	FOI	256, 1M	U3, U5
U7.3	549297-41	SHIND SHOL	PIQU/	256, 1M	U3, U5
U7.4	549297-45	1022 11 1911-1941	F/O /	256, 1M	U3, U5
U8	549250-15	and the second	1004	256, 1M	U3, U5
U8.1	549250-19	314. rkprove 90,44	HQ1	256, 1M	U3, U5
U8.3	549250-22	al I spega	153.6	256, 1M	U3, U5
U8.4	549250-26			256, 1M	U3, U5
U10	549849	↓	2M	256, 1M	U3, U5

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Non EFIS FMA A/T N1 LIMIT AFDS CON TO A/T FMC P/RST A/P OFF A/P A/P STATUS N1 LIMIT A/T AFDS CRZ LNAV WC SP VOR LOC CLB ARM REDUCED V/S G/S FLARE TO

When EFIS is installed, the FMAs are located in the EADI. The Thrust Mode Annunciator displays N1 thrust modes.

A/T

A/P

CWS F

CWS PITCH

A/P STATUS

TMA LIGHTS TEST switch in TEST, this display - blinks

R-TO R-CLB CRZ G/A CON A/T LIM

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 $1 \frac{1}{2} \underbrace{\bigcirc}_{TEST}$

FMC P/RST

EFIS Control Panel that comes with the 300/500 with GPS.



CAT I: DA/MDA ≥ 200 Visibility $\ge 1/2$ mile or RVR ≥ 1800 1. Requires one transmissometer.

- 2. If both autopilots are inop, the Monitored Approach Procedure should still be used with the FO flying manually.
- 3. CAT I or Non-precision approach, PM will call "Approach lights in sight", and/or "Runway in sight". Informative, not directive.
- 4. When conducting non-precision or CAT I ILS approach, you may
- descend to 100' above TDZE with approach lights in sight. 5. May not descend below 100' above the TDZE unless visual refer-
- ence to the runway is established. 6. MDA and DA altitude value measured by barometric altimeter and
- is controlling. Height value from a radio altitude is advisory. 7. CAT I using MDA are: VOR, LOC, NDB, RNAV without VNAV.
- 8. CAT I using DA are ILS and RNAV with VNAV.

CAT II: DH≥100 RVR≥1200 RVR≥1000*

- 1. Will be made with autoland if a/c and crew are autoland capable.
- 2. Single autopilot is authorized to CAT II minimums.
- 3. First Officers, think of taking it to the DH then to a missed app.
- 4. Height value (DH), based on RA, is used for CAT II ops except where procedures have "Radio Altitude Not Authorized" (RANA). Due to irregular underlying terrain, typically use the first indication of arrival at the inner marker as a means to establish DH. Altitude value (DA) measured by barometric altimeter is advisory.
- 5. CAT II Autoland and CAT IIIA procedures are the same except for the decision height.
- 6. For CAT II, TDZ, MID, and ROLLOUT RVR should be provided for any runway over 8000 ft.; TDZ and ROLLOUT for runways less than 8000 ft.
- 7. You are required to have landing minimums prior to GS intercept altitude. If weather goes below landing minimums once established on the glideslope, you may continue to landing on CAT I or CAT II approach if approach lights, red terminating bars, runway end lights, touchdown zone lights, etc are visible at miminums,
- 8. May not descend below DH unless visual reference to the CAT II lighting system is established.

* If published as the approach minima.

If weather conditions are below 4000 RVR or 3/4 mile visibility a FD must be used or a coupled approach must be made. LOW VISIBILITY APPROACHES (CAT I, II, III)

- If TDZ RVR is at or below 2400 (defines a low visibility approach) a. monitored Approach should be flown,
- b. autopilot should be used,
- c. the crew must brief (and fly) the category of approach having

the lowest minimum applicable to facility, aircraft, and crew. If TDZ RVR is at or below 1800 an auto-coupler is required. If TDZ RVR is below 1600, two transmissometers are required. If TDZ RVR is below 1200

- a. autoland is required,
- b. braking action must be fair or better,
- c. takeoff or landing ops require Surface Movement Guidance and Control System (Low Visibility Taxi Procedure - ICAO)

ILS APPROACH

CAT III: DH < 100 or no DH RVR < 1200

CAT IIIA: DH < 100 or no DH RVR ≥ 600 CAT IIIB: DH < 50 or no DH RVR < 700 but ≥ 150

- 1. Requires 737-NG and autoland.
- 2. SMGCS defines Low Visibility Taxi Routes and goes into effect when visibility is less than 1200 RVR.
- 3. Four operational differences between CAT II Autoland and CAT IIIA approach:
- a. Status annunciator must indicate CAT IIIA
- b. RVR minimums for CAT IIIA approach have specific transmissometer requirements (3). (See chart at bottom)
- c. CAT IIIA procedure using a fail-passive autoflight system incorporates a DH set on RA (or an equivalent IM position fix).
- d. Captain makes additonal callouts of "200" at 200 ft above
- TDZE and "Approaching minimums, I'm going heads up" at 150 ft above TDZE.
- 4. You are required to have landing minimums prior to GS intercept altitude. And, you must have the minimum RVR for landing prior to the DH. (May continue to landing if you can use CAT I or II criteria.)

FAIL PASSIVE

A system which, in the event of a failure, causes no significant deviation of aircraft flight path or attitude.

- AC 120-29A groups instrument approaches into 3 categories: (a) xLS
- ILS, MLS, GLS (Global Landing System)
- (b) RNAV
- FMS, RNAV using traditional VOR/DME sensors, GNSS (c) Instrument Approach Procedures other than xLS or RNAV
- traditional approaches such as VOR, NDB, LOC, LOC Back crs. and ASR

Visibility	RVR	APPROACH	BARO	RA	
1	5000	TYPE	SELIO	SELIO	
_	5000	CAT I	Published DA	Published DH	
3/4	4000	CAT II	Published DH (TDZE + 200 ft)	Published RA	
1/2	2400	CAT IIIA	TDZE + 50 ft	50 ft RA	
1/4	1600	BOLD indicates controlling altimeter.			

Visibility Requirements: TDZ MID ROLLOUT NOTES LIGHTS RVR Down to: Required Controlling Not req'd Advisory Not req'd Advisory MID can sub for TDZ if inop CAT I DA(H)/MDA ≥ 200 Visibility ≥ 1/2 mile or RVR ≥ 1800 TDZ and CL * * Required Not req'd Controlling Advisory Not req'd Advisory HIRL, TDZ, CL ALSF 1, II, ICAO CAT II DH ≥ 100 RVR ≥ 1200 * No Substitutions * * Required Advisory Required Controlling Required Controlling If only two, both CAT III DH < 100 RVR < 1200 ** control. Required Required Controlling Required CAT IIIA DH < 100 BVB ≥ 600 * * * CAT IIIB DH < 50 RVR < 600 but ≥ 150 * * *

* For CAT II approaches: if TDZ RVR is below 1600, an advisory Mid or Rollout RVR must be reported ≥ 1000 if published as the approach minima.

PF = Pilot Flying / **PM** = Pilot Monitoring

B737 PROFILES PF = Pilot Flying

PM = Pilot Monitoring

GENERAL:

- 1. Captain briefs Monitored Procedure; FO briefs the approach chart. 2. Flaps 40 slightly more sight over nose
- a. Landing lights optional, cockpit lights low
- b. Max Seat height (consider sighting of FMA)
- c. Autobrakes req'd recommend 3 and don't kick off till < 80 kts.
- d. Start APU for backup electrics and check stby ADI in ILS APP.
- 3. ATC is required to have approach/runway lights on step 5.
- 4. Non-EFIS CAT II ops, both Captain and First Officer must position HSI switch to VOR/ILS prior to commencing the approach. 5. -500: This step not required for NG
- Both pilots must select MANUAL prior to commencing the approach to display ILS data on ADI.
- 6. Except for dual-channel approach and autoland, autothrottle must be disconnected prior to: non-autoland ILS, no lower than 50 ft AGL non-precision or visual, no lower than 100 ft AGL
- 7. CAT II and III approaches will not be flown if LLWAS or windshear with reported airspeed gain or loss is greater than 10 kts.

AUTOLAND:

- 1. Status annunciator will be either CAT IIIA on NG 737 or CAT II AUTOLAND on all other aircraft.
- 2. Autothrottle and two autopilots are required criteria for engagement are: valid ILS frequency in both nav radios, same inbound course in both course windows, and APP armed.
- 3. If you practice an autoland with RVR >2400, ask Approach and Tower for "Beam Protection for autoland". ATC does not hold a/c short of the ILS Hold Short Line until 800 and/or 2 nm. The ILS signal is not protected from airborne interference (i.e. a/c ahead of you) until wx goes below 200 ft ceiling and/or 2000' RVR.
- When cleared for the approach, arm APP and engage second A/P. If the second A/P is not engaged by 800 ft RA it is locked out.
- 5. After G/S capture and 1500 ft the second A/P pitch channel is engaged and the ILS Deviation Warning Test is performed. SINGLE CH disappears and FLARE ARMED is annunciated. Dual A/P GA is armed.
- 6. If FLARE is not armed by 350 ft RA both A/Ps disengage.
- 7. After touchdown, Captain must disconnect A/P because there is no automatic tracking of centerline.
- 8. On a missed approach, when LVL CHG is selected at 1000 ft AGL, the last autopilot engaged will disconnect; this will be "A" A/P under normal operations. The Captain, if flying the missed, should be aware that "B" A/P might be the master.
- 9. Wind limits: headwind 20 kts, crosswind 15 kts, tailwind 10 kts.

All US Cat I operating minimums below 1/2 statute mile (RVR2400) and all Cat II and III operating minimums are based on BVB Controlling RVR must be at or above minimums prior to final approach segment. *** Controlling RVR must be at or above mins prior to final approach segment and prior to descent below DH.

VOR, LOC, LOC (Back Crs), NDB (Single FMC and DME-DME Updating) (Dual FMC and GPS) / CAT I

B737 PROFILES PF = Pilot Flying **PM** = Pilot Monitoring





B737 PROFILES

Page 3

RNAV Considerations:

- The RNAV Approach (or GPS Approach) is designed to be flown in LNAV and VNAV (BARO VNAV).
- The RNAV approach in the 737 is not as easy as the ground based ILS but it beats the traditional step-down technique.
- 3. Practice in VFR conditions, especially if parallel approaches are being conducted. Do not wait until you actually need this tool to use it. With the AP engaged, take the airplane right down to minimums to see just how well it lines up with the landing threshold. Expect a GPS updated system to perform the best.
- 4. BÅRO VNAV presents computed vertical guidance referenced to a specific vertical path angle (VPA). The computer resolved vertical guidance is based on barometric altitude. The correct setting of the altimeter does not correct for non-standard temperature. The only way to meet this requirement is to observe the limiting minimum aerodrome temperature annotated on the chart. Errors become proportionally greater with altitude above the altimeter site, usually an airport. The colder the temperature, the shallower the actual angle flown. Ref: VPA DEVIATIONS chart.
- 5. (300-500) Place both nav switches in AUTO.
- (700-800) You will notice a lower ANP with GPS input. 6. Speed Control:
- a. If your airline's management team has not had the foresight to order Speed Intervention, the RNAV Approach gets a little more complicated. (You can tell where I stand on this issue)
- b. Speed Intervention allows one to control speed using the open IAS / MACH window while remaining in VNAV. Speed Intervention should be standard equipment on the 737, just as it
- is on all the Big Boeings, but the factory does not see it that way.
 c. It hardly needs to be said that in today's environment, most approaches to a hub airport come with speed clearances from the approach control-
- to a hub airport come with speed clearances from the approach controller. For the crew flying the 737 without Speed Intervention, you have two choices for speed control; use the Mode Control Panel V/S or LVL CHG, which opens the Ks / MACH window, or use VNAV, in which case the target speed follows the flap handle! VNAV offers altitude protection on the LEGS pages, but you may have to disconnect the autothrottle and set the throttles manually. The flap handle derived speed may not match the speed clearance (or your own desired speed). Do not use VNAV SPD with manual throttles.
- Use the autopilot. This will reduce the chance of cross-track error. On the 10 mile range, the magenta route must not exceed the width of the airplane symbol.

Using V/S or LVL CHG to the FAF 1. Advantages:

a. For the crew without Speed Intervention, V/S or LVLCHG is the easiest

method of meeting an ATC speed clearance during the stepdown phase; use of the autothrottles may be maintained throughout the approach. b. If there is no ATC speed clearance, VNAV SPD or VNAV PATH can be

RNAV APPROACH

NOTES

- used.
- 2. Disadvantages:
- a. Each stepdown must be entered in the MCP ALT select.
 b. Tell your teammate to remind you to reset the MCP ALT after each ALT HOLD
- 3. Monitor stepdowns using the green altitude trend vector.
- 4. Though you can use V/S to follow the PDI inside the FAF, I'd recommend transitioning to VNAV PATH at the FAF to maintain the constant vertical angle to the threshold. This will lower your workload.

Using VNAV SPD or VNAV PATH to the FAF:

1. Advantages:

- a. VNAV will not bust the altitude restrictions (stepdowns) on the LEGS page prior to the FAF as long as you remain in VNAV. If you ever leave VNAV or V/S or LVL CHG, be sure to re-check the MCP altitude.
- b. VNAV may bust the DA/DDA.
- c. The MCP ALT must be set below the FAF altitude or VNAV will disengage at the FAF. The MCP ALT may be set to zero (or whatever your SOP calls for).
- 2. Monitor stepdowns using the green altitude trend vector.
- I recommend using VNAV SPD for step-downs because it's confusing trying to figure out when PATH will start each idle descent (unless you have the geometric point-to-point option).
- a. In VNAV SPD the airplane will descend at idle throttle at the active speed to the next altitude restriction on the LEGS page. Just like LVL CHG, it is not slaved to the path, but to speed.

Arriving at the DA:

- If one of the *required visual references* is not in sight prior to the DA you must level off at the DA. This will result in a mandatory missed approach. Ideally, you want the runway in sight prior to DA/DDA. When the field is in sight, disconnect the autopilot no later than 50ft below the DA/DDA and continue the approach visually.
- ane Initiate a Go-Around for the following:
 - 1. Deviation from the lateral and vertical path, as described.
 - Lack of adequate visual references at minimums.
 If the ANP exceeds the RNP inside the FAF (message UNABLE REQD NAV
 - The ANP exceeds the KNP inside the PAP (incssage bit ALL inclus in AP PERF).
 Next Generation a/c with U10.2 software and up allows winding the MCP
 - A. Next Generation are with 010.2 software and up allows winding the MCH ALT to the missed approach altitude after passing the FAF by a few hundred feet.

VNAV PATH vs VNAV SPD VNAV PATH

- a. The vertical flight path is slaved to the PDI.
- b. VNAV PATH will be indicated on the FMA if in VNAV. The DES page will be titled ACT PATH DES.
- c. The active speed will be highlighted at 3L on the DES page.d. When being vectored for the approach, it will be a speed from the
- SPD REST field such as **[240]** or **[210]** or it may be flap driven such as **[190 / FLAPS**]
- e. Unless you have the geometric point-to-point option (CO does not), the airplane will fly level until intercepting the next step-down path. Active speed is controlled by the flap-handle, or the Speed Intervention window (optional equipment).
- f. For those without speed intervention, disconnecting the autothrottle allows manual control of the airspeed if needed.

VNAV SPD

- a. The vertical flight path is slaved to the active speed on the DES page or the Speed Intervention window; it is very similar to LVL CHG.
 b. VNAV SPD will be indicated on the FMA if in VNAV.
- The DES page will be titled ACT SPD DES. The PATH > prompt will be displayed at LSK SR if the XTK ERR is less than the RNP and can be re-selected. The PATH > prompt will appear after an intercept-leg-to followed by engagement of LNAV or after a direct-to operation.
- c. The active speed will be highlighted at 3L on the DES page.
- d. When being vectored for the approach, it will be a speed from the SPD REST field such as 240 or 210 or it may be flap driven such as
 - 190 / FLAPS

Arriving at the FAF:

- 1. Don't arrive at the FAF with excess energy. If the controller requests "190 to the marker", just say "Unable"
- 2. Desireable configuration:
- 4 miles from FAF Gear down, Flaps 15 PDI approaching center – Flaps 30
- PDI approaching center raps 50
 3. Though you can use V/S to follow the PDI, I recommend VNAV; this will lower your workload. If you press the VNAV button (sometimes necessary to hold for a couple of seconds) but it does not engage, then as a backup, use V/S to follow the PDI. Teach yourself how to use the FPA, V/B, and V/S information on the DES page. You did remember to spin the MCP ATT to zero before pressing the VNAV button didn't you?
- A. The FMC will automatically change to VNAV PATH when you reach a LEG with a Gradient Path (GP), Gradient Path is a leg with an angle contained in the database, so there's no need to select the PATH prompt (DES page) prior to reaching the marker.
- 5. The target speed will come from your selection of the VREF on the APPROACH REF page plus the WIND additive. The target speed is active when the gear and landing flaps are selected. If you forget to make your VREF selection, the target speed will not go below the flaps 15 speed, and you'll get a message APPRCH VREF NOT SELECTED.

B737 PROFILES PF = Pilot Flying PM = Pilot Monitoring

Calculating a VDP

Assuming you are level at the MDA, the VDP is reached when the

V/B indicates 2.8 to 3°. Ref: Procedures B and C. This takes

I ways to compute VDP, ranked by accuracy and ease of use:

Enter runway wpt and threshold altitude at 3R of DES page.

VASI - but won't work if in the clouds or greater than 4 nm.

CONSTANT ANGLE

Pilot Procedural Technique

(This is not "Vertical Guidance" (VNAV) or an RNAV Approach)

Non EFIS with U1.x (old) software

- 1. Must be manually built; two ways.
- Your teammate must back you up in constructing this wpt. (a) Retrieve the destination runway's coordinates using the REF NAV DATA page. Write them down then use REF NAV DATA again to build a wpt using these coordinates. Example: Name it R26
- (b) The runway wpt can also be built using a Place-Bearing/Distance method from the OM/FAF.

Example: NDB approach to RW26 at IAH: NIXIN265/5.7

- 2. Put this created wpt in a FIX page for storeage and use later.
- 3. When desired, place your runway wpt from the FIX page to the s/p and add the desired altitude to it. Example using R26, we'd put R26/0150 into 3R of the DES page. The V/B on the DES page will display your angle to the runway.

PROCEDURE A STEP DOWN PROCEDURE

- 1. Arrive at the FAF fully configured and at target speed.
- 4. At 1000 AGL, reduce V/S to 1000 fpm.
- - 5. At MDA, (ALT HOLD annunciated) set missed approach altitude. V/S is armed 6. If field is in sight start descent at the VDP, not before or after.

 - 7. If field does not appear before the VDP fly to the missed approach point and accomplish the missed approach procedure.

PROCEDURE B CONSTANT ANGLE (VNAV inside FAF not available)

- 1. At cruise and before briefing the approach, build a wpt at the runway threshold. Ref: BUILDING A RUNWAY WAYPOINT.
- 2. Plan to shoot the VOR or LOC approach with raw data. Use LNAV for an NDB and LOC Back Crs approach, but monitor raw data as it is controlling.
- 3. While being vectored, take the created wpt from the FIX page and place in 3R of the DES page with the desired altitude. Now you can monitor your angle from the runway by watching the angle indicator (V/B). Displays on the DES page at lines 3R and 4R will not interfer with a VNAV PATH/SPD descent. Think ANGLE, not PATH, when looking at the V/B. (Angle calculator)
- accuracy is to monitor the ANP. If you don't have ANP, a technique is to compare the LOC or VOR DME (RDMI) to the RNAV DME (FIX page). (Example: Raw data IGHI
- 6. Arrive at the FAF fully configured and at target speed. The MDA should be set in the
- 7. At the FAF, check the angle indicator; when it reaches 2.8°, and not until, thumbwheel
- display, shows the angle you are to the threshold. Do not let it get less than your own limit - mine is 2.8°. (2.75° - 3.77° are considered standard). It's best just to bracket 3°. Now keep the FPA at 3° using the V/S thumbwheel.
- 8. As you descend, the wind usually changes; the V/S required to maintain a 3° V/B will also change - it is very dynamic. If you get below 2.8°, set V/S to zero until the angle is within your desired range. The required V/S is usually higher at the FAF than
- displayed at line 4. You'll find the angle indicator and FPA indicator very handy tools.
- Don't use the FPA or V/B below the MDA or if the FMC position is not accurate.

10.If the field does not come in sight prior to the MDA, level at the MDA, set the missed approach altitude and continue to the missed approach point. Don't dive for the runway after passing the VDP or if the angle indicator is in excess of your own limit. (Don't rotate through the MDA unless your governing body has approved such a maneuver; the MDA cannot be treated like a DH.)

B737 PROFILES

PF = Pilot Flying

PM = Pilot Monitoring

PROCEDURE C STEP DOWN PROCEDURE USING V/B FOR VDP

Steps 1 through 6 are the same as Procedure B.

- (Steps 7, 8, and 9 are the same as steps 3, 4, and 5 of Procedure A.)
- 7. At the FAF, dial 1,000 to 1,500 fpm descent in the V/S window.
- 8. At 1000 AGL, reduce V/S to 1000 fpm.
- 9. At MDA, (ALT HOLD annunciated) set missed approach altitude. V/S is armed.
- 10. When the field comes in sight, start descent when the V/B indicates 2.8°, not before. Dial the V/S that is displayed at line 4R.
- 11. If field does not appear before the V/B indicates 3.0°, fly to the missed approach point and accomplish the missed approach procedure.

LEARNING PROCEDURE

Learn how to shoot Procedure B or C approaches by practicing when an ILS is being conducted in visual conditions. You'll learn how to quickly set the FMC up and how the V/B and V/S indications on the DES page operate. This will lead to confidence in the procedure.

Notes

The Constant Angle technique is only recommended if you do not have the capability of using VNAV. VNAV is superior to this Constant Angle technique because there's less work involved in setup, and the A/P can be coupled to the VNAV path. However, the RNAV approach must be contained in the database with a GP leg and your aircraft must be capable of such an approach; and your carrier must allow and train the procedure.

For non-precision approaches that do not have vertical guidance, the minimum altitude may be specified as a minimum descent altitude - MDA (H). You cannot rotate through the floor of an MDA.

For non-precision approaches that use a VNAV path, such as the RNAV approach in this package, the minimum altitude may be specified as a decision altitude - DA (H). You may rotate through the DA in a missed approach.

This is a collection of "angle notes" from practice over the past several years. The learning curve continues with this tool. Please send me your experiences and questions.

All examples below assume no wind. The angle should be adjusted if configured differently or if you have a headwind or tailwind on final.

With the runway threshold and altitude entered at 3R of DES page ... (1) The limit you can start your turn to base from a downwind is when V/B

displays 8° (flaps 10, gr. down and 200 kts). (2) You can start your turn to base...

from a teardrop when V/B displays 8.5° (flaps 10, gr. down and 200 kts). You want about 4.5 degrees V/B on 2 nm base, and configured at 170 kts. You want to be less than 4 degrees turning onto final, configured. You can fly direct to the runway at 250 kts until the V/B from the threshold is 2.0°, then start decelerating (idle power) and configuring. If you're flying direct-to or dog-leg-to the runway at V/B from the runway of 3°. 250 kts and calm winds, you've got an energy problem.

Page 5

- - DME (110.9) vs: RNAV IGHI DME (IGHI entered in the FIX page.)

 - the V/S that is indicated at line 4R of the DES. You're actually setting the FPA to 3°! The angle indicator (V/B), right next to the V/S

 - at lower altitudes. You'll go below your desired V/B if your V/S is greater than that
 - 9. When the field is in sight, continue flying the V/S that maintains the 3° FPA, then take over visually. You'll be impressed with the smoothness of this technique. Caution:
- the threshold crossing height. (needs 4 characters for altitude) 4. The V/B on the DES page will display your angle to the runway.

300 ft per mile = 2.8° slope. Divide HAT by 300. Ex: LOC 26 IAH. HAT at MDA is 464 ft. Divide by 300 = 1.5 nm needed to descend from MDA to runway. VDP is 1.5 nm from runway threshold or D3.2 IJYV. (1.7 + 1.5) Timino For 130 kt gs: 10 ft per second = 2.8° slope. [Time from FAF to MAP] minus [10% of HAT]

DME

Angle (V/B) indication on DEScent page

study and practice but works great!

Ex: NDB 26 IAH. HAT at MDA is 624 ft or 62 seconds. FAF to MAP is 2:27 at 140 kts. Subtract 62 = 1:25. So, FAF to VDP is 1:25. This is a rough estimate. For each 10 kts above 130 kt groundspeed, add 10 seconds.

V/S Selection at a 2.8° point such as the OM or the VDP:

Divide the groundspeed by two. Add a zero. Ex: 140 kts = 700 fpm This rate of descent will equal a 2.8° angle. Add 50' for 3°. (750 fpm) CAUTION: As you descend, the ground speed usually decreases, necessitating a corresponding decrease in the selected vertical speed. Good rule of thumb when you're up to your knees in alligator ponds at night.

BUILDING A RUNWAY WAYPOINT ILS Approach loaded and no need to display step down altitudes. 1. From the ARRIVALS page, select the ILS approach.

- 2. Delete all altitudes on the LEGS page except the altitude at the runway. Of course you don't want to use this technique when you
- plan to use these "LEG" altitudes on an RNAV approach. 3. When being vectored in HDG SEL, do an intercept-to or direct-to a wpt on the approach or the runway itself.
- 4. The V/B on the DES page will display your angle to the runway because it's the only wpt on the LEGS page left with a hard altitude

runway.

5. Note: There can be no DISCOs on the LEGS page prior to the

Altitudes desired to be left on LEGS page.

- 1. From the ARRIVALS page, select the runway or ILS approach.
- 2. Not req'd for 10.5 and up. Using the Along Track Wpt feature, place the runway in the s/p, type /-.1 after it, and place back on top of the runway. A wpt one tenth of a mile inside the threshold will appear. Downselect this new wpt to the s/p and press the

ERASE prompt. Now the LEGS page is unchanged. The new wpt in the s/p. This is your new runway threshold wpt. Put this created wpt in a FIX page for storeage for use later. (Ex: RW201) 3. When desired, place your runway wpt from the FIX page to the

scratchpad and add the desired altitude to it. Example using RW26, we'd put RW201/0180 into 3R of the DES page. This wpt

created .1 nm inside the runway always needs 30 feet more than

- MCP ALT SEL window. V/S is now armed.

- While being vectored for the approach, accomplish an intercept-leg-to the applicable wpt and select the DES page to monitor the angle to the runway. 5. The V/B tool needs an accurate FMC position. The easiest way to check FMC position

2. The MDA should be set in the MCPALT SEL window. V/S is armed. 3. At the FAF, dial 1000 to 1500 fpm descent in the V/S window.

Helpful hints:

Go into the sim with a positive attitude. It's an opportunity to practice maneuvers, some of which you haven't had the chance to do for a while. It should always be a good learning experience. Practice to improve your instrument scan on the line by flying without the Flight Director on a regula basis. A good scan will help enormously during non-normal ops.

PITCH 'N POWER

target altitude.

Parts from INSTRUMENT FLYING, Dept of US Air Force, 1960 (I've done some editing) Learn what to change (pitch, bank, or power) and titude and or power. When the attitude and power are

how much change is required. This is the Control properly controlled, indications on the performance and Performance Method.

The control instruments are the attitude indica- a minimum of lag. tor (ADI) and the power indicators (N1 or Fuel Flow)

The performance instruments will know when altitude is calculated by using 10% of the climb or to change the attitude and / or power. They are the descent rate. If you're climbing at 1,500 fpm, begin altimeter, vertical speed, airspeed, direction, and leveling off no later than 150 ft before reaching the navigation (HSI or Moving Map) indicators.

Establishing an attitude and power setting (control) When leveling the 737, pulling the thrust levers will result in the desired performance. Known pitch back will bring the nose down. Pushing the thrust and approximate fuel flows or N1 will help reduce levers up will raise the nose. your workload.

How to know what to change (pitch and bank of the ADI. The instruments scanned depends on the the nose, or thrust) is simple. Pitch control, by raising maneuver, but it may include shifting the eyes from or lowering the nose is used primarily to maintain the ADI to the altimeter, dart over to the heading an altitude or to control the vertical speed. Bank indicator, back to the ADI, then to the airspeed. This control is used to maintain a heading or a desired takes many hours of concentrated practice, especially turn. Bank changes are made in reference to nav in a high speed airplane. Left neglected, scanning requirements, such as a heading vector, tracking the skills pick up drag rather than speed. magenta line on the Map, or following the localizer. Symptoms of insufficient reference to the control Fuel Flow/N1 is used for maintaining or changing instruments are readily recognizable. If you do not the airspeed (except during fixed power maneuvers have in mind some definite attitude and power setting such as climbout).

After or during the change of attitude and / or on the performance instruments fluxuate erratically, power, the performance instruments are crosschecked then you are not referring sufficiently to the control to see if their indications changed as desired. Flying instruments. You will be "chasing" indications, by reference to instruments is simply a continuous especially the FD. repetition of this process. You must glance from the Develop these skills and you can save an airplane, ADI to the altimeter - back to the ADI - then a glance crew, and passengers that has lost a system such at another performance instrument, back to the ADI, as the pitot-static or one that has improper Flight and so forth, including the standby ADI. The proper Director commands. Learning these skills will make relative amount of attention must be given to each you a better pilot because you can integrate the raw performance instrument. Do not devote too much data with the FD cues, and increase your own self attention to one performance instrument and fail to confidence. cross-check the control instrument.

A good scanning skill can be maintained even 25°, use 25° bank. Heading change less than 25°, when the autopilot is engaged.

PITCH 'N POWER CONTROL AND PERFORMANCE METHOD Helpful hints: Anytime you turn a knob, move a switch, or issue a command, look for results. "If.... then..."

Changes in the indications on the performance

instruments will lag slightly behind changes of at-

instruments will stabilize or change smoothly with

A level-off leadpoint is the altitude at which you

should begin applying control for level flight. This

A scan technique should begin and end with

that are to be held or established and the indications

Banking Rule: For heading changes more than

Roll-out Rule: Divide the bank angle by 2. For a 20° bank begin roll-out 10° before the desired

divide the heading change by 2.

heading.

that's your que for full concentration.

Both pilots are flying all the time. Just happens one is on the controls. When you take the active runway for takeoff, Always roll towards the "sky pointer"

Regardless of aircraft attitude, FAST always consider the Bank Index ٠ Pointer as being straight up. 0 Think of the Bank Index Pointer as the "sky pointer".

DH ∇



